

GEORGIA DEPARTMENT OF TRANSPORTATION

GDOT Project No: NH000-0073-03(242)

PI No: 714130

JBT Project No. 255717

Bridge No. 33

I-75 REVERSIBLE OVER FREY RD

November, 2009

COBB COUNTY

DESIGN CALCULATIONS

Note 1: Georgia Department of Transportation (GDOT) terminated Contract Number TOURDPPI60072 for its convenience prior to the completion of all work under that contract and directed that the work with respect to these calculations be discontinued.

(a) These calculations were not completed at the time of GDOT's direction and the information contained herein is not complete and/or has not been fully verified or checked. These calculations are a work-in-progress and are presented only as such.

(b) Any user is cautioned that the use of these calculations and any related information or calculations, without access to pertinent factors and without proper regard for their purpose, could lead to erroneous conclusions.

(c) If any such calculations or any information contained herein is used in future work efforts or any follow on design work activity, a complete confirmation of the information contained herein should be performed prior to any such use.

(d) GTP has no responsibility for the use of this information not under its direct control.

Prepared for Georgia Transportation Partners
Atlanta, Georgia

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Purpose of Calculation

Bridge design calculations for Bridge #33 were made for costing purposes.

1. Specifications and References

AASHTO 17th Edition, 2002

GDOT Bridge Design Manual, 2008

2. Computer

Computer Type Used: PC

Operating System: Windows XP, Pentium 4, 2GB RAM (min.)

3. Computer Programs (Standard Computer Program)

Excel, Microsoft Office 2003 – JBT Calculation Spreadsheets

BRLLCA, 2008 – Live Load Case Program, by GDOT

BRPIER, 2008 – Pier Design and Analysis, by GDOT

BRSPAN, 2008 – Simple Beam Design and Analysis, by GDOT

CALCULATION COVER SHEET

PROJECT	JOB NO.	CALC NO.	SHEET
I-75 / I-575 NORTHWEST CORRIDOR	NH000-0073-03(242)	BR#33	1
SUBJECT	DISCIPLINE		
Slab Design	STRUCTURAL		

CALCULATION STATUS DESIGNATION	PRELIMINARY	CONFIRMED	SUPSEDED	VOIDED	INCOMPLETE
	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>

COMPUTER PROGRAM/TYPE	SCP	MAINFRAME	PC	PROGRAM	VERSION/RELEASE NO.
	<input checked="" type="radio"/> YES <input type="radio"/> NO	<input type="radio"/>	<input checked="" type="radio"/>	Excel	2003

Note 1: Georgia Department of Transportation (GDOT) terminated Contract Number TOURDPP160072 for its convenience prior to the completion of all work under that contract and directed that the work with respect to these calculations be discontinued.

(a) These calculations were not completed at the time of GDOT's direction and the information contained herein is not complete and/or has not been fully verified or checked. These calculations are a work-in-progress and are presented only as such.

(b) Any user is cautioned that the use of these calculations and any related information or calculations, without access to factors and without proper regard for their purpose, could lead to erroneous conclusions.

(c) If any such calculations or any information contained herein is used in future work efforts or any follow on design work activity, a complete confirmation of the information contained herein should be performed prior to any such use.

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Slab Design calculations are included for spans 1, 2, and 3.

A	As per GDOT's termination for convenience direction	13	13	JCR			11/30/09
NO.	REASON FOR REVISION	TOTAL NO. OF SHEETS	LAST SHEET NO.	BY	CHECKED	APPROVED/ ACCEPTED	DATE
RECORD OF REVISIONS							

CALCULATION SHEET

PROJECT: I-75 / I-575 NORTHWEST CORRIDOR
JOB NUMBER NH000-0073-03(242)
CALC NO. BR#33

SUBJECT: Slab Design
BY: JCR DATE: 11/30/2009

SHEET NO.
SHEET REV.

Sufficient sample calculations representative of the scope and conditions in the design calculation were performed and the results compared to demonstrate the computer program adequacy.

BRIDGE: I-75 over Frey Road
COUNTY: COBB
P.I. NO: 713640
PROJECT: NH000-0575-01(028)

J.B. TRIMBLE, INC.



SPAN 1

JOB NO: 31-6036
DESIGNED BY: SHG
DATE: 10/14/2009

psc
10/24/09

PRELIMINARY INFORMATION

INTERMEDIATE SLAB THICKNESS = 8.000 IN
OVERHANG SLAB THICKNESS = 8.000 IN
GIRDER SPACING = 7.167 FT
NUMBER OF GIRDERS = 4
OVERHANG WIDTH = 3.083 FT
TOP FLANGE WIDTH = 12.000 IN
CONCRETE STRENGTH, f_c = 3500 PSI
STEEL STRENGTH, f_y = 60000 PSI
PARAPET HEIGHT = 2.667 FT
PARAPET WIDTH = 1.625 FT
PARAPET AREA = 2.700 SF
C.G. FROM OUTSIDE = 0.667 FT
TOP BAR CLEARANCE = 2.750 IN
BOTTOM BAR CLEARANCE = 1.000 IN
GROOVED DEPTH = 0.250 IN
DESIGN SPEED = 50.00 MPH (IF CENTRIFUGAL CONSIDERED)
RADIUS = 5890.00 FT (IF CENTRIFUGAL CONSIDERED)
WHEEL LOAD = 16.00 KIPS HS20
IMPACT FACTOR = 1.30
ADDITIONAL LOAD = 30.00 PSF
RAILING LOAD = 10.00 KIP AT TOP OF PARAPET

BAR DETAILS		
SIZE	AREA	WEIGHT
Not Needed	0	0
No. 3	0.11	0.376
No. 4	0.20	0.668
No. 5	0.31	1.043
No. 6	0.44	1.502
No. 7	0.60	2.044
No. 8	0.79	2.670
No. 9	1.00	3.400
No. 10	1.27	4.300
No. 11	1.56	5.310
No. 14	2.25	7.650
No. 18	4.00	13.600

INTERMEDIATE SLAB DESIGN

BEAM TYPE: STEEL (TBL STEEL, PSC, BULB-T)

EFFECTIVE SPAN LENGTH = 6.667 FT

AASHTO 3.24.1.2

DEAD LOAD

SLAB D.L. = 0.100 KIP/FT/LF
ADDITIONAL D.L. = 0.030 KIP/FT/LF
TOTAL D.L. = 0.130 KIP / FT / LF

DEAD LOAD MOMENT = $1.3 \cdot (WT \cdot DL) \cdot (SPAN)^2 / 10 = 0.751$ KIP-FT / LF

LIVE LOAD

WHEEL LOAD = 16.00 KIPS
CONT. FACTOR = 0.80
IMPACT = 1.30

LIVE LOAD MOMENT = $2.17 \cdot ((S + 2)/32) \cdot P \cdot (LL + I) \cdot 0.8 = 9.780$ KIP-FT / LF

AASHTO 3.24.3.1

CENTRIFUGAL LOAD

$C = 6.65 \cdot S^2 / R = 0.028$ FRACTION OF LIVE LOAD

AASHTO 3.10.1

CENTRIFUGAL FORCE MOMENT = $1.3 \cdot ((S + 2)/32) \cdot P \cdot (LL + I) \cdot 0.8 \cdot C = 0.166$ KIP-FT / LF

AASHTO TABLE 3.22.1A

TOTAL DESIGN MOMENT (ϕM_u) = 10.697 KIP-FT / LF = 128.37 K-IN / LF

FLEXURE STRENGTH

$\phi M_n > M_u$ $\phi = 0.90$

AASHTO 8.16.3.2

$\phi M_n = \phi \cdot [A_s \cdot f_y \cdot (d - a/2)]$ where $a = A_s \cdot f_y / (0.85 \cdot f_c \cdot b)$

$a = 1.681$ As
 $d_{top} = 4.938$ IN USE 5 BAR As = 0.31 IN² / LF
 $d_{bot} = 6.438$ IN USE 5 BAR As = 0.31 IN² / LF

TOP STEEL

266.625 As - 45.38 As² = 128.37 K-IN / LF

TOP BAR = NO. 5 SPACED AT 6.375 IN As = 0.58 IN² / LF

$\phi M_n = 140.13$ K-IN / LF $\geq \phi M_u = 128.37$ K-IN / LF OK

BOTTOM STEEL

347.625 As - 45.38 As² = 128.37 K-IN / LF

BOT BAR = NO. 5 SPACED AT 6.375 IN As = 0.58 IN² / LF

$\phi M_n = 187.40$ K-IN / LF $\geq \phi M_u = 128.37$ K-IN / LF OK

BRIDGE: I-75 over Frey Road
COUNTY: COBB
P.I. NO: 713640
PROJECT: NH000-0575-01(028)

J.B. TRIMBLE, INC.



SPAN 1

JOB NO: 31-6036
DESIGNED BY: SHG
DATE: 10/14/2009

OVERHANG SLAB DESIGN

EFFECTIVE SPAN LENGTH = 2.583 FT

AASHTO 3.24.5.1

DEAD LOAD

SLAB D.L. = 0.100 KIP/FT/LF
ADDITIONAL D.L. = 0.030 KIP/FT/LF
PARAPET D.L. = 0.405 KIP/FT/LF

DL MOMENT @ FLANGE:

SLAB MOM = 0.334 KIP-FT/LF
ADD'L MOM = 0.014 KIP-FT/LF
PARAPET MOM = 0.776 KIP-FT/LF

TOTAL MOM = 1.124 KIP-FT/LF

DL MOMENT @ EDGE OF BARRIER:

SLAB MOM = 0.132 KIP-FT/LF
ADD'L MOM = 0.000 KIP-FT/LF
PARAPET MOM = 0.388 KIP-FT/LF

TOTAL MOM = 0.520 KIP-FT/LF

DEAD LOAD MOMENT @ FLANGE = 1.3 * TOTAL MOMENT = 1.461 KIP-FT / LF
D.L. MOMENT @ EDGE OF BARRIER = 1.3 * TOTAL MOMENT = 0.676 KIP-FT / LF

LIVE LOAD

WHEEL LOAD = 16.00 KIPS

IMPACT = 1.30
MOM ARM (X) = 0.46 FT
E = 0.8 * X + 3.75 = 4.12 FT

LIVE LOAD MOMENT = 2.17 * (P(LL + I) / E) * X = 5.625 KIP-FT / LF

AASHTO 3.24.5.1.1

CENTRIFUGAL LOAD

C = 6.68 * S^2 / R = 0.028 FRACTION OF LIVE LOAD

CENTRIFUGAL FORCE MOMENT = 1.3 * (P(LL + I) / E) * X * C = 0.142 KIP-FT / LF

RAILING LOAD

RAILING LOAD = 10.00 KIPS

RAILING LOAD @ FLANGE:

MOM ARM (H) = 3.111 FT
DISTANCE (X) = 1.92 FT
E = 0.8 * X + 5.00 = 6.53 FT

RAILING LOAD @ EDGE OF BARRIER:

MOM ARM (H) = 3.11 FT
DISTANCE (X) = 0.96 FT
E = 0.8 * X + 5.00 = 5.77 FT

RAIL MOM @ FLANGE = 2.17 * (P_{rail} / E) * H = 10.333 KIP-FT / LF

RAIL MOM @ EDGE OF BARRIER = 2.17 * (P_{rail} / E) * H = 11.707 KIP-FT / LF

AASHTO 3.24.5.2

SUMMARY OF MOMENTS:

DL + LL @ FLANGE = 6.628 KIP-FT / LF
DL + RAIL @ FLANGE = 11.794 KIP-FT / LF
DL + RAIL @ BARRIER = 12.383 KIP-FT / LF

TOTAL DESIGN MOMENT (∅ Mu) = 12.383 KIP-FT / LF = 148.60 K-IN / LF

FLEXURE STRENGTH

∅ Mn > Mu

∅ = 0.90

AASHTO 8.16.3.2

∅ Mn = ∅ * [As * fy * (d - a/2)] where a = As * fy / (0.85 * fc * b)

a = 1.651 As

d_{top} = 4.938 IN

USE 5 BAR

As = 0.31 IN² / LF

PROVIDE ADDITIONAL OVERHANG STEEL = 4 BAR

As = 0.20 IN² / LF

TOP STEEL

266.625 As -

45.38 As/2 =

148.60 K-IN / LF

TOP BAR = NO. 5 SPACED AT 6.375 IN As = 0.58 IN² / LF

∅ Mn = 146.13 K-IN / LF < ∅ Mu = 148.60 K-IN / LF ADD. REINF. NEEDED!!

ADD'L BAR = NO. 4 SPACED AT 12.75 IN As = 0.19 IN² / LF

Mn = 178.74 K-IN / LF ≥ Mu = 148.60 K-IN / LF OK

BRIDGE: I-75 over Frey Road
COUNTY: COBB
P.I. NO: 713640
PROJECT: NH000-0575-01(028)

J.B. TRIMBLE, INC.



SPAN 2

JOB NO: 31-6036
DESIGNED BY: SHG
DATE: 10/14/2009

*PSG
10/20/09*

PRELIMINARY INFORMATION

INTERMEDIATE SLAB THICKNESS = 8.000 IN
OVERHANG SLAB THICKNESS = 8.000 IN
GIRDER SPACING = 7.166 FT
NUMBER OF GIRDERS = 4
OVERHANG WIDTH = 3.063 FT
TOP FLANGE WIDTH = 14.000 IN
CONCRETE STRENGTH, f_c = 3500 PSI
STEEL STRENGTH, f_y = 60000 PSI
PARAPET HEIGHT = 2.667 FT
PARAPET WIDTH = 1.625 FT
PARAPET AREA = 2.700 SF
C.G. FROM OUTSIDE = 0.667 FT
TOP BAR CLEARANCE = 2.750 IN
BOTTOM BAR CLEARANCE = 1.000 IN
GROOVED DEPTH = 0.250 IN
DESIGN SPEED = 50.00 MPH (IF CENTRIFUGAL CONSIDERED)
RADIUS = 5890.00 FT (IF CENTRIFUGAL CONSIDERED)
WHEEL LOAD = 16.00 KIPS H520
IMPACT FACTOR = 1.30
ADDITIONAL LOAD = 30.00 PSF
RAILING LOAD = 10.00 KIP AT TOP OF PARAPET

BAR DETAILS		
SIZE	AREA	WEIGHT
Not Needed	0	0
No. 3	0.11	0.376
No. 4	0.20	0.668
No. 5	0.31	1.043
No. 6	0.44	1.502
No. 7	0.60	2.044
No. 8	0.79	2.670
No. 9	1.00	3.400
No. 10	1.27	4.300
No. 11	1.56	5.310
No. 14	2.25	7.650
No. 18	4.00	13.600

INTERMEDIATE SLAB DESIGN

BEAM TYPE: STEEL (TB, STEEL, PSC, BULB-T)

EFFECTIVE SPAN LENGTH = 6.583 FT

AASHTO 3.24.1.2

DEAD LOAD

SLAB D.L. = 0.100 KIP/FT/LF
ADDITIONAL D.L. = 0.030 KIP/FT/LF
TOTAL D.L. = 0.130 KIP / FT / LF

$$\text{DEAD LOAD MOMENT} = 1.3 \cdot (\text{WT DL}) \cdot (\text{SPAN})^2 / 10 = 0.732 \text{ KIP-FT / LF}$$

LIVE LOAD

WHEEL LOAD = 16.00 KIPS
CONT. FACTOR = 0.80
IMPACT = 1.30

$$\text{LIVE LOAD MOMENT} = 2.17 \cdot ((S + 2)/32) \cdot P \cdot (LL + I) \cdot 0.8 = 9.685 \text{ KIP-FT / LF}$$

AASHTO 3.24.3.1

CENTRIFUGAL LOAD

$$C = 6.68 \cdot S^2 / R = 0.028 \text{ FRACTION OF LIVE LOAD}$$

AASHTO 3.10.1

$$\text{CENTRIFUGAL FORCE MOMENT} = 1.3 \cdot ((S + 2)/32) \cdot P \cdot (LL + I) \cdot 0.8 \cdot C = 0.165 \text{ KIP-FT / LF}$$

AASHTO TABLE 3.22.1A

$$\text{TOTAL DESIGN MOMENT } (\phi M_u) = 10.582 \text{ KIP-FT / LF} = 126.98 \text{ K-IN / LF}$$

FLEXURE STRENGTH

$$\phi M_n > M_u \quad \phi = 0.90$$

AASHTO 8.16.3.2

$$\phi M_n = \phi \cdot [A_s \cdot f_y \cdot (d - a/2)] \quad \text{where } a = A_s \cdot f_y / (0.85 \cdot f_c \cdot b)$$

$a = 1.681$ As
 $d_{top} = 4.938$ IN USE 5 BAR As = 0.31 IN² / LF
 $d_{bot} = 6.438$ IN USE 5 BAR As = 0.31 IN² / LF

TOP STEEL

$$266.625 \text{ As} - 45.38 \text{ As}^2 = 126.98 \text{ K-IN / LF}$$

TOP BAR = NO. 5 SPACED AT 6.375 IN As = 0.58 IN² / LF

$$\phi M_n = 140.13 \text{ K-IN / LF} \geq \phi M_u = 126.98 \text{ K-IN / LF} \quad \text{OK}$$

BOTTOM STEEL

$$347.625 \text{ As} - 45.38 \text{ As}^2 = 126.98 \text{ K-IN / LF}$$

BOT BAR = NO. 5 SPACED AT 6.375 IN As = 0.58 IN² / LF

$$\phi M_n = 187.40 \text{ K-IN / LF} \geq \phi M_u = 126.98 \text{ K-IN / LF} \quad \text{OK}$$

BRIDGE: I-75 over Frey Road
COUNTY: COBB
P.L. NO: 713640
PROJECT: NH000-0575-01(028)

J.B. TRIMBLE, INC.



SPAN 2

JOB NO: 31-6036
DESIGNED BY: SHG
DATE: 10/14/2009

OVERHANG SLAB DESIGN

EFFECTIVE SPAN LENGTH = 2.500 FT

AASHTO 3.24.5.1

DEAD LOAD

SLAB D.L. = 0.100 KIP/FT/LF
ADDITIONAL D.L. = 0.030 KIP/FT/LF
PARAPET D.L. = 0.405 KIP/FT/LF

DL MOMENT @ FLANGE:

SLAB MOM = 0.312 KIP-FT/LF
ADD'L MOM = 0.011 KIP-FT/LF
PARAPET MOM = 0.742 KIP-FT/LF
TOTAL MOM = 1.066 KIP-FT/LF

DL MOMENT @ EDGE OF BARRIER:

SLAB MOM = 0.132 KIP-FT/LF
ADD'L MOM = 0.000 KIP-FT/LF
PARAPET MOM = 0.388 KIP-FT/LF
TOTAL MOM = 0.520 KIP-FT/LF

DEAD LOAD MOMENT @ FLANGE = 1.3 * TOTAL MOMENT = 1.386 KIP-FT / LF
D.L. MOMENT @ EDGE OF BARRIER = 1.3 * TOTAL MOMENT = 0.676 KIP-FT / LF

LIVE LOAD

WHEEL LOAD = 16.00 KIPS
IMPACT = 1.30
MOM ARM (X) = 0.46 FT
E = 0.8 * X + 3.75 = 4.12 FT

LIVE LOAD MOMENT = 2.17 * (P(LL + I) / E) * X = 5.022 KIP-FT / LF

AASHTO 3.24.5.1.1

CENTRIFUGAL LOAD

C = 6.68 * S² / R = 0.026 FRACTION OF LIVE LOAD

CENTRIFUGAL FORCE MOMENT = 1.3 * (P(LL + I) / E) * X * C = 0.142 KIP-FT / LF

RAILING LOAD

RAILING LOAD = 10.00 KIPS

AASHTO 3.24.5.2

RAILING LOAD @ FLANGE:

MOM ARM (H) = 3.111 FT
DISTANCE (X) = 1.83 FT
E = 0.8 * X + 5.00 = 6.47 FT

RAILING LOAD @ EDGE OF BARRIER:

MOM ARM (H) = 3.11 FT
DISTANCE (X) = 0.96 FT
E = 0.8 * X + 5.00 = 5.77 FT

RAIL MOM @ FLANGE = 2.17 * (P_{rail} / E) * H = 10.440 KIP-FT / LF

RAIL MOM @ EDGE OF BARRIER = 2.17 * (P_{rail} / E) * H = 11.707 KIP-FT / LF

SUMMARY OF MOMENTS:

DL + LL @ FLANGE = 6.550 KIP-FT / LF
DL + RAIL @ FLANGE = 11.826 KIP-FT / LF
DL + RAIL @ BARRIER = 12.383 KIP-FT / LF

TOTAL DESIGN MOMENT (∅ M_u) = 12.383 KIP-FT / LF = 148.60 K-IN / LF

FLEXURE STRENGTH

AASHTO 6.16.3.2

∅ M_n > M_u ∅ = 0.90

∅ M_n = ∅ * [A_s * f_y * (d - a/2)] where a = A_s * f_y / [0.85 * f_c * b]

a = 1.681 As
d_{top} = 4.938 IN

USE 5 BAR

As = 0.31 IN² / LF

PROVIDE ADDITIONAL OVERHANG STEEL = 4 BAR

As = 0.20 IN² / LF

TOP STEEL

266.625 As - 45.38 As² = 148.60 K-IN / LF

TOP BAR = NO. 5 SPACED AT 6.375 IN As = 0.58 IN² / LF

∅ M_n = 140.13 K-IN / LF < ∅ M_u = 148.60 K-IN / LF ADD. REINF. NEEDED!!

ADD'L BAR = NO. 4 SPACED AT 12.75 IN As = 0.19 IN² / LF

M_n = 178.74 K-IN / LF ≥ M_u = 148.60 K-IN / LF OK

BRIDGE: I-75 over Frey Road
COUNTY: COBB
P.I. NO: 713640
PROJECT: NH000-0575-01(028)

J.B. TRIMBLE, INC.



SPAN 3

JOB NO: 31-6036
DESIGNED BY: SHG
DATE: 10/14/2009

PSC
10/20/09

PRELIMINARY INFORMATION

INTERMEDIATE SLAB THICKNESS = 7.875 IN
OVERHANG SLAB THICKNESS = 7.875 IN
GIRDER SPACING = 6.833 FT
NUMBER OF GIRDERS = 4
OVERHANG WIDTH = 3.333 FT
TOP FLANGE WIDTH = 12.000 IN
CONCRETE STRENGTH, f_c = 3500 PSI
STEEL STRENGTH, f_y = 60000 PSI
PARAPET HEIGHT = 2.867 FT
PARAPET WIDTH = 1.825 FT
PARAPET AREA = 2.700 SF
C.G. FROM OUTSIDE = 0.867 FT
TOP BAR CLEARANCE = 2.750 IN
BOTTOM BAR CLEARANCE = 1.000 IN
GROOVED DEPTH = 0.250 IN
DESIGN SPEED = 50.00 MPH (IF CENTRIFUGAL CONSIDERED)
RADIUS = 5890.00 FT (IF CENTRIFUGAL CONSIDERED)
WHEEL LOAD = 16.00 KIPS HS20
IMPACT FACTOR = 1.30
ADDITIONAL LOAD = 30.00 PSF
RAILING LOAD = 10.00 KIP AT TOP OF PARAPET

BAR DETAILS		
SIZE	AREA	WEIGHT
Not Needed	0	0
No. 3	0.11	0.375
No. 4	0.20	0.668
No. 5	0.31	1.043
No. 6	0.44	1.502
No. 7	0.60	2.044
No. 8	0.79	2.670
No. 9	1.00	3.400
No. 10	1.27	4.300
No. 11	1.56	5.310
No. 14	2.25	7.650
No. 18	4.00	13.600

INTERMEDIATE SLAB DESIGN

BEAM TYPE: STEEL (TB, STEEL, PSC, BULB-T)

EFFECTIVE SPAN LENGTH = 6.333 FT

AASHTO 3.24.1.2

DEAD LOAD

SLAB D.L. = 0.098 KIP/FT/LF
ADDITIONAL D.L. = 0.030 KIP/FT/LF
TOTAL D.L. = 0.128 KIP / FT / LF

$$\text{DEAD LOAD MOMENT} = 1.3 \cdot (\text{WT DL}) \cdot (\text{SPAN})^2 / 10 = 0.670 \text{ KIP-FT / LF}$$

LIVE LOAD

WHEEL LOAD = 16.00 KIPS
CONT. FACTOR = 0.80
IMPACT = 1.30

$$\text{LIVE LOAD MOMENT} = 2.17 \cdot ((5 + 2/32) \cdot P \cdot (LL + I) \cdot 0.8 = 9.493 \text{ KIP-FT / LF}$$

AASHTO 3.24.3.1

CENTRIFUGAL LOAD

$$C = 6.68 \cdot S^2 / R = 0.028 \text{ FRACTION OF LIVE LOAD}$$

AASHTO 3.10.1

$$\text{CENTRIFUGAL FORCE MOMENT} = 1.3 \cdot ((5 + 2/32) \cdot P \cdot (LL + I) \cdot 0.8 \cdot C = 0.160 \text{ KIP-FT / LF}$$

AASHTO TABLE 3.22.1A

$$\text{TOTAL DESIGN MOMENT } (\phi M_u) = 10.232 \text{ KIP-FT / LF} = 122.79 \text{ K-IN / LF}$$

FLEXURE STRENGTH

$$\phi M_n > M_u \quad \phi = 0.90$$

AASHTO 8.16.3.2

$$\phi M_n = \phi \cdot [A_s \cdot f_y \cdot (d - a/2)] \quad \text{where } a = A_s \cdot f_y / [0.85 \cdot f_c \cdot b]$$

$a = 1.681$ As
 $d_{top} = 4.813$ IN USE 5 BAR As = 0.31 IN² / LF
 $d_{bot} = 6.313$ IN USE 5 BAR As = 0.31 IN² / LF

TOP STEEL

$$259.875 \text{ As} - 45.38 \text{ As}^2 = 122.79 \text{ K-IN / LF}$$

TOP BAR = NO. 5 SPACED AT 6.500 IN As = 0.57 IN² / LF

$$\phi M_n = 133.87 \text{ K-IN / LF} \geq \phi M_u = 122.79 \text{ K-IN / LF} \quad \text{OK}$$

BOTTOM STEEL

$$340.875 \text{ As} - 45.38 \text{ As}^2 = 122.79 \text{ K-IN / LF}$$

BOT BAR = NO. 5 SPACED AT 6.500 IN As = 0.57 IN² / LF

$$\phi M_n = 180.22 \text{ K-IN / LF} \geq \phi M_u = 122.79 \text{ K-IN / LF} \quad \text{OK}$$

BRIDGE: I-75 over Frey Road
COUNTY: COBB
P.I. NO: 713640
PROJECT: NH000-0575-01(028)

J.B. TRIMBLE, INC.



SPAN 3

JOB NO: 31-6036
DESIGNED BY: SHG
DATE: 10/14/2009

OVERHANG SLAB DESIGN

EFFECTIVE SPAN LENGTH = 2.633 FT

AASHTO 3.24.5.1

DEAD LOAD

SLAB D.L. = 0.098 KIP/FT/LF
ADDITIONAL D.L. = 0.030 KIP/FT/LF
PARAPET D.L. = 0.405 KIP/FT/LF

DL MOMENT @ FLANGE:

SLAB MOM = 0.395 KIP-FT/LF
ADD'L MOM = 0.022 KIP-FT/LF
PARAPET MOM = 0.877 KIP-FT/LF

TOTAL MOM = 1.294 KIP-FT/LF

DL MOMENT @ EDGE OF BARRIER:

SLAB MOM = 0.130 KIP-FT/LF
ADD'L MOM = 0.000 KIP-FT/LF
PARAPET MOM = 0.368 KIP-FT/LF

TOTAL MOM = 0.518 KIP-FT/LF

DEAD LOAD MOMENT @ FLANGE = 1.3 * TOTAL MOMENT = 1.683 KIP-FT / LF
D.L. MOMENT @ EDGE OF BARRIER = 1.3 * TOTAL MOMENT = 0.674 KIP-FT / LF

LIVE LOAD

WHEEL LOAD = 16.00 KIPS

IMPACT = 1.30
MOM ARM (X) = 0.71 FT
E = 0.8 * X + 3.75 = 4.32 FT

LIVE LOAD MOMENT = 2.17 * (P(LL + I) / E) * X = 7.403 KIP-FT / LF

AASHTO 3.24.5.1.1

CENTRIFUGAL LOAD

C = 6.68 * S² / R = 0.028 FRACTION OF LIVE LOAD

CENTRIFUGAL FORCE MOMENT = 1.3 * (P(LL + I) / E) * X * C = 0.210 KIP-FT / LF

RAILING LOAD

RAILING LOAD = 10.00 KIPS

RAILING LOAD @ FLANGE:

MOM ARM (H) = 3.104 FT
DISTANCE (X) = 2.17 FT
E = 0.8 * X + 5.00 = 6.73 FT

RAILING LOAD @ EDGE OF BARRIER:

MOM ARM (H) = 3.10 FT
DISTANCE (X) = 0.96 FT
E = 0.8 * X + 5.00 = 5.77 FT

RAIL MOM @ FLANGE = 2.17 * (P_{rail} / E) * H = 10.004 KIP-FT / LF

RAIL MOM @ EDGE OF BARRIER = 2.17 * (P_{rail} / E) * H = 11.681 KIP-FT / LF

AASHTO 3.24.5.2

SUMMARY OF MOMENTS:

DL + LL @ FLANGE = 9.296 KIP-FT / LF
DL + RAIL @ FLANGE = 11.687 KIP-FT / LF
DL + RAIL @ BARRIER = 12.355 KIP-FT / LF

TOTAL DESIGN MOMENT (∅ M_u) = 12.355 KIP-FT / LF = 148.25 K-IN / LF

FLEXURE STRENGTH

∅ M_n > M_u ∅ = 0.90

AASHTO 8.16.3.2

∅ M_n = ∅ * [A_s * f_y * (d - a/2)] where a = A_s * f_y / [0.85 * f_c * b]

a = 1.681 As
d_{top} = 4.813 IN

USE 5 BAR

As = 0.31 IN² / LF

PROVIDE ADDITIONAL OVERHANG STEEL = 4 BAR

As = 0.20 IN² / LF

TOP STEEL

259.875 As - 45.38 As/2 = 148.25 K-IN / LF

TOP BAR = NO. 5 SPACED AT 6.500 IN As = 0.57 IN² / LF

∅ M_n = 133.87 K-IN / LF < ∅ M_u = 148.25 K-IN / LF ADD. REINF. NEEDED!!

ADD'L BAR = NO. 4 SPACED AT 13.00 IN As = 0.18 IN² / LF

M_n = 176.71 K-IN / LF ≥ M_u = 148.25 K-IN / LF OK

SERVICE LOAD DESIGN OF BRIDGE SLAB

Georgia Department of Transportation
Office of Bridge and Structural Design
October 2003

13-MAY-04
07:49:26

WHEEL LOAD (Kips)	fc (ksi)	fs (ksi)	n	SLAB COVER (in)	FUTURE PAVING (kips/ft ²)	CONTINUITY FACTOR
16.00	1.400	24.000	9	2.750	0.030	0.8
=====						
EFFECTIVE SPAN LENGTH (ft-in)	SLAB THICKNESS MINIMUM ACTUAL (in) (in)		SIZE AND SPACING OF MAIN REINFORCEMENT (in)		DISTRUBUTION REINFORCEMENT MIDDLE HALF OUTER QUARTERS	
3 - 6	6.8150	7.000	# 5 at	8.625	3 - # 4	2 - # 4
3 - 7	6.8463	7.000	# 5 at	8.375	3 - # 4	2 - # 4
3 - 8	6.8774	7.000	# 5 at	8.250	3 - # 4	2 - # 4
3 - 9	6.9083	7.000	# 5 at	8.125	3 - # 4	2 - # 4
3 - 10	6.9391	7.000	# 5 at	8.000	3 - # 4	2 - # 4
3 - 11	6.9698	7.000	# 5 at	7.875	4 - # 4	2 - # 4
4 - 0	7.0018	7.125	# 5 at	8.000	4 - # 4	2 - # 4
4 - 1	7.0323	7.125	# 5 at	7.875	4 - # 4	2 - # 4
4 - 2	7.0626	7.125	# 5 at	7.750	4 - # 4	2 - # 4
4 - 3	7.0927	7.125	# 5 at	7.625	4 - # 4	2 - # 4
4 - 4	7.1228	7.125	# 5 at	7.500	4 - # 4	2 - # 4
4 - 5	7.1544	7.250	# 5 at	7.625	4 - # 4	2 - # 4
4 - 6	7.1843	7.250	# 5 at	7.500	4 - # 4	2 - # 4
4 - 7	7.2140	7.250	# 5 at	7.500	4 - # 4	2 - # 4
4 - 8	7.2436	7.250	# 5 at	7.375	4 - # 4	2 - # 4
4 - 9	7.2751	7.375	# 5 at	7.500	4 - # 4	2 - # 4
4 - 10	7.3045	7.375	# 5 at	7.375	5 - # 4	4 - # 4
4 - 11	7.3338	7.375	# 5 at	7.250	5 - # 4	4 - # 4
5 - 0	7.3630	7.375	# 5 at	7.125	5 - # 4	4 - # 4
5 - 1	7.3943	7.500	# 5 at	7.250	5 - # 4	4 - # 4
5 - 2	7.4234	7.500	# 5 at	7.125	5 - # 4	4 - # 4
5 - 3	7.4524	7.500	# 5 at	7.000	5 - # 4	4 - # 4
5 - 4	7.4812	7.500	# 5 at	7.000	5 - # 4	4 - # 4
5 - 5	7.5124	7.625	# 5 at	7.000	5 - # 4	4 - # 4
5 - 6	7.5412	7.625	# 5 at	7.000	5 - # 4	4 - # 4
5 - 7	7.5698	7.625	# 5 at	6.875	6 - # 4	4 - # 4
5 - 8	7.5984	7.625	# 5 at	6.750	6 - # 4	4 - # 4
5 - 9	7.6295	7.750	# 5 at	6.875	6 - # 4	4 - # 4
5 - 10	7.6579	7.750	# 5 at	6.750	6 - # 4	4 - # 4
5 - 11	7.6863	7.750	# 5 at	6.750	6 - # 4	4 - # 4
6 - 0	7.7145	7.750	# 5 at	6.625	6 - # 4	4 - # 4
6 - 1	7.7427	7.750	# 5 at	6.500	6 - # 4	4 - # 4
6 - 2	7.7738	7.875	# 5 at	6.625	6 - # 4	4 - # 4
6 - 3	7.8019	7.875	# 5 at	6.500	6 - # 4	4 - # 4
6 - 4	7.8299	7.875	# 5 at	6.500	7 - # 4	4 - # 4
6 - 5	7.8578	7.875	# 5 at	6.375	7 - # 4	4 - # 4

Span 3
6'-10"
-1'-0"
+2#(12")
6'-4"

SERVICE LOAD DESIGN OF BRIDGE SLAB

Georgia Department of Transportation
Office of Bridge and Structural Design
October 2003

13-MAY-04
07:49:26

WHEEL LOAD (Kips)	fc (ksi)	fs (ksi)	n	SLAB COVER (in)	FUTURE PAVING (kips/ft ²)	CONTINUITY FACTOR
16.00	1.400	24.000	9	2.750	0.030	0.8
EFFECTIVE SPAN LENGTH (ft-in)	SLAB THICKNESS MINIMUM (in)	ACTUAL (in)	SIZE AND SPACING OF MAIN REINFORCEMENT (in)	DISTRUBUTION REINFORCEMENT MIDDLE HALF	OUTER QUARTERS	
6 - 6	7.8889	8.000	# 5 at 6.500	7 -# 4	4 -# 4	
6 - 7	7.9167	8.000	# 5 at 6.375	7 -# 4	4 -# 4	
6 - 8	7.9445	8.000	# 5 at 6.375	7 -# 4	4 -# 4	
6 - 9	7.9722	8.000	# 5 at 6.250	7 -# 4	4 -# 4	
6 - 10	7.9998	8.000	# 5 at 6.250	7 -# 4	4 -# 4	
6 - 11	8.0309	8.125	# 5 at 6.250	7 -# 4	4 -# 4	
7 - 0	8.0585	8.125	# 5 at 6.250	7 -# 4	4 -# 4	
7 - 1	8.0860	8.125	# 5 at 6.125	8 -# 4	4 -# 4	
7 - 2	8.1134	8.125	# 5 at 6.125	8 -# 4	4 -# 4	
7 - 3	8.1446	8.250	# 5 at 6.125	8 -# 4	4 -# 4	
7 - 4	8.1719	8.250	# 5 at 6.125	8 -# 4	4 -# 4	
7 - 5	8.1992	8.250	# 5 at 6.000	8 -# 4	4 -# 4	
7 - 6	8.2265	8.250	# 5 at 6.000	8 -# 4	4 -# 4	
7 - 7	8.2577	8.375	# 5 at 6.000	8 -# 4	4 -# 4	
7 - 8	8.2849	8.375	# 5 at 6.000	8 -# 4	4 -# 4	
7 - 9	8.3121	8.375	# 5 at 5.875	9 -# 4	6 -# 4	
7 - 10	8.3392	8.375	# 5 at 5.875	9 -# 4	6 -# 4	
7 - 11	8.3662	8.375	# 5 at 5.750	9 -# 4	6 -# 4	
8 - 0	8.3976	8.500	# 5 at 5.875	9 -# 4	6 -# 4	
8 - 1	8.4246	8.500	# 5 at 5.750	9 -# 4	6 -# 4	
8 - 2	8.4515	8.500	# 5 at 5.750	9 -# 4	6 -# 4	
8 - 3	8.4784	8.500	# 5 at 5.625	9 -# 4	6 -# 4	
8 - 4	8.5099	8.625	# 5 at 5.750	9 -# 4	6 -# 4	
8 - 5	8.5367	8.625	# 5 at 5.625	10 -# 4	6 -# 4	
8 - 6	8.5636	8.625	# 5 at 5.625	10 -# 4	6 -# 4	
8 - 7	8.5903	8.625	# 5 at 5.500	10 -# 4	6 -# 4	
8 - 8	8.6170	8.625	# 5 at 5.500	10 -# 4	6 -# 4	
8 - 9	8.6487	8.750	# 5 at 5.625	10 -# 4	6 -# 4	
8 - 10	8.6754	8.750	# 5 at 5.500	10 -# 4	6 -# 4	
8 - 11	8.7020	8.750	# 5 at 5.500	11 -# 4	6 -# 4	
9 - 0	8.7286	8.750	# 5 at 5.375	11 -# 4	6 -# 4	
9 - 1	8.7605	8.875	# 5 at 5.500	11 -# 4	6 -# 4	
9 - 2	8.7871	8.875	# 5 at 5.375	11 -# 4	6 -# 4	
9 - 3	8.8136	8.875	# 5 at 5.375	11 -# 4	6 -# 4	
9 - 4	8.8401	8.875	# 5 at 5.375	11 -# 4	6 -# 4	
9 - 5	8.8665	8.875	# 5 at 5.250	12 -# 4	6 -# 4	

Span 2 →
Span 3 →

SECTION IV – CONCRETE AND REINFORCING STEEL

BRIDGE DECK DESIGN

No. 4.01

When designing bridge decks, the following criteria shall be applied:

For cast-in-place decks north of the fall line:

1. Specify Class AA concrete except for post-tensioned concrete boxes which shall have Class AA as a minimum, but may require a higher 28-day strength.
2. **Specify 2 3/4" (70 mm) cover to top bar reinforcement for bridge decks on interstate routes, state routes and routes with design year ADT equal to or greater than 2000.**
3. Specify 2 1/2" (65 mm) cover to top bar reinforcement for bridge decks on all other routes.

For cast-in-place decks south of the fall line:

1. Specify Class AA concrete except for post-tensioned concrete boxes which shall have Class AA as a minimum, but may require a higher 28-day strength.
2. Specify 2 1/4" (60 mm) cover to top bar reinforcement for bridge decks on interstate routes, state routes and routes with design year ADT equal to or greater than 2000.
3. Specify 2" (50 mm) cover to top bar reinforcement for bridge decks on all other routes.

For bridge decks of precast concrete elements, specify 2" cover to top bar reinforcement statewide.

Note that 1/4" of concrete thickness may be planed off of the top of cast-in-place decks on interstate routes, state routes and routes with design year ADT equal to or greater than 2000. Therefore, reduce slab thickness accordingly for strength calculations of composite slabs on steel or PSC beams and post-tensioned boxes.

Deck slabs shall be designed by the Service Load method with $f_c = 1400$ psi (10 MPa), as a rule.

The minimum 28 day strength (f'_c) for the deck concrete shall be 3500 psi (25 MPa). Slabs shall be designed so that the main slab reinforcement is the same in the bottom of the slab as in the top. To achieve this, the effective depth shall be taken as the distance from the bottom of the slab to the centroid of the top main reinforcing steel for both positive and negative moment. Positive and negative moments shall be assumed to be equal and shall be calculated in accordance with the AASHTO Specifications.

See Fig. 4-01 for a location map of the fall line for Georgia.

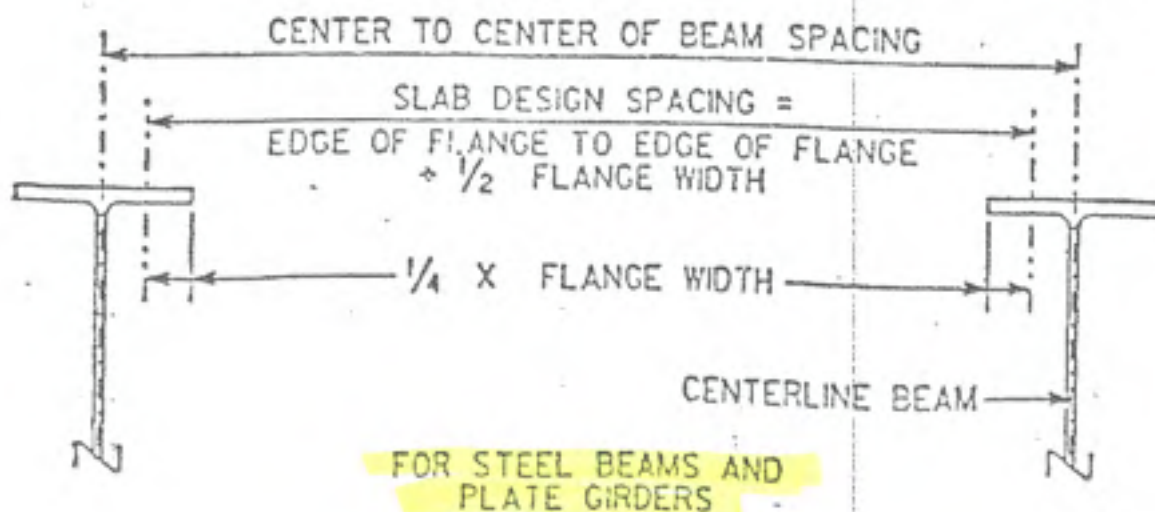
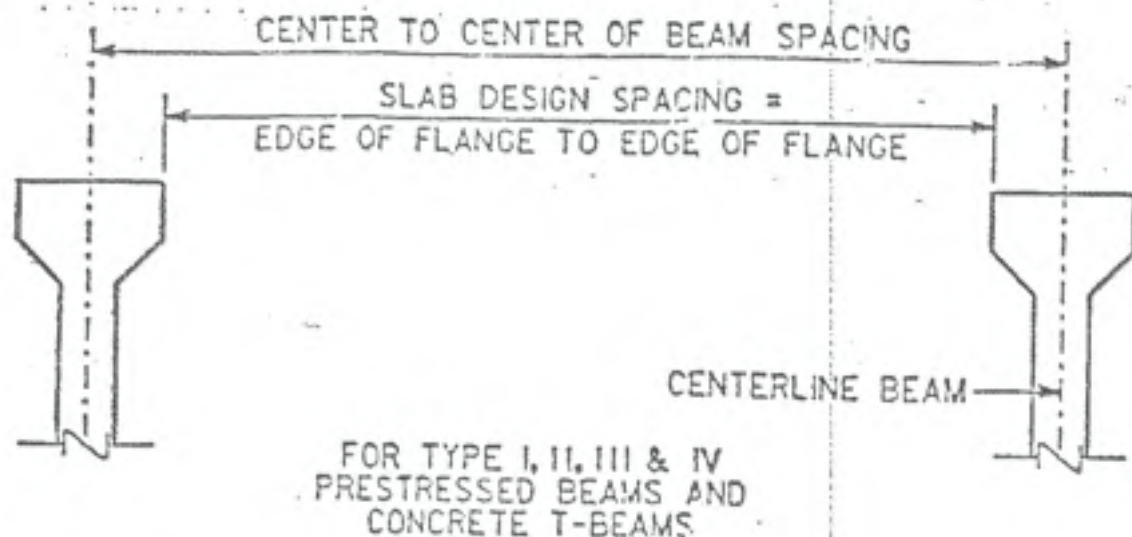
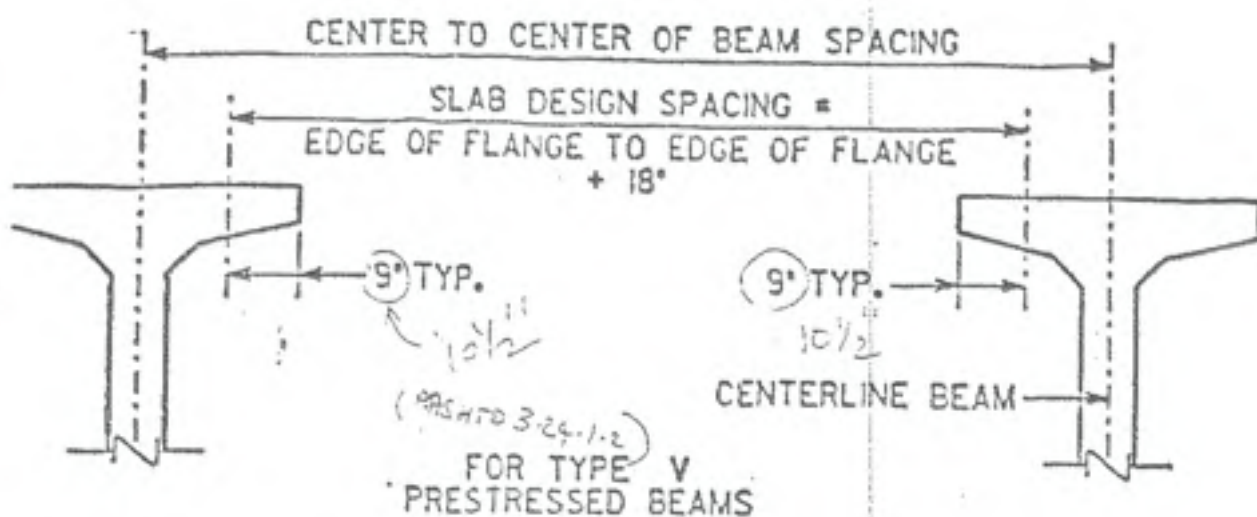


FIG. NO. 1 (cont'd)

CALCULATION COVER SHEET

PROJECT I-75 / I-575 NORTHWEST CORRIDOR	JOB NO. NH000-0073-03(242)	CALC NO. BR#33	SHEET 1
SUBJECT Beam Design Input		DISCIPLINE STRUCTURAL	

CALCULATION STATUS DESIGNATION	PRELIMINARY <input type="checkbox"/>	CONFIRMED <input type="checkbox"/>	SUPSEDED <input type="checkbox"/>	VOIDED <input type="checkbox"/>	INCOMPLETE <input checked="" type="checkbox"/>
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COMPUTER PROGRAM/TYPE	SCP <input checked="" type="radio"/> YES <input type="radio"/> NO	MAINFRAME <input type="radio"/>	PC <input checked="" type="radio"/>	PROGRAM Excel	VERSION/RELEASE NO. 2003
----------------------------------	--	--	--	----------------------	---------------------------------

Note 1: Georgia Department of Transportation (GDOT) terminated Contract Number TOURDPPI60072 for its convenience prior the completion of all work under that contract and directed that the work with respect to these calculations be discontinued.

(a) These calculations were not completed at the time of GDOT's direction and the information contained herein is not complete and/or has not been fully verified or checked. These calculations are a work-in-progress and are presented only as such.

(b) Any user is cautioned that the use of these calculations and any related information or calculations, without access to factors and without proper regard for their purpose, could lead to erroneous conclusions.

(c) If any such calculations or any information contained herein is used in future work efforts or any follow on design work activity, a complete confirmation of the information contained herein should be performed prior to any such use.

(d) GTP has no responsibility for the use of this information not under its direct control.

Beam Design Input calculations are included for spans 1, 2 and 3.

A	As per GDOT's termination for convenience direction	7	7	JCR			11/30/09
NO.	REASON FOR REVISION	TOTAL NO. OF SHEETS	LAST SHEET NO.	BY	CHECKED	APPROVED/ ACCEPTED	DATE

RECORD OF REVISIONS

CALCULATION SHEET

PROJECT: I-75 / I-575 NORTHWEST CORRIDOR
JOB NUMBER NH000-0073-03(242)
CALC NO. BR#33

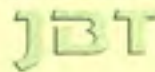
SUBJECT: Beam Design Input - Span 1
BY: JCR DATE: 11/30/2009

SHEET NO.
SHEET REV.

Sufficient sample calculations representative of the scope and conditions in the design calculation were performed and the results compared to demonstrate the computer program adequacy.

BRIDGE: I-75 over Frey Road
COUNTY: COBB
P.I. NO: 713640
PROJECT: NH000-0575-01(028)

J.B. TRIMBLE, INC.



JOB NO: 31-6036
DESIGNED BY: SHG
DATE: 10/16/2009

ps 11/4/09

SPAN 1

Beam Type:

D' DIMENSION = 9.125 IN
MIN. CORING DEPTH = 0.375 IN

AASHTO 8.10.1.1 - Compression Flange Width

WBM FLANGE = 12.00 in.
b = 8m Spacing = 86.00 in. CONTROLS
b = 1/4 Span Length = 268.00 in.
b = WBM FLANGE + 2[6 SLAB] = 105.00 in.

BRIDGE GEOMETRY INPUT:

LARGER BEAM SPACING 7.167 FT
SMALLER BEAM SPACING 7.167 FT
SKEW ANGLE 39.00 DEGREES

SLAB:

D' DIMENSION 9.125 IN
DESIGN SLAB DEPTH 7.750 IN
CORING WIDTH 1.000 FT
CORING DEPTH 0.875 IN
SLAB & CORING WEIGHT 6.766 KIP/FT
SIP FORMWORK 0.099 KIP/FT

DECK OVERLAY

AVERAGE THICKNESS 0.250 IN
DECK OVERLAY WEIGHT 6.822 KIP/FT
ROADWAY WIDTH 26.000 FT
FUTURE WEARING SURFACE 0.195 KIP/FT

UTILITIES

GAS MAIN (not added to W_{DL}) 0.00 KIP/FT
TELEPHONE CONDUITS (not added to W_{DL}) 0.00 KIP/FT
WATER MAIN 0.00 KIP/FT

EDGE BEAM:

DEPTH (from top of slab) 2.26 FT
WIDTH 1.000 FT
EDGE BM. WEIGHT 3.187 KIP

DIAPHRAGM:

Plate (3/8" X 5' X 2'-8") 0.017 KIP
CHANNEL (MC 18" X 42.7") 0.043 KIP/FT
DIAPH. WEIGHT 0.339 KIP

END WALL:

DEPTH (from top of slab) 5.010 FT
WIDTH 0.667 FT
PAVING NOTCH WIDTH 0.667 FT
AVG. PAVING NOTCH DEPTH 0.833 FT
END WALL WEIGHT 6.843 KIP

PARAPET:

SW, PARL, FENCE, & MEDIAN WEIGHT 1.900 KIP/FT
NUMBER OF BEAMS 4
PARAPET WEIGHT 0.475 KIP/FT

SIDEWALK LIVE LOAD:

SIDEWALK WIDTH 0 FT
SIDEWALK LOAD 0.060 KIP/FT²
NUMBER OF BEAMS 4
SIDEWALK LIVE LOAD PER BEAM 0.000 KIP/FT

SIMPLE SPAN PROGRAM INPUT:

LENGTH = 96.00 FT
Moment Dist. Factor (DFM) = 1.303
End Shear Dist. Factor (DFV) = 1.606
LL Deflection Dist. Factor (DFD) = 1.000
Non-Composite DL ($W_{DL,NC}$) = 0.826 KLF
Composite DL ($W_{DL,C}$) = 0.670 KLF W/ F.W.S.
Sidewalk LL (W_{walk}) = 0.000 KLF
Effective Concrete Width (W_e) = 86.000 IN
Concrete Slab Thickness (T_s) = 7.750 IN
Minimum Coring (DF) = 0.750 IN

P-LOADS:

XP1 0.00 FT
P1 6.843 K
XP2 10.500 FT
P2 0.339 K
XP3 35.500 FT
P3 0.339 K
XP4 60.500 FT
P4 0.339 K
XP5 85.500 FT
P5 0.339 K
XP6 96.000 FT
P6 3.187 K

DEAD LOAD CALCULATION:

SPAN LENGTH 96.00 FT
BEAM WEIGHT 0.295 KLF
TOTAL DL 1.701 KIP/FT
REACTION (K) 81.656
MOMENT (K-FT) 1959.749

P-LOADS:

TYPE	LOAD (K)	POSITION (FT)	REACTION (K)	MOMENT (K-FT)
END WALL:	6.843	0.00	6.843	0.000
DIAPHRAGM:	0.339	10.5000	0.302	3.169
DIAPHRAGM:	0.339	35.500	0.214	7.581
DIAPHRAGM:	0.339	60.5000	0.125	7.581
DIAPHRAGM:	0.339	85.5000	0.037	3.169
EDGE BEAM:	3.187	96.00	0.000	0.000

TOTAL DL: REACTION (K) 89.1 MOMENT (K-FT) 1978.1

LIVE LOAD CALCULATION:

BEAM DISTRIBUTION

MOMENT	1.303	WHEEL	VERIFY !!
0.652	AXLE		
SHEAR	1.606	WHEEL	VERIFY !!
0.802	AXLE		

IMPACT FACTOR

1.226
HS 20 LOADING: MIDSPAN: 5448 KIP-FT
MAX: 1452.1 KIP-FT

HS 20 REACTION:

TRUCK	65.00	KIP	57.85	KIP
LANE	56.72	KIP	50.12	KIP

TOTAL LL + I: REACTION (K) 57.8 MOMENT (K-FT) 1156.8
MAX TOTAL LL + I: 1160.1

TOTAL D.L. + L.L. = REACTION (K) 147.0 MOMENT (K-FT) 3134.9

DEFLECTIONS CALCULATION:

NO. LANES	2	FACTOR	1.000
NO. BEAMS	4		
REDUCTION FACTOR	1.00		

CALCULATION SHEET

PROJECT: I-75 / I-575 NORTHWEST CORRIDOR
JOB NUMBER NH000-0073-03(242)
CALC NO. BR#33

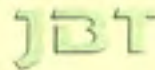
SUBJECT: Beam Design Input - Span 2
BY: JCR DATE: 11/30/2009

SHEET NO.
SHEET REV.

Sufficient sample calculations representative of the scope and conditions in the design calculation were performed and the results compared to demonstrate the computer program adequacy.

BRIDGE: I-75 over Frey Road
COUNTY: COBB
P.L. NO: 713640
PROJECT: NH000-0575-01(028)

J.B. TRIMBLE, INC.



JOB NO: 31-6036
DESIGNED BY: SHG
DATE: 10/16/2009

ASC
10/16/09

SPAN 2

Beam Type:

T₁ DIMENSION = 9.125 IN
MIN. COPING DEPTH = 0.375 IN

AASHTO 8.10.1.1 - Compression Flange Width

WBM FLANGE = 12.00 in.
b = Bm Spacing = 86.00 in. CONTROLS
b = 1/4 Span Length = 360.00 in.
b = WBM FLANGE + 2(5 ISLAB) = 105.00 in.

BRIDGE GEOMETRY INPUT:

LARGER BEAM SPACING 7.167 FT
SMALLER BEAM SPACING 7.167 FT
SKEW ANGLE 33.00 DEGREES

SLAB:

T₁ DIMENSION 9.125 IN
DESIGN SLAB DEPTH 7.750 IN
COPING WIDTH 1.000 FT
COPING DEPTH 0.875 IN
SLAB & COPING WEIGHT 0.706 KIP/FT
SP FORMWORK 0.099 KIP/FT

DECK OVERLAY

AVERAGE THICKNESS 0.250 IN
DECK OVERLAY WEIGHT 0.022 KIP/FT
ROADWAY WIDTH 26.000 FT
FUTURE WEARING SURFACE 0.195 KIP/FT

UTILITIES

GAS MAIN (not added to W_{DL}) 0.00 KIP/FT
TUPHON: CONDUITS (not added to W_{DL}) 0.00 KIP/FT
WATER MAIN 0.00 KIP/FT

EDGE BEAM:

DEPTH (from top of slab) 2.26 FT
WIDTH 1.000 FT
EDGE BM. WEIGHT 3.187 KIP

DIAPHRAGM:

Plate (3/8" X 5' X 2'-8") 0.017 KIP
CHANNEL (MC 18" X 42.7") 0.043 KIP/FT
DIAPHR. WEIGHT 0.339 KIP

PARAPET:

SW, PAR., FENCE, & MEDIAN WEIGHT 1.900 KIP/FT
NUMBER OF BEAMS 4
PARAPET WEIGHT 0.475 KIP/FT

SIDEWALK LIVE LOAD:

SIDEWALK WIDTH 0 FT
SIDEWALK LOAD 0.061 KIP/FT²
NUMBER OF BEAMS 4
SIDEWALK LIVE LOAD PER BEAM 0.000 KIP/FT

DEAD LOAD CALCULATION:

SPAN LENGTH 120.00 FT
BEAM WEIGHT 0.286 KLF
TOTAL DL 1.782 KIP/FT
P-LOADS:
TYPE LOAD (K) POSITION (FT)
EDGE BEAM 3.187 0.00
DIAPHRAGM 0.339 20.000
DIAPHRAGM 0.339 40.000
DIAPHRAGM 0.339 60.000
DIAPHRAGM 0.339 80.000
DIAPHRAGM 0.339 100.000
EDGE BEAM 3.187 120.00
REACTION (K) MOMENT (K-FT)
106.939 3206.157
TOTAL DL : 111.8 3247.7

LIVE LOAD CALCULATION:

BEAM DISTRIBUTION

MOMENT 1.303 WHEEL VERIFY III
0.652 AXLE
SHEAR 1.605 WHEEL VERIFY III
0.802 AXLE

IMPACT FACTOR

1.204
HS 20 LOADING: MDSPAN: 1980 KIP-FT
MAX: 1980.3 KIP-FT

HS 20 REACTION:

TRUCK LANE 66.40 KIP 57.80 KIP
64.40 KIP 55.24 KIP

REACTION (K) MOMENT (K-FT)
TOTAL LL + I: 57.9 1474.9
MAX TOTAL LL + I: 1477.4

REACTION (K) MOMENT (K-FT)
TOTAL D.L. + L.L. = 168.9 4722.6

DEFLECTIONS CALCULATION:

NO. LANES 2
NO. BEAMS 4
REDUCTION FACTOR 1.00 FACTOR 1.000

SIMPLE SPAN PROGRAM INPUT:

LENGTH = 120.00 FT
Moment Dist. Factor (DFM) = 1.303
End Shear Dist. Factor (DFV) = 1.605
LL Deflection Dist. Factor (DFD) = 1.000
Non- Composite DL (W_{DL}) = 0.826 KLF
Composite DL (W_{DL}) = 0.670 KLF W/ F.W.S.
Sidewalk LL (W_{DL}) = 0.000 KLF
Effective Concrete Width (W_e) = 86.00 IN
Concrete Slab Thickness (T_s) = 7.750 IN
Minimum Coping (D_f) = 0.750 IN
P-LOADS:
XP1 0.00 FT
P1 3.187 K
XP2 20.000 FT
P2 0.339 K
XP3 40.000 FT
P3 0.339 K
XP4 60.000 FT
P4 0.339 K
XP5 80.000 FT
P5 0.339 K
XP6 100.000 FT
P6 0.339 K
XP7 120.000 FT
P7 3.187 K

CALCULATION SHEET

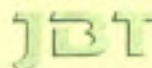
PROJECT: I-75 / I-575 NORTHWEST CORRIDOR
JOB NUMBER NH000-0073-03(242)
CALC NO. BR#33

SUBJECT: Beam Design Input - Span 3
BY: JCR DATE: 11/30/2009

SHEET NO.
SHEET REV.

Sufficient sample calculations representative of the scope and conditions in the design calculation were performed and the results compared to demonstrate the computer program adequacy.

JOB NO: 31-6036
DESIGNED BY: SHG
DATE: 10/16/2006



TV DIMENSION =	9.75	IN
MIN. COPING DEPTH =	0.375	IN

AASHTO 8.10.1.1 - Compression Flange Width		
wBM FLANGE =	12.00	in.
b = 8in Spacing =	82.00	in. CONTROLS
b = 1/4 Span Length =	319.50	in.
b = WBM FLANGE + 256 (SLAB) =	103.50	in.

SIDEWALK WIDTH	0	FT
SIDEWALK LOAD	0.064	KIP/FT ²
NUMBER OF BEAMS	4	
SIDEWALK LIVE LOAD PER BEAM	0.000	KIP/FT

REDUCTION FACTOR	1.00	FACTOR	1.000
------------------	------	--------	-------

XP1	0.00	F7
P1	8.834	K
XP2	12.260	F7
P2	0.326	K
XP3	33.260	F7
P3	0.326	K
XP4	53.260	F7
P4	0.326	K
XP6	73.260	F7
P6	0.326	K
XP6	93.260	F7
P6	0.326	K
XP7	106.800	F7
P7	3.267	K

CALCULATION COVER SHEET

PROJECT	JOB NO.	CALC NO.	SHEET
I-75 / I-575 NORTHWEST CORRIDOR	NH000-0073-03(242)	BR#33	1
SUBJECT	DISCIPLINE		
Beam Design Output	STRUCTURAL		

CALCULATION STATUS DESIGNATION	PRELIMINARY	CONFIRMED	SUPSEDED	VOIDED	INCOMPLETE
	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>

COMPUTER PROGRAM/TYPE	SCP	MAINFRAME	PC	PROGRAM	VERSION/RELEASE NO.
	<input checked="" type="radio"/> YES <input type="radio"/> NO	<input type="radio"/>	<input checked="" type="radio"/>	GDOT BRSPAN	06/26/2008

Note 1: Georgia Department of Transportation (GDOT) terminated Contract Number TOURDPP160072 for its convenience the completion of all work under that contract and directed that the work with respect to these calculations be discontinued.

(a) These calculations were not completed at the time of GDOT's direction and the information contained herein is not and/or has not been fully verified or checked. These calculations are a work-in-progress and are presented only as such.

(b) Any user is cautioned that the use of these calculations and any related information or calculations, without access to factors and without proper regard for their purpose, could lead to erroneous conclusions.

(c) If any such calculations or any information contained herein is used in future work efforts or any follow on design work a complete confirmation of the information contained herein should be performed prior to any such use.

(d) GTP has no responsibility for the use of this information not under its direct control.

Beam design output is included for spans 1, 2 and 3.

A	As per GDOT's termination for convenience direction	13	13	JCR			11/30/09
NO.	REASON FOR REVISION	TOTAL NO. OF SHEETS	LAST SHEET NO.	BY	CHECKED	APPROVED/ ACCEPTED	DATE
RECORD OF REVISIONS							

CALCULATION SHEET

PROJECT: I-75 / I-575 NORTHWEST CORRIDOR
JOB NUMBER NH000-0073-03(242)
CALC NO. BR#33

SUBJECT: Beam Design Output - Span 1
BY: JCR DATE: 11/30/2009

SHEET NO.
SHEET REV.

Sufficient sample calculations representative of the scope and conditions in the design calculation were performed and the results compared to demonstrate the computer program adequacy.

I-75 OVER STEVE FREY RD - SPAN 1

SPAN DATA

BEAM	D/A	L.L.C.	T L M	LENGTH	D.F.M.	D.F.V.	D.F.D.	NPL
CG	1	MS20	0 0 0	96.000	1.303	1.605	1.000	6

WDLNC	WDLG	SWLL	E	W BM	FS	FC	WG	TYPE STEEL
0.826	0.670	0.000	29.00	0.000	27.00	1.400	0.490	572

CONCENTRATED LOADS

X1	P1	X2	P2	X3	P3	X4	P4
0.000	6.843	10.500	0.339	35.500	0.339	60.500	0.339
85.500	0.339	96.000	3.187	0.000	0.000	0.000	0.000

BEAM DATA

ROLLED	SECTION PROPERTIES	PLATE GIRDER WEB	TOP FLANGE	BOTTOM FLANGE
BEAM	P NP I Y TOP Y BOT	D T	W T	W T
OWF 0 0 0	0.0 0.000 0.000	48.00 0.6250	12.00 0.7500	12.00 1.3750
OWF 0				

COMPOSITE SLAB

WIDTH	THICKNESS	COPING	SHEAR CAPACITY	ULTIMATE STRENGTH	N=ES/EC
86.000	7.750	0.000	12.38 K/ROW	25.21 KIPS EACH	9

BOTTOM COVER	PLATE	TOP COVER	PLATE	CONSTANT
X-BEGIN THICKNESS WIDTH LENGTH		X-BEGIN THICKNESS WIDTH LENGTH		W T
23.00 2.0000 12.00 50.00		0.00 0.0000 0.00 0.00		0 0

PLATE GIRDER PROPERTIES

WEB	TOP FLANGE	BOTTOM FLANGE	WEB AND FLANGES PROPERTIES
DEPTH THICK	WIDTH THICK	WIDTH THICK	AREA Y-TOP Y-BOTTOM I
48.00 0.6250	12.00 0.7500	12.00 1.3750	55.500 28.137 21.988 20530.0

WEB AND COVER PLATES

BOTTOM	COVER	PLATE	TOP	COVER	PLATE
X-BEGIN THICKNESS WIDTH LENGTH			X-BEGIN THICKNESS WIDTH LENGTH		
23.00 2.0000 12.00 50.00			0.00 0.7500 12.00 0.00		

WEB WITH COVER PLATES PROPERTIES

AREA	Y-TOP	Y-BOTTOM	I
63.000	30.792	19.958	23816.1

COMPOSITE SECTION PROPERTIES

N	WEB AND FLANGES				WEB AND PLATES					
	YTC	YTS	YBS	I	Q SLAB	YTC	YTS	YBS	I	Q SLAB
9	17.59	9.84	40.29	53410.5	1015.6	19.81	12.06	38.69	65096.4	1180.1
27	26.03	18.28	31.84	38162.3		28.78	21.03	29.72	45254.1	

NUMBER OF SHEAR CONNECTORS NEEDED TO PROVIDE FOR ULTIMATE STRENGTH 186

NUMBER OF LONGITUDINAL STIFFENERS NEEDED 0

TRANSVERSE STIFFENERS NOT REQUIRED

SIMPLE SPAN OUTPUT DATA PROBLEM NUMBER S2NW

SP	GIRDER	P-LOAD	MOMENTS (K-FT.) AT SPAN 1/20 POINTS				LIVE LOAD	RR-I
			NON-C.	TOT.NC	COMP.	SIDEWK		
1	44.4	3.3	180.8	228.4	146.6	0.0	235.5 T	0.0
2	84.4	6.5	342.6	433.5	277.9	0.0	443.3 T	0.0
3	120.1	8.4	485.3	613.9	393.6	0.0	623.5 T	0.0
4	151.5	10.1	609.0	770.5	494.0	0.0	776.1 T	0.0
5	178.5	11.7	713.7	903.8	578.9	0.0	901.2 T	0.0
6	200.7	13.3	799.3	1013.3	648.3	0.0	998.6 T	0.0
7	218.0	14.9	865.9	1098.8	702.4	0.0	1072.8 T	0.0
8	230.3	15.6	913.5	1159.4	741.0	0.0	1128.4 T	0.0
9	237.7	15.6	942.0	1195.4	764.1	0.0	1156.4 T	0.0
10	240.2	15.6	951.6	1207.4	771.8	0.0	1156.8 T	0.0

STRESS (PSI) AT SPAN 1/20 POINTS

SP	MINIMUM STRESS		MAXIMUM STRESS			ALLOWABLE FS	R FACTOR	
	TOP-S	BOT-S	TOP-C	TOP-S	BOT-S		TOP-S	BOT-S
1	4600	-4404	147	5120	-6535	27000	0.898	0.674
2	8727	-8353	278	9706	-12366	27000	0.899	0.676
3	12358	-11831	393	13737	-17474	27000	0.900	0.677
4	15512	-14849	490	17228	-21874	27000	0.900	0.679
5	17251	-13650	529	19254	-20078	27000	0.896	0.680
6	19337	-15299	588	21557	-22421	27000	0.897	0.682
7	20965	-16585	633	23350	-24236	27000	0.898	0.684
8	22120	-17498	667	24629	-25546	27000	0.898	0.685
9	22807	-18042	685	25378	-26290	27000	0.899	0.686
10	23036	-18223	687	25608	-26474	27000	0.900	0.688

SHEARS (KIPS) AT SPAN 1/20 POINTS

S2NW

[illegible]

DEAD LOAD DEFLECTIONS (INCHES)						SHEAR	
SP	GIRDER	P-LOAD	NON-C.	TOT.NC	COMP.	RANGE (KIPS)	CON.SPAC (IN)
0	0.000	0.000	0.000	0.000	0.000	57.9	11.25
1	0.095	0.006	0.381	0.483	0.164	50.6	12.87
2	0.188	0.013	0.750	0.950	0.322	49.8	13.08
3	0.275	0.019	1.096	1.389	0.471	49.1	13.26
4	0.353	0.024	1.409	1.787	0.605	48.4	13.45
5	0.422	0.028	1.682	2.133	0.722	48.0	14.23
6	0.480	0.032	1.912	2.425	0.820	48.0	14.23
7	0.526	0.035	2.096	2.658	0.899	48.3	14.15
8	0.560	0.038	2.230	2.828	0.956	48.5	14.08
9	0.581	0.039	2.312	2.932	0.991	48.7	14.03
10	0.588	0.039	2.339	2.967	1.002	48.7	14.02

LIVE LOAD DEFLECTIONS (INCHES)					
TRUCK	LANE	MILITARY	RAILROAD	SIDEWALK	L/ 800
0.724	0.601	0.506	0.000	0.000	1.440

CALCULATION SHEET

PROJECT: I-75 / I-575 NORTHWEST CORRIDOR
JOB NUMBER NH000-0073-03(242)
CALC NO. BR#33

SUBJECT: Beam Design Output - Span 2
BY: JCR DATE: 11/30/2009

SHEET NO.
SHEET REV.

Sufficient sample calculations representative of the scope and conditions in the design calculation were performed and the results compared to demonstrate the computer program adequacy.

SIMPLE SPAN
 REVISED: JUNE 26, 2008

I-75 OVER STEVE FREY RD - SPAN 2

PSC
 11/4/09

SPAN DATA

BEAM	D/A	L.L.C.	T L M	LENGTH	D.F.M.	D.F.V.	D.F.D.	NPL
CG	1	HS20	0 0 0	120.000	1.303	1.605	1.000	7

MDLNC	MDLC	SWLL	E	W BM	FS	PC	WG	TYPE STEEL
0.826	0.670	0.000	29.00	0.000	27.00	1.400	0.490	572

CONCENTRATED LOADS

X1	P1	X2	P2	X3	P3	X4	P4
0.000	3.187	20.000	0.339	40.000	0.339	60.000	0.339
80.000	0.339	100.000	0.339	120.000	3.187	0.000	0.000

BEAM DATA

ROLLED	SECTION PROPERTIES				PLATE GIRDER WEB		TOP FLANGE		BOTTOM FLANGE			
BEAM	P	NP	I	Y TOP	Y BOT	D	T	W	T	W	T	
OWF	0	0	0	0.0	0.000	0.000	48.00	0.6250	13.50	1.3750	18.50	1.3750
OWF	0											

COMPOSITE SLAB

WIDTH	THICKNESS	COPING	SHEAR CAPACITY		ULTIMATE STRENGTH		N=ES/EC	
86.000	7.750	0.000	12.38	K/ROW	25.21	KIPS EACH		9

BOTTOM COVER PLATE				TOP COVER PLATE				CONSTANT	
X-BEGIN	THICKNESS	WIDTH	LENGTH	X-BEGIN	THICKNESS	WIDTH	LENGTH	W	T
30.00	2.0000	18.50	60.00	30.00	2.0000	13.50	60.00	0	0

PLATE GIRDER PROPERTIES

WEB		TOP FLANGE		BOTTOM FLANGE		WEB AND FLANGES PROPERTIES			
DEPTH	THICK	WIDTH	THICK	WIDTH	THICK	AREA	Y-TOP	Y-BOTTOM	I
48.00	0.6250	13.50	1.3750	18.50	1.3750	74.000	27.669	23.081	32194.4

WEB AND COVER PLATES

BOTTOM COVER PLATE				TOP COVER PLATE			
X-BEGIN	THICKNESS	WIDTH	LENGTH	X-BEGIN	THICKNESS	WIDTH	LENGTH
30.00	2.0000	18.50	60.00	30.00	2.0000	13.50	60.00

WEB WITH COVER PLATES PROPERTIES

AREA	Y-TOP	Y-BOTTOM	I
94.000	28.660	23.340	45116.4

COMPOSITE SECTION PROPERTIES

WEB AND FLANGES					WEB AND PLATES					
N	YTC	YTS	YBS	I	Q SLAB	YTC	YTS	YBS	I	Q SLAB
9	19.95	11.58	39.17	70867.8	1190.7	22.07	14.32	37.68	89332.4	1347.7
27	28.00	19.62	31.13	51472.9		29.64	21.89	30.11	65934.6	

NUMBER OF SHEAR CONNECTORS NEEDED TO PROVIDE FOR ULTIMATE STRENGTH 186

NUMBER OF LONGITUDINAL STIFFENERS NEEDED 0

TRANSVERSE STIFFENERS NOT REQUIRED

SIMPLE SPAN OUTPUT DATA PROBLEM NUMBER S2NW

SP	GIRDER	P-LOAD	MOMENTS (K-FT.) AT SPAN 1/20 POINTS					RR-I
			NON-C.	TOT.NC	COMP.	SIDEWK	LIVE LOAD	
1	98.4	5.1	282.5	385.9	229.1	0.0	295.6 T	0.0
2	187.7	10.2	535.2	733.1	434.2	0.0	557.3 T	0.0
3	267.9	15.3	758.3	1041.4	615.1	0.0	785.1 T	0.0
4	339.1	19.0	951.6	1309.6	771.8	0.0	979.0 T	0.0
5	401.2	22.0	1115.1	1538.3	904.5	0.0	1139.0 T	0.0
6	453.0	25.1	1248.9	1727.0	1013.0	0.0	1265.2 T	0.0
7	493.3	27.5	1353.0	1873.8	1097.5	0.0	1361.8 T	0.0
8	522.1	28.5	1427.3	1977.9	1157.8	0.0	1433.4 T	0.0
9	539.4	29.5	1471.9	2040.8	1193.9	0.0	1471.0 T	0.0
10	545.1	30.5	1486.8	2062.4	1206.0	0.0	1474.8 T	0.0

STRESS (PSI) AT SPAN 1/20 POINTS

SP	MINIMUM STRESS		MAXIMUM STRESS			ALLOWABLE FS	R FACTOR	
	TOP-S	BOT-S	TOP-C	TOP-S	BOT-S		TOP-S	BOT-S
1	5028	-4983	166	5607	-6943	27000	0.897	0.718
2	9546	-9457	314	10639	-13154	27000	0.897	0.719
3	13553	-13423	443	15093	-18630	27000	0.898	0.720
4	17036	-16868	554	18956	-23361	27000	0.899	0.722
5	15330	-14506	555	17521	-20271	27000	0.875	0.716
6	17201	-16272	619	19635	-22675	27000	0.876	0.718
7	18656	-17645	667	21276	-24538	27000	0.877	0.719
8	19690	-18622	703	22447	-25877	27000	0.877	0.720
9	20313	-19211	723	23144	-26656	27000	0.878	0.721
10	20526	-19411	726	23364	-26876	27000	0.879	0.722

SHEARS (KIPS) AT SPAN 1/20 POINTS

S2NW

SP	GIRDER	P-LOAD	NON-C.	TOT.NC	COMP.	SIDEWK	LIVE LOAD	RR-I
0	17.2	4.0	49.6	70.7	40.2	0.0	57.9 T	0.0
1	15.6	0.8	44.6	61.1	36.2	0.0	49.5 T	0.0
2	14.1	0.8	39.6	54.6	32.2	0.0	46.8 T	0.0
3	12.6	0.8	34.7	48.2	28.1	0.0	44.2 T	0.0
4	11.1	0.5	29.7	41.4	24.1	0.0	41.5 T	0.0
5	9.6	0.5	24.8	34.9	20.1	0.0	38.9 T	0.0
6	7.7	0.5	19.8	28.0	16.1	0.0	36.2 T	0.0
7	5.8	0.2	14.9	20.8	12.1	0.0	33.5 T	0.0
8	3.8	0.2	9.9	13.9	8.0	0.0	30.7 T	0.0
9	1.9	0.2	5.0	7.0	4.0	0.0	27.9 T	0.0
10	0.0	0.2	0.0	0.2	0.0	0.0	25.2 T	0.0

DEAD LOAD DEFLECTIONS (INCHES)						SHEAR	
SP	GIRDER	P-LOAD	NON-C.	TOT.NC	COMP.	RANGE (KIPS)	CON.SPAC (IN)
0	0.000	0.000	0.000	0.000	0.000	57.9	12.72
1	0.190	0.010	0.525	0.725	0.282	50.8	14.50
2	0.373	0.021	1.032	1.425	0.555	50.2	14.67
3	0.543	0.030	1.503	2.077	0.810	49.6	14.85
4	0.696	0.038	1.924	2.659	1.039	49.2	14.97
5	0.826	0.046	2.282	3.154	1.236	49.4	16.62
6	0.935	0.052	2.580	3.567	1.401	49.7	16.50
7	1.022	0.056	2.819	3.898	1.533	50.0	16.40
8	1.086	0.060	2.994	4.140	1.630	50.2	16.35
9	1.126	0.062	3.101	4.288	1.689	50.3	16.32
10	1.139	0.063	3.138	4.340	1.709	50.3	16.31

LIVE LOAD DEFLECTIONS (INCHES)					
TRUCK	LANE	MILITARY	RAILROAD	SIDEWALK	L/ 800
1.037	0.992	0.713	0.000	0.000	1.800

CALCULATION SHEET

PROJECT: I-75 / I-575 NORTHWEST CORRIDOR
JOB NUMBER NH000-0073-03(242)
CALC NO. BR#33

SUBJECT: Beam Design Output - Span 3
BY: JCR DATE: 11/30/2009

SHEET NO.
SHEET REV.

Sufficient sample calculations representative of the scope and conditions in the design calculation were performed and the results compared to demonstrate the computer program adequacy.

16-OCT-09 GEORGIA DEPARTMENT OF TRANSPORTATION PROB. NO. S2NW
 13:23:21 PRECONSTRUCTION DIVISION - OFFICE OF BRIDGE & STRUCTURAL DESIGN
 SIMPLE SPAN
 REVISED: JUNE 26, 2008

I-75 OVER STEVE FREY RD - SPAN 3

SPAN DATA

BEAM	D/A	L.L.C.	T L M	LENGTH	D.F.M.	D.F.V.	D.F.D.	NPL
CG	1	MS20	0 0 0	106.500	1.242	1.537	1.000	7

WDLNC	WDLG	SWLL	E	W BM	FS	FC	WG	TYPE STEEL
0.782	0.670	0.000	29.00	0.000	27.00	1.400	0.490	572

CONCENTRATED LOADS

X1	P1	X2	P2	X3	P3	X4	P4
0.000	6.834	13.250	0.325	33.250	0.325	53.250	0.325
73.250	0.325	93.250	0.325	106.500	3.267	0.000	0.000

BEAM DATA

ROLLED	SECTION PROPERTIES				PLATE GIRDER WEB		TOP FLANGE		BOTTOM FLANGE		
BEAM	P	NP	I	Y TOP	Y BOT	D	T	W	T	W	T
OWF 0 0 0	0.0	0.000	0.000	48.00	0.6250	12.00	1.0000	14.00	1.3750		
OWF 0											

COMPOSITE SLAB

WIDTH	THICKNESS	COPING	SHEAR CAPACITY		ULTIMATE STRENGTH		N=ES/EC	
82.000	7.375	0.000	12.38	K/ROW	25.21	KIPS EACH		9

BOTTOM COVER PLATE				TOP COVER PLATE				CONSTANT	
X-BEGIN	THICKNESS	WIDTH	LENGTH	X-BEGIN	THICKNESS	WIDTH	LENGTH	W	T
25.75	2.0000	14.00	55.00	25.75	1.5000	12.00	55.00	0	0

PLATE GIRDER PROPERTIES

WEB		TOP FLANGE		BOTTOM FLANGE		WEB AND FLANGES PROPERTIES			
DEPTH	THICK	WIDTH	THICK	WIDTH	THICK	AREA	Y-TOP	Y-BOTTOM	I
48.00	0.6250	12.00	1.0000	14.00	1.3750	61.250	27.959	22.416	24163.1

WEB AND COVER PLATES

BOTTOM COVER PLATE				TOP COVER PLATE			
X-BEGIN	THICKNESS	WIDTH	LENGTH	X-BEGIN	THICKNESS	WIDTH	LENGTH
25.75	2.0000	14.00	55.00	25.75	1.5000	12.00	55.00

WEB WITH COVER PLATES PROPERTIES

AREA	Y-TOP	Y-BOTTOM	I
76.000	28.849	22.651	33446.6

COMPOSITE SECTION PROPERTIES

N	WEB AND FLANGES					WEB AND PLATES				
	YTC	YTS	YBS	I	Q SLAB	YTC	YTS	YBS	I	Q SLAB
9	19.02	11.14	39.23	57580.0	1030.0	20.96	13.58	37.92	71504.4	1160.3
27	27.23	19.35	31.02	41213.0		28.82	21.44	30.06	51861.6	

NUMBER OF SHEAR CONNECTORS NEEDED TO PROVIDE FOR ULTIMATE STRENGTH 168

NUMBER OF LONGITUDINAL STIFFENERS NEEDED 0

TRANSVERSE STIFFENERS NOT REQUIRED

SIMPLE SPAN OUTPUT DATA PROBLEM NUMBER S2NW

SP	GIRDER	P-LOAD	MOMENTS (K-FT.) AT SPAN 1/20 POINTS				LIVE LOAD	RR-I
			NON-C.	TOT.NC	COMP.	SIDEWK		
1	63.5	4.3	210.7	278.5	180.5	0.0	249.7 T	0.0
2	121.1	8.7	399.1	528.9	342.0	0.0	470.4 T	0.0
3	172.8	12.1	565.4	750.3	484.5	0.0	662.1 T	0.0
4	218.5	14.7	709.6	942.8	607.9	0.0	825.0 T	0.0
5	258.4	17.3	831.5	1107.2	712.4	0.0	958.8 T	0.0
6	291.3	19.9	931.3	1242.5	797.9	0.0	1063.7 T	0.0
7	317.0	21.2	1008.9	1347.1	864.4	0.0	1143.9 T	0.0
8	335.3	22.0	1064.4	1421.7	911.9	0.0	1203.6 T	0.0
9	346.3	22.9	1097.6	1466.9	940.4	0.0	1234.4 T	0.0
10	350.0	23.8	1108.7	1482.5	949.9	0.0	1236.1 T	0.0

STRESS (PSI) AT SPAN 1/20 POINTS

SP	MINIMUM STRESS		MAXIMUM STRESS			ALLOWABLE FS	R FACTOR	
	TOP-S	BOT-S	TOP-C	TOP-S	BOT-S		TOP-S	BOT-S
1	4883	-4730	162	5463	-6771	27000	0.894	0.699
2	9270	-8976	307	10362	-12822	27000	0.895	0.700
3	13147	-12728	433	14684	-18142	27000	0.895	0.702
4	16516	-15987	541	18431	-22732	27000	0.896	0.703
5	14994	-13952	550	17179	-20054	27000	0.873	0.696
6	16819	-15647	612	19244	-22416	27000	0.874	0.698
7	18231	-16959	660	20839	-24239	27000	0.875	0.700
8	19239	-17896	695	21983	-25555	27000	0.875	0.700
9	19848	-18461	714	22661	-26316	27000	0.876	0.702
10	20057	-18654	717	22874	-26520	27000	0.877	0.703

SHEARS (KIPS) AT SPAN 1/20 POINTS

S2NW

SP	GIRDER	P-LOAD	NON-C.	TOT.NC	COMP.	SIDEWK	LIVE LOAD	RR-I
0	12.5	7.6	41.6	61.8	35.7	0.0	55.3 T	0.0
1	11.4	0.8	37.5	49.7	32.1	0.0	47.1 T	0.0
2	10.3	0.8	33.3	44.4	28.5	0.0	44.5 T	0.0
3	9.1	0.5	29.1	38.8	25.0	0.0	42.0 T	0.0
4	8.0	0.5	25.0	33.5	21.4	0.0	39.4 T	0.0
5	6.9	0.5	20.8	28.2	17.8	0.0	36.8 T	0.0
6	5.5	0.5	16.7	22.7	14.3	0.0	34.2 T	0.0
7	4.1	0.2	12.5	16.8	10.7	0.0	31.6 T	0.0
8	2.8	0.2	8.3	11.2	7.1	0.0	29.0 T	0.0
9	1.4	0.2	4.2	5.7	3.6	0.0	26.3 T	0.0
10	0.0	0.2	0.0	0.2	0.0	0.0	23.6 T	0.0

DEAD LOAD DEFLECTIONS (INCHES)						SHEAR	
SP	GIRDER	P-LOAD	NON-C.	TOT.NC	COMP.	RANGE (KIPS)	CON.SPAC (IN)
0	0.000	0.000	0.000	0.000	0.000	55.3	12.50
1	0.129	0.009	0.413	0.550	0.221	48.4	14.31
2	0.253	0.017	0.811	1.081	0.434	47.7	14.51
3	0.368	0.025	1.182	1.575	0.634	47.1	14.70
4	0.472	0.032	1.513	2.017	0.813	46.4	14.90
5	0.561	0.038	1.795	2.393	0.968	46.4	16.45
6	0.634	0.043	2.030	2.707	1.098	46.6	16.38
7	0.694	0.047	2.218	2.958	1.201	46.9	16.28
8	0.737	0.049	2.355	3.141	1.277	47.1	16.20
9	0.763	0.051	2.438	3.252	1.323	47.2	16.17
10	0.772	0.052	2.466	3.290	1.339	47.2	16.16

LIVE LOAD DEFLECTIONS (INCHES)					
TRUCK	LANE	MILITARY	RAILROAD	SIDEWALK	L/ 800
0.902	0.798	0.625	0.000	0.000	1.597

CALCULATION COVER SHEET

PROJECT	JOB NO.	CALC NO.	SHEET
I-75 / I-575 NORTHWEST CORRIDOR	NH000-0073-03(242)	BR#33	1
SUBJECT	DISCIPLINE		
Shear Stud Spacing Calculations	STRUCTURAL		

CALCULATION STATUS DESIGNATION	PRELIMINARY	CONFIRMED	SUPSEDED	VOIDED	INCOMPLETE
	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>

COMPUTER PROGRAM/TYPE	SCP <input checked="" type="radio"/> YES <input type="radio"/> NO	MAINFRAME <input type="radio"/>	PC <input checked="" type="radio"/>	PROGRAM Excel	VERSION/RELEASE NO. 2003
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Note 1: Georgia Department of Transportation (GDOT) terminated Contract Number TOURDPP160072 for its convenience prior to the completion of all work under that contract and directed that the work with respect to these calculations be discontinued.

(a) These calculations were not completed at the time of GDOT's direction and the information contained herein is not complete and/or has not been fully verified or checked. These calculations are a work-in-progress and are presented only as such.

(b) Any user is cautioned that the use of these calculations and any related information or calculations, without access to factors and without proper regard for their purpose, could lead to erroneous conclusions.

(c) If any such calculations or any information contained herein is used in future work efforts or any follow on design work activity, a complete confirmation of the information contained herein should be performed prior to any such use.

(d) GTP has no responsibility for the use of this information not under its direct control.

Design calculations for steel beam shear stud spacings are included for spans 1, 2, and 3.

A	As per GDOT's termination for convenience direction	10	10	JCR			11/30/09
NO.	REASON FOR REVISION	TOTAL NO. OF SHEETS	LAST SHEET NO.	BY	CHECKED	APPROVED/ ACCEPTED	DATE
RECORD OF REVISIONS							

CALCULATION SHEET

PROJECT: I-75 / I-575 NORTHWEST CORRIDOR
JOB NUMBER NH000-0073-03(242)
CALC NO. BR#33

SUBJECT: Shear Stud Spacing Calculations - Span 1
BY: JCR DATE: 11/30/2009

SHEET NO.
SHEET REV.

Sufficient sample calculations representative of the scope and conditions in the design calculation were performed and the results compared to demonstrate the computer program adequacy.

BRIDGE: I-75 over Frey Road
COUNTY: COBB
P.I. NO: 713640
PROJECT: NH000-0575-01(028)



J.B. TRIMBLE, INC.
JOB NO: 31-6036
DESIGNED BY: SHG
DATE: 10/14/2009

STUD SHEAR CONNECTORS

Beam Type Top Flange Width = 12"

Stud $\varnothing = 0.75"$

No. of Studs = 4

$Z_r = \alpha d^2$ (kips / studs)			
$\alpha \backslash d$ (in)	0.5	0.75	1
13000	3.25	7.31	13.00
10600	2.65	5.96	10.60
7850	1.96	4.42	7.85
5500	1.38	3.09	5.50

ADT (2001) = 1,000

ADT (2021) = 80,000

% TRUCKS = 4.4%

DIRECTIONAL = 100%

ADT (2031) = 119,500 in one direction

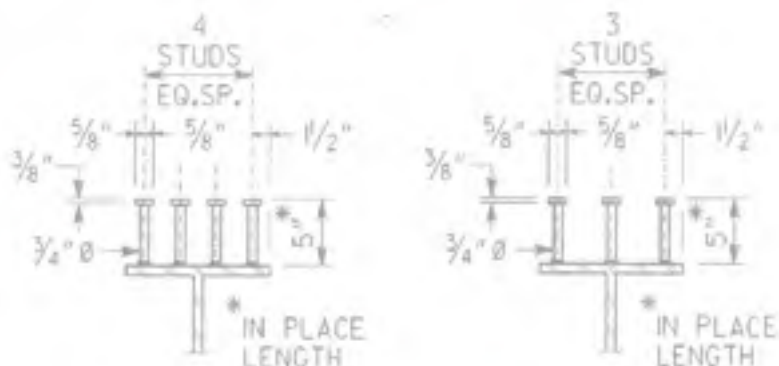
ADTT = 5,258 > 2500
USE 2,000,000 CYCLES

$Z_r = \alpha d^2$ (kips / row)			
Number of Studs : 3			
$\alpha \backslash d$ (in)	0.5	0.75	1
13000	9.75	21.94	39.00
10600	7.95	17.89	31.80
7850	5.89	13.25	23.55
5500	4.13	9.28	16.50

$Z_r = \alpha d^2$ (kips / row)			
Number of Studs : 4			
$\alpha \backslash d$	0.5	0.75	1
13000	13.00	29.25	52.00
10600	10.60	23.85	42.40
7850	7.85	17.66	31.40
5500	5.50	12.38	22.00

$E_c = 150^{1.5} 33 (f'_c)^{1.5}$ (AASHTO 10.38.5.1.2)

$S_u = 0.4 d^2 (f'_c E_c)^{1/2}$ (AASHTO)			
d (in)	f'_c (psi)	E_c (psi)	S_u (kips)
0.5	3000	3320561	9.98
0.75	3000	3320561	22.46
1	3000	3320561	39.92
0.5	3500	3586616	11.20
0.75	3500	3586616	25.21
1	3500	3586616	44.82



AASHTO 10.38.2.4 The clear distance between the edge of a girder flange and the edge of the shear connector shall be not less than 1". Adjacent stud shear connectors shall not be closer than 4 diameters center to center.

GDOT calls for 3/4" \varnothing studs and 1 1/2" clear from edge of girder flange to CL of stud. Therefore, 4 studs are only allowed for beams with a minimum flange width of 12"+/-.

Shear Capacity (Z_r) = 12.38 K/Row

Ultimate Strength (S_u) = 25.21 kips

BRIDGE: I-75 over Frey Road
COUNTY: COBB
P.I. NO: 713640
PROJECT: NH000-0575-01(028)



J.B. TRIMBLE, INC.
JOB NO: 31-6036
DESIGNED BY: SHG
DATE: 10/14/2009

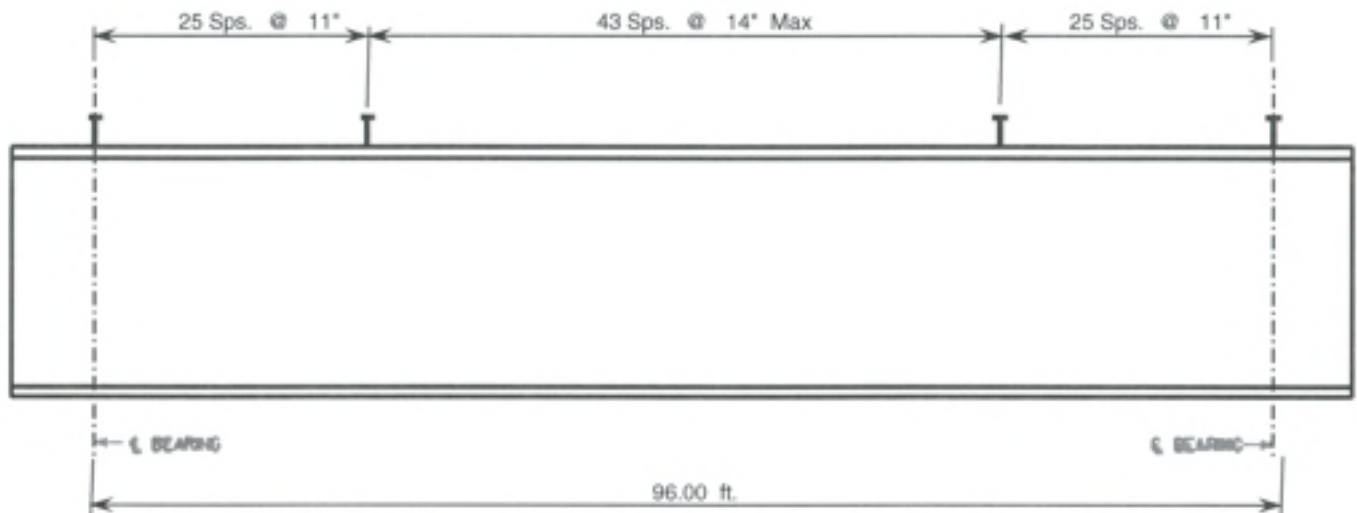
PJC 11/4/09

SHEAR STUD SPACING

Design Length = 96 ft.

Location (ft.)	s (in)
0.0	11.25
4.8	12.87
9.6	13.08
14.4	13.26
19.2	13.45
24.0	14.23
28.8	14.23
33.6	14.15
38.4	14.08
43.2	14.03
48.0	14.02

	Spacing 1	Spacing 2
Stud Spacing:	11 in.	14 in.



CALCULATION SHEET

PROJECT: I-75 / I-575 NORTHWEST CORRIDOR
JOB NUMBER NH000-0073-03(242)
CALC NO. BR#33

SUBJECT: Shear Stud Spacing Calculations - Span 2
BY: JCR DATE: 11/30/2009

SHEET NO.
SHEET REV.

Sufficient sample calculations representative of the scope and conditions in the design calculation were performed and the results compared to demonstrate the computer program adequacy.

BRIDGE: I-75 over Frey Road
COUNTY: COBB
P.I. NO: 713640
PROJECT: NH000-0575-01(028)



J.B. TRIMBLE, INC.
JOB NO: 31-6036
DESIGNED BY: SHG
DATE: 10/14/2009

STUD SHEAR CONNECTORS

Beam Type Top Flange Width = 13.5"

Stud $\varnothing = 0.75"$

No. of Studs = 4

$$Z_r = \alpha d^2 \text{ (kips / studs)}$$

$\alpha \backslash d \text{ (in)}$	0.5	0.75	1
13000	3.25	7.31	13.00
10600	2.65	5.96	10.60
7850	1.96	4.42	7.85
5500	1.38	3.09	5.50

ADT (2001) = 1,000

ADT (2021) = 80,000

% TRUCKS = 4.4%

DIRECTIONAL = 100%

ADT (2031) = 119,500 in one direction

ADTT = 5,258 > 2500
USE 2,000,000 CYCLES

$$Z_r = \alpha d^2 \text{ (kips / row)}$$

$$\text{Number of Studs : 3}$$

$\alpha \backslash d \text{ (in)}$	0.5	0.75	1
13000	9.75	21.94	39.00
10600	7.95	17.89	31.80
7850	5.89	13.25	23.55
5500	4.13	9.28	16.50

$$Z_r = \alpha d^2 \text{ (kips / row)}$$

$$\text{Number of Studs : 4}$$

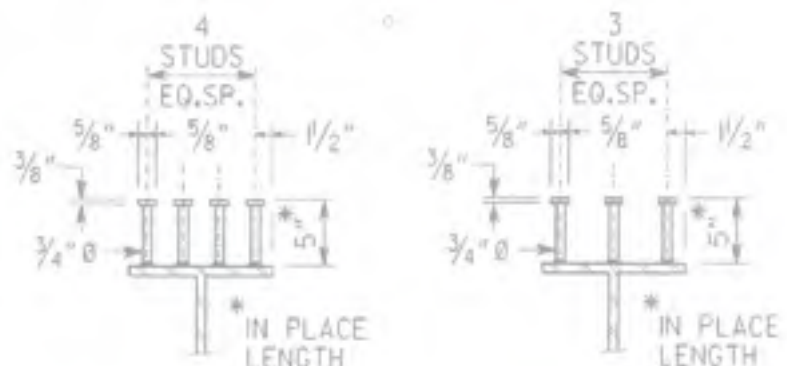
$\alpha \backslash d$	0.5	0.75	1
13000	13.00	29.25	52.00
10600	10.60	23.85	42.40
7850	7.85	17.66	31.40
5500	5.50	12.38	22.00

$E_c = 150^{1.5} 33 (f'_c)^{1/4}$ (AASHTO 10.38.5.1.2)

$$S_u = 0.4 d^2 (f'_c E_c)^{1/2}$$

$$\text{(AASHTO)}$$

$d \text{ (in)}$	$f'_c \text{ (psi)}$	$E_c \text{ (psi)}$	$S_u \text{ (kips)}$
0.5	3000	3320561	9.98
0.75	3000	3320561	22.46
1	3000	3320561	39.92
0.5	3500	3586616	11.20
0.75	3500	3586616	25.21
1	3500	3586616	44.82



AASHTO 10.38.2.4 The clear distance between the edge of a girder flange and the edge of the shear connector shall be not less than 1". Adjacent stud shear connectors shall not be closer than 4 diameters center to center.

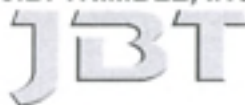
GDOT calls for 3/4" \varnothing studs and 1 1/2" clear from edge of girder flange to CL of stud. Therefore, 4 studs are only allowed for beams with a minimum flange width of 12"+/-.

Shear Capacity (Z_r) = 12.38 K/Row

Ultimate Strength (S_u) = 25.21 kips

BRIDGE: I-75 over Frey Road
 COUNTY: COBB
 P.I. NO: 713640
 PROJECT: NH000-0575-01(028)

J.B. TRIMBLE, INC.



J.B. TRIMBLE, INC.
 JOB NO: 31-6036
 DESIGNED BY: SHG
 DATE: 10/14/2009

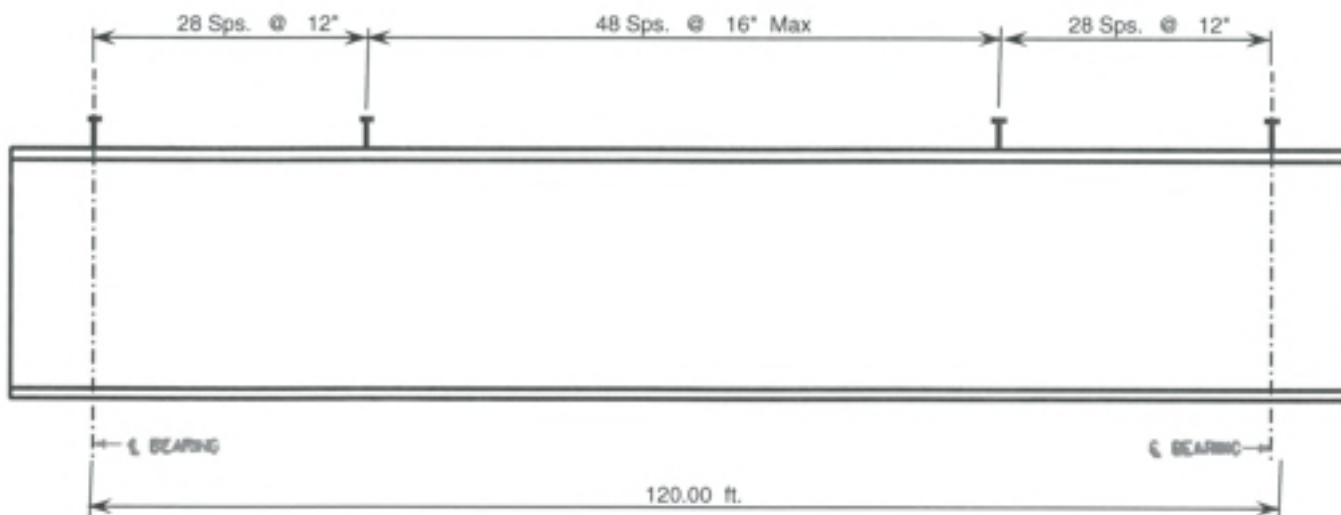
SHEAR STUD SPACING

Design Length = 120 ft.

PSC
11/4/09

Location (ft.)	s (in)
0.0	12.72
6.0	14.50
12.0	14.67
18.0	14.85
24.0	14.97
30.0	16.62
36.0	16.50
42.0	16.40
48.0	16.35
54.0	16.32
60.0	16.31

	Spacing 1	Spacing 2
Stud Spacing:	12 in.	16 in.



CALCULATION SHEET

PROJECT: I-75 / I-575 NORTHWEST CORRIDOR
JOB NUMBER NH000-0073-03(242)
CALC NO. BR#33

SUBJECT: Shear Stud Spacing Calculations - Span 3
BY: JCR DATE: 11/30/2009

SHEET NO.
SHEET REV.

Sufficient sample calculations representative of the scope and conditions in the design calculation were performed and the results compared to demonstrate the computer program adequacy.

BRIDGE: I-75 over Frey Road
COUNTY: COBB
P.I. NO: 713640
PROJECT: NH000-0575-01(028)



J.B. TRIMBLE, INC.
JOB NO: 31-6036
DESIGNED BY: SHG
DATE: 10/14/2009

STUD SHEAR CONNECTORS

Beam Type Top Flange Width = 12"

Stud $\varnothing = 0.75"$

No. of Studs = 4

$Z_r = \alpha d^2$ (kips / studs)			
$\alpha \backslash d$ (in)	0.5	0.75	1
13000	3.25	7.31	13.00
10600	2.65	5.96	10.60
7850	1.96	4.42	7.85
5500	1.38	3.09	5.50

ADT (2001) = 1,000

ADT (2021) = 80,000

% TRUCKS = 4.4%

DIRECTIONAL = 100%

ADT (2031) = 119,500 in one direction

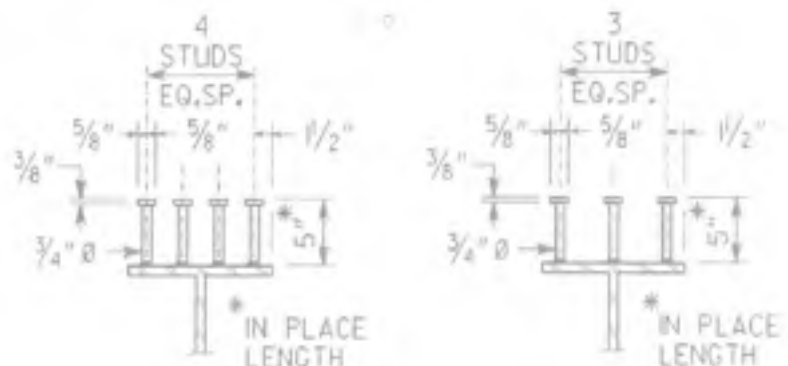
ADTT = 5,258 > 2500
USE 2,000,000 CYCLES

$Z_r = \alpha d^2$ (kips / row)			
Number of Studs : 3			
$\alpha \backslash d$ (in)	0.5	0.75	1
13000	9.75	21.94	39.00
10600	7.95	17.89	31.80
7850	5.89	13.25	23.55
5500	4.13	9.28	16.50

$Z_r = \alpha d^2$ (kips / row)			
Number of Studs : 4			
$\alpha \backslash d$	0.5	0.75	1
13000	13.00	29.25	52.00
10600	10.60	23.85	42.40
7850	7.85	17.66	31.40
5500	5.50	12.38	22.00

$E_c = 150^{1.5} 33 (f'_c)^{1/4}$ (AASHTO 10.38.5.1.2)

$S_u = 0.4 d^2 (f'_c E_c)^{1/2}$ (AASHTO)			
d (in)	f'_c (psi)	E_c (psi)	S_u (kips)
0.5	3000	3320561	9.98
0.75	3000	3320561	22.46
1	3000	3320561	39.92
0.5	3500	3586616	11.20
0.75	3500	3586616	25.21
1	3500	3586616	44.82



AASHTO 10.38.2.4 The clear distance between the edge of a girder flange and the edge of the shear connector shall be not less than 1". Adjacent stud shear connectors shall not be closer than 4 diameters center to center.

GDOT calls for 3/4" \varnothing studs and 1 1/2" clear from edge of girder flange to CL of stud. Therefore, 4 studs are only allowed for beams with a minimum flange width of 12" +/-.

Shear Capacity (Z_r) = 12.38 K/Row

Ultimate Strength (S_u) = 25.21 kips

BRIDGE: I-75 over Frey Road
COUNTY: COBB
P.I. NO: 713640
PROJECT: NH000-0575-01(028)



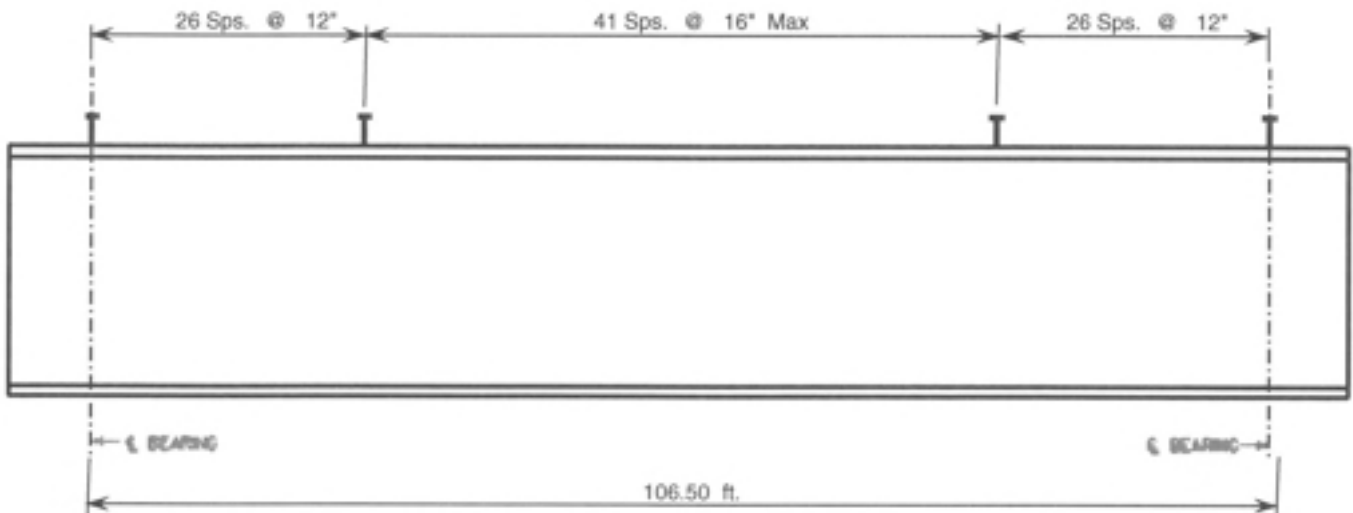
J.B. TRIMBLE, INC.
JOB NO: 31-6036
DESIGNED BY: SHG
DATE: 10/14/2009

SHEAR STUD SPACING

Design Length = 106.5 ft.

Location (ft.)	s (in)
0.0	12.50
5.3	14.31
10.7	14.51
16.0	14.70
21.3	14.90
26.6	16.45
32.0	16.38
37.3	16.28
42.6	16.20
47.9	16.17
53.3	16.16

	Spacing 1	Spacing 2
Stud Spacing:	12 in.	16 in.



CALCULATION COVER SHEET

PROJECT	JOB NO.	CALC NO.	SHEET
I-75 / I-575 NORTHWEST CORRIDOR	NH000-0073-03(242)	BR#33	1
SUBJECT	DISCIPLINE		
Bearing Design	STRUCTURAL		

CALCULATION STATUS DESIGNATION	PRELIMINARY	CONFIRMED	SUPSEDED	VOIDED	INCOMPLETE
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COMPUTER PROGRAM/TYPE	SCP	MAINFRAME	PC	PROGRAM	VERSION/RELEASE NO.
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Note 1: Georgia Department of Transportation (GDOT) terminated Contract Number TOURDPP160072 for its convenience prior to the completion of all work under that contract and directed that the work with respect to these calculations be discontinued.

(a) These calculations were not completed at the time of GDOT's direction and the information contained herein is not complete and/or has not been fully verified or checked. These calculations are a work-in-progress and are presented only as such.

(b) Any user is cautioned that the use of these calculations and any related information or calculations, without access to factors and without proper regard for their purpose, could lead to erroneous conclusions.

(c) If any such calculations or any information contained herein is used in future work efforts or any follow on design work activity, a complete confirmation of the information contained herein should be performed prior to any such use.

(d) GTP has no responsibility for the use of this information not under its direct control.

Bearing Design calculations are included for bearings at bents 1, 2, 3 and 4.

A	As per GDOT's termination for convenience direction	9	9	JCR			11/30/09
NO.	REASON FOR REVISION	TOTAL NO. OF SHEETS	LAST SHEET NO.	BY	CHECKED	APPROVED/ ACCEPTED	DATE
RECORD OF REVISIONS							

CALCULATION SHEET

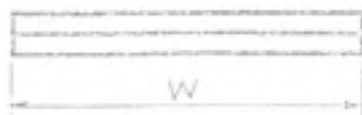
PROJECT: I-75 / I-575 NORTHWEST CORRIDOR
JOB NUMBER NH000-0073-03(242)
CALC NO. BR#33

SUBJECT: Bearing Design
BY: JCR DATE: 11/30/2009

SHEET NO.
SHEET REV.

Sufficient sample calculations representative of the scope and conditions in the design calculation were performed and the results compared to demonstrate the computer program adequacy.

SUGGESTED SHAPE AND SIZE OF SELF LUBRICATING BRONZE PLATES



SIZE AND MAXIMUM LOAD					
W	L	T	WITH SLOTS 2-3 X 1 ³ / ₁₆	WITH HOLES 2-1 ³ / ₁₆ Ø	PLAIN
10	7	1			140
10	8	1 ¹ / ₄			160
10	9	1 ¹ / ₂			180
10 ¹ / ₂	7	1			147
10 ¹ / ₂	8	1 ¹ / ₄			168
10 ¹ / ₂	9	1 ¹ / ₂			189
12	6	1	131	140	144
12	7	1	155	164	168
12	8	1 ¹ / ₂	179	188	192
12	9	1 ¹ / ₂			216

USE ONLY THOSE PLATES WHICH HAVE A MAXIMUM LOAD SHOWN

PURPOSE: To standardize plate sizes within the office so that plates may be stocked by suppliers, thus making them more economical.

DESIGN SPECIFICATION: Bronze plates shall conform to ASTM Designation B 22 Alloy B and supplemental specifications and shall have an allowable unit stress of 2000 psi in compression.

LIMITATIONS: Sliding plate type bearings shall not be used where the anticipated total movement (expansion plus contraction) exceeds 3 inches for assemblies without anchor bolts through the flanges and 2 inches for assemblies with anchor bolts through the flanges.

When the gradient of the girder at the bearing exceeds 4.0%, the top of the upper plate (sole plate) shall be beveled to match the girder gradient.

COEFFICIENT OF FRICTION: For design purposes a value of 0.10 shall be used.

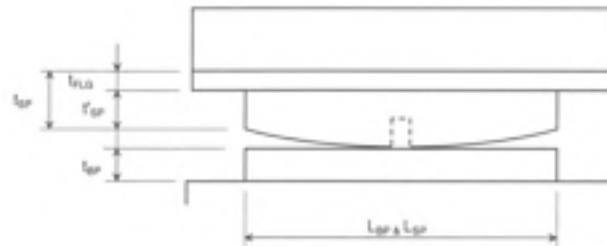
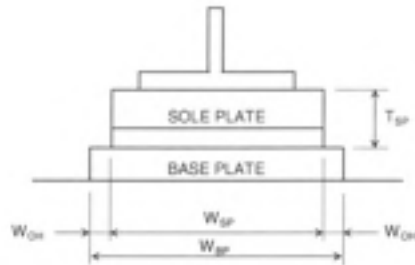
NOTE: Width of LBS B is to be 2" less than width of SLE B.

BRIDGE: I-75 over Frey Road
COUNTY: COBB
P.I. NO: 713640
PROJECT: NH000-0575-01(028)

J.B. TRIMBLE, INC.



JOB NO: 31-6036
DESIGNED BY: SHG
DATE: 10/31/2009



BENTS 1

FIXED BEARING CALCULATIONS

GENERAL INPUT:

Beam Type	Plate Girder	
R (Reaction) =	147.0 Kips	
Bottom Flange Thickness, t_{FLG} =	1.375 in	35 mm
W_{SP} =	12.00 in	305 mm
W_{BP} =	12.00 in	305 mm
L_{SP} =	11.75 in	298 mm
F_c =	3500 psi	
$F_b = 0.3F_c$ =	1,050 ksi	
AASHTO Art. 8.15.2.1.3		

SOLE PLATE:

$$M=RL/8$$

$$S=wt^2/6$$

$$I_p=MS$$

F_y =	36000 psi	AASHTO Table 10.2B
$F_{yb} = .55F_y$ =	19.8 ksi	AASHTO 10.32.1A
$t_{SP} = [3/4(RW_{SP})/(L_{SP}F_{yb})]^{1/3}$ =	2.38 in.	
$t'_{SP} = t_{SP} - t_{FLG}$ =	1.01	26 mm
Rad (Radius) =	18.00 in	
$= t'_{SP} + Rad \cdot [Rad^2 - (1/2 L_{SP})^2]^{1/2}$ =	2.00 in -----> use =	51 mm

BASE (MASONRY) PLATE: $M=(RW)(W/2)(W/4)=RW/8$

$$S_x=W_{SP}T_{BP}^2/6$$

$$I_p=MS$$

$L_{BP} = R/(W_{BP}F_b)$ =	11.67 in -----> use =	11.75	in	298 mm
$t_{BP} = [3/4(RL_{BP})/(W_{BP}F_{yb})]^{1/3}$ =	2.33 in -----> use =	2.50	in	64 mm

ALLOWABLE BEARING ON CONCRETE:

$$f_b = R/(L_{BP} \cdot W_{BP}) = 1.042 \text{ ksi} \quad f_b < F_b \rightarrow \text{OK}$$

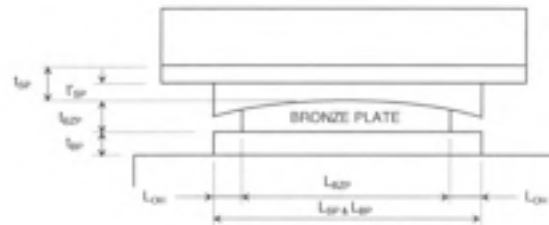
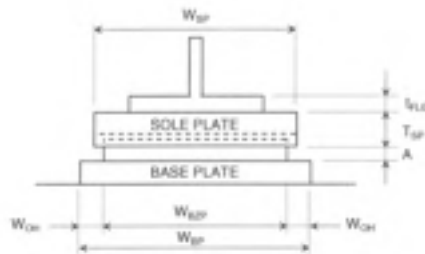
BASE PLATE			SOLE PLATE			BEARING DEPTH
WIDTH	LENGTH	HEIGHT	WIDTH	LENGTH	HEIGHT	
12"	11.75"	2.5"	12"	11.75"	2"	4.5"

BRIDGE: I-75 over Frey Road
COUNTY: COBB
P.I. NO: 713640
PROJECT: NH000-0575-01(028)

J.B. TRIMBLE, INC.



JOB NO: 31-6036
DESIGNED BY: SHG
DATE: 10/31/2009



EXPANSION BEARING CALCULATIONS

BENT 2 BK

GENERAL INPUT:

Beam Type	Plate Girder	
R (Reaction) =	147.0	Kips
Bottom Flange Thick, t_{FLG} =	1.375	in
W_{SP} =	12.00	in
W_{BP} =	12.00	in
W_{GP} =	12.00	in
L_{SP} =	9.00	in
L_{BP} =	12.00	in
		35 mm
		305 mm
		305 mm
		305 mm
		229 mm
		305 mm

ALLOWABLE BEARING ON CONCRETE:

f'_c =	3500	psi
$F_b = 0.3f'_c$ =	1.050	ksi
$f_b = R/(L_{BP} * W_{GP})$ =	1.021	ksi
		fb < Fb → OK

BRONZE PLATE WIDTH (W_{BP}):

TYPE = SELF LUBRICATING ASTM B22 ALLOY 911				
BEARING CAPACITY =	2000	psi		
L_{BP} =	6.12	in	use =	7.0 in 178 mm

BASE (MASONRY) PLATE:

Max of W_{CH} or L_{CH} =	2.50	in
$M = wL^2/2 = t_b \text{ Max}(W_{CH} \text{ or } L_{CH})^2/2$ =	3.19	K-in
F_y =	36000	psi
$F_{yb} = .55F_y$ =	19.8	ksi
$t_{BP} = [6M/F_{yb}]^{1/3}$ =	0.98	in
		use = 1.00 in 25 mm
		AASHTO Table 10.2B
		AASHTO 10.32.1A

SOLE PLATE:

$t_{SP} = [3/4(RW_{SP})/(L_{SP}F_{yb})]^{1/3}$ =	2.72	in
$t'_{SP} = t_{SP} - t_{FLG}$ =	1.35	in
		use = 1.50 in
Rad (Radius) =	18.00	in
$T_{SP} = t'_{SP} + \text{Rad} \cdot [\text{Rad}^2 - (1/2 L_{BP})^2]^{1/2}$ =	1.84	in
		use = 2.00 in

BRONZE PLATE THICKNESS (t_{BP}):

A =	0.50	in
$t_{BP} = (T_{SP} - t'_{SP}) + A$ =	1.00	in
		use = 1.00 in 25 mm

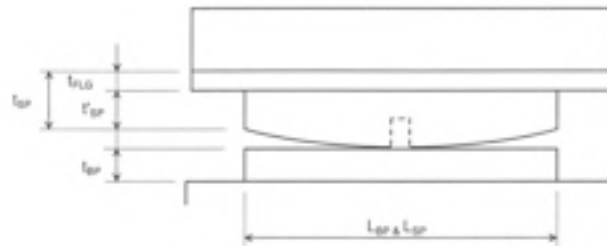
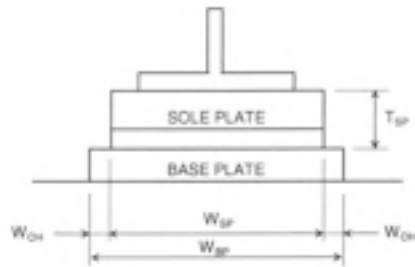
BASE PLATE			SOLE PLATE			BRONZE PLATE			BEARING DEPTH
WIDTH	LENGTH	HEIGHT	WIDTH	LENGTH	HEIGHT	WIDTH	LENGTH	HEIGHT	
12"	12"	1"	12"	9"	1.5"	12"	7"	1"	3.5"

BRIDGE: I-75 over Frey Road
COUNTY: COBB
P.I. NO: 713640
PROJECT: NH000-0575-01(028)

J.B. TRIMBLE, INC.



JOB NO: 31-6036
DESIGNED BY: SHG
DATE: 10/31/2009



BENTS 2 AH

FIXED BEARING CALCULATIONS

GENERAL INPUT:

Beam Type	Plate Girder	
R (Reaction) =	168.9 Kips	
Bottom Flange Thickness, t_{FLG} =	1.375 in	35 mm
W_{SP} =	18.50 in	470 mm
W_{BP} =	18.50 in	470 mm
L_{SP} =	8.75 in	222 mm
F_c =	3500 psi	
$F_b = 0.3F_c$ =	1.050 ksi	
AASHTO Art. 8.15.2.1.3		

SOLE PLATE:

$M=RL/8$

$S=wt^3/6$

$t_p=MS$

F_y =	36000 psi	AASHTO Table 10.2B
$F_{yb} = .55F_y$ =	19.8 ksi	AASHTO 10.32.1A
$t_{SP} = [3/4(RW_{SP})/(L_{SP}F_{yb})]^{1/3}$ =	3.68 in.	
$t'_{SP} = t_{SP} - t_{FLG}$ =	2.30	58 mm
Rad (Radius) =	18.00 in	
$= t'_{SP} + Rad \cdot [Rad^2 - (1/2L_{SP})^2]^{1/2}$ =	2.84 in -----> use =	76 mm

BASE (MASONRY) PLATE: $M=(RW)(W/2)(W/4)=RW/8$

$S_x=W_{SP}T_{SP}^2/6$

$t_p=M/S$

$L_{BP} = R/(W_{BP}F_b)$ =	8.69 in -----> use =	8.75	in	222 mm
$t_{BP} = [3/4(RL_{BP})/(W_{BP}F_{yb})]^{1/3}$ =	1.74 in -----> use =	1.75	in	44 mm

ALLOWABLE BEARING ON CONCRETE:

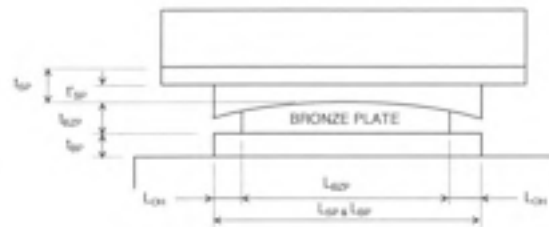
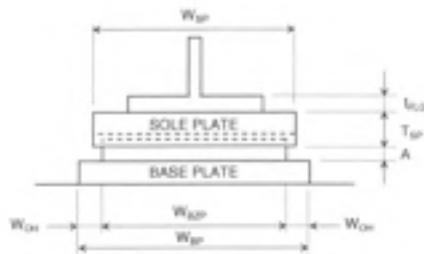
$$f_b = R/(L_{BP} \cdot W_{BP}) = 1.043 \text{ ksi} \quad f_b < F_b \rightarrow \text{OK}$$

BASE PLATE			SOLE PLATE			BEARING DEPTH
WIDTH	LENGTH	HEIGHT	WIDTH	LENGTH	HEIGHT	
18.5"	8.75"	1.75"	18.5"	8.75"	3"	4.75"

BRIDGE: I-75 over Frey Road
COUNTY: COBB
P.I. NO: 713640
PROJECT: NH000-0575-01(028)

J.B. TRIMBLE, INC.
JBT

JOB NO: 31-6036
DESIGNED BY: SHG
DATE: 10/31/2009



EXPANSION BEARING CALCULATIONS

BENT 3 BK

GENERAL INPUT:

Beam Type	Plate Girder	
R (Reaction) =	168.9	Kips
Bottom Flange Thick, t_{LUG} =	1.375	in
W_{SP} =	18.50	in
W_{SP} =	12.00	in
W_{SP} =	18.50	in
L_{SP} =	10.00	in
L_{SP} =	10.00	in
		35 mm
		470 mm
		305 mm
		470 mm
		254 mm
		254 mm

ALLOWABLE BEARING ON CONCRETE:

f'_c =	3500	psi
$F_b = 0.3f'_c$ =	1.050	ksi
$f_b = R/(L_{SP} * W_{SP})$ =	0.913	ksi
		$f_b < F_b \rightarrow OK$

BRONZE PLATE WIDTH (W_{SP}):

TYPE = SELF LUBRICATING ASTM B22 ALLOY 911				
BEARING CAPACITY =	2000	psi		
L_{SP} =	7.04	in	-----> use =	8.0 in 203 mm

BASE (MASONRY) PLATE:

Max of W_{CH} or L_{CH} =	3.25	in
$M = wL^2/2 = f_b \text{ Max}(W_{CH} \text{ or } L_{CH})^2/2$ =	4.82	K-in
F_y =	36000	psi
$F_{yb} = .55F_y$ =	19.8	ksi
$t_{SP} = [6M/F_{yb}]^{1/3}$ =	1.21	in
		use = 1.25 in 32 mm
		AASHTO Table 10.2B
		AASHTO 10.32.1A

SOLE PLATE:

$t_{SP} = [3/4(RW_{SP})/(L_{SP}F_{yb})]^{1/3}$ =	3.44	in.
$t'_{SP} = t_{SP} - t_{LUG}$ =	2.07	in
		use = 2.25 in
Rad (Radius) =	18.00	in
$T_{SP} = t'_{SP} + \text{Rad} \cdot [\text{Rad}^2 - (1/2L_{SP})^2]^{1/2}$ =	2.70	in
		use = 2.75 in

BRONZE PLATE THICKNESS (t_{SP}):

A =	0.75	in
$t_{SP} = (T_{SP} - t'_{SP}) + A$ =	1.25	in
		use = 1.25 in 32 mm

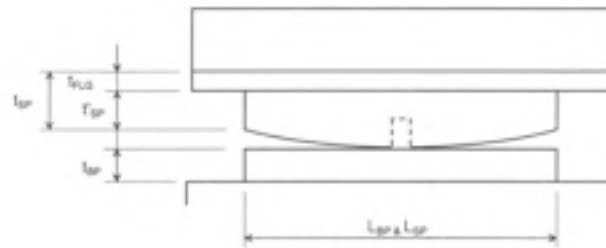
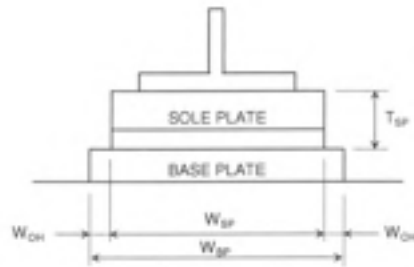
BASE PLATE			SOLE PLATE			BRONZE PLATE			BEARING DEPTH
WIDTH	LENGTH	HEIGHT	WIDTH	LENGTH	HEIGHT	WIDTH	LENGTH	HEIGHT	
18.5"	10"	1.25"	18.5"	10"	2.25"	12"	8"	1.25"	4.75"

BRIDGE: I-75 over Frey Road
COUNTY: COBB
P.I. NO: 713640
PROJECT: NH000-0575-01(028)

J.B. TRIMBLE, INC.



JOB NO: 31-6036
DESIGNED BY: SHG
DATE: 10/31/2009



BENTS 3 AH

FIXED BEARING CALCULATIONS

GENERAL INPUT:

Beam Type	Plate Gider	
R (Reaction) =	152.9 Kips	
Bottom Flange Thickness, t_{FLG} =	1.375 in	35 mm
W_{SP} =	14.00 in	356 mm
W_{BP} =	14.00 in	356 mm
L_{SP} =	10.50 in	267 mm
F_c =	3500 psi	
$F_b = 0.3F_c$ =	1,050 ksi	
AASHTO Art. 8.15.2.1.3		

SOLE PLATE:

$$M=RL/8$$

$$S=wt^3/6$$

$$I_p=M/S$$

F_y =	36000 psi	AASHTO Table 10.2B
$F_{yb} = .55F_y$ =	19.8 ksi	AASHTO 10.32.1A
$t_{SP} = [3/4(RW_{SP})/(L_{SP}F_{yb})]^{1/3}$ =	2.78 in.	
$t'_{SP} = t_{SP} - t_{FLG}$ =	1.40	36 mm
Rad (Radius) =	18.00 in	
$= t'_{SP} + Rad - [Rad^2 - (1/2 L_{SP})^2]^{1/2}$ =	2.19 in -----> use =	2.25 in 57 mm

BASE (MASONRY) PLATE: $M=(RW)(W/2)(W/4)=RW/8$

$$S_y=W_{SP}T_{SP}^2/6$$

$$I_p=M/S$$

$L_{BP} = R/(W_{BP}F_b) =$	10.40 in -----> use =	10.50 in	267 mm
$t_{BP} = [3/4(RL_{BP})/(W_{BP}F_{yb})]^{1/3} =$	2.08 in -----> use =	2.25 in	57 mm

ALLOWABLE BEARING ON CONCRETE:

$$f_b = R/(L_{BP} * W_{BP}) = 1.040 \text{ ksi} \quad f_b < F_b \rightarrow \text{OK}$$

BASE PLATE			SOLE PLATE			BEARING DEPTH
WIDTH	LENGTH	HEIGHT	WIDTH	LENGTH	HEIGHT	
14"	10.5"	2.25"	14"	10.5"	2.25"	4.5"

JOB NO: 31-6036
DESIGNED BY: SHG
DATE: 10/31/2009

CALCULATION COVER SHEET

PROJECT	JOB NO.	CALC NO.	SHEET
I-75 / I-575 NORTHWEST CORRIDOR	NH000-0073-03(242)	BR#33	1
SUBJECT	DISCIPLINE		
Substructure Design Input	STRUCTURAL		

CALCULATION STATUS DESIGNATION	PRELIMINARY	CONFIRMED	SUPSEDED	VOIDED	INCOMPLETE
	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>

COMPUTER PROGRAM/TYPE	SCP	MAINFRAME	PC	PROGRAM	VERSION/RELEASE NO.
	<input checked="" type="radio"/> YES <input type="radio"/> NO	<input type="radio"/>	<input checked="" type="radio"/>	Excel	2003

Note 1: Georgia Department of Transportation (GDOT) terminated Contract Number TOURDPP160072 for its convenience prior to the completion of all work under that contract and directed that the work with respect to these calculations be discontinued.

(a) These calculations were not completed at the time of GDOT's direction and the information contained herein is not complete and/or has not been fully verified or checked. These calculations are a work-in-progress and are presented only as such.

(b) Any user is cautioned that the use of these calculations and any related information or calculations, without access to factors and without proper regard for their purpose, could lead to erroneous conclusions.

(c) If any such calculations or any information contained herein is used in future work efforts or any follow on design work activity, a complete confirmation of the information contained herein should be performed prior to any such use.

(d) GTP has no responsibility for the use of this information not under its direct control.

Substructure Design Input calculations are included for bent 3.

A	As per GDOT's termination for convenience direction	5	5	JCR			11/30/09
NO.	REASON FOR REVISION	TOTAL NO. OF SHEETS	LAST SHEET NO.	BY	CHECKED	APPROVED/ ACCEPTED	DATE
RECORD OF REVISIONS							

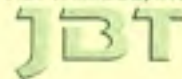
CALCULATION SHEET

PROJECT: I-75 / I-575 NORTHWEST CORRIDOR
JOB NUMBER NH000-0073-03(242)
CALC NO. BR#33

SUBJECT: Bent Design Input - Bent 3
BY: JCR DATE: 11/30/2009

SHEET NO.
SHEET REV.

Sufficient sample calculations representative of the scope and conditions in the design calculation were performed and the results compared to demonstrate the computer program adequacy.



PIER DESIGN CALCULATIONS

BENT 3

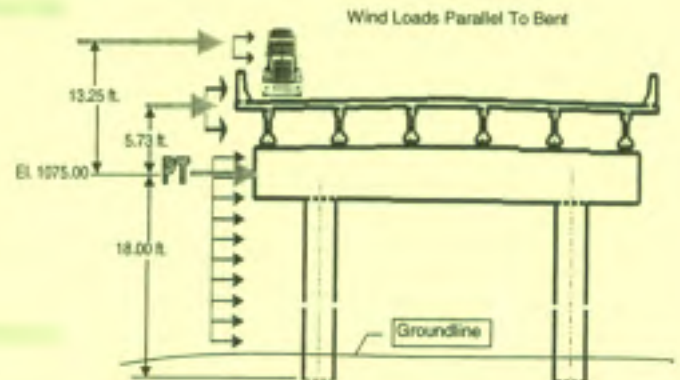
GENERAL REQUIREMENTS:

Live Load cases:	See GDOT Program BRLLCA													
Skew Angle:	33.00	* FROM CL BRIDGE		Is Bent Fix "F" or Exp. "E"?	E	F = Fix								
	57	* FROM CL BENT				E = Exp								
Concrete Strength:	3500	psi												
Rebar Strength:	60000	psi												
Ec =	3587	ksi		AASHTO 8.7.1										
Es =	29000	ksi		AASHTO 8.7.2										
Allowable Steel Stress:	24000	psi		AASHTO 8.15.2.2										
n = Ec/Es =	8			AASHTO 8.15.3.4										
Cap Bar size:	11	#												
Stirup Size:	5	#												
Maximum bars / row in cap:	17	bars												
Column Steel Ratios:	1	% min.												
	8	% max.												
Edge of Column to main rebar:	3.135	in.												
Impact Factor	<table><tr><th>Length (ft)</th><th>Impact</th></tr><tr><td>LEFT SPAN</td><td>1.202</td></tr><tr><td>RIGHT SPAN</td><td>1.208</td></tr><tr><td>Avg. Impact =</td><td>1.20</td></tr></table>						Length (ft)	Impact	LEFT SPAN	1.202	RIGHT SPAN	1.208	Avg. Impact =	1.20
Length (ft)	Impact													
LEFT SPAN	1.202													
RIGHT SPAN	1.208													
Avg. Impact =	1.20													
Soil Weight	0.120	ksf												
Columns:	TYPE S (S-SQUARE or RECTANGULAR, C-CIRCULAR, P-PILES)													
Pile Spacing:	0.00	ft. MIN	0	ft. MAX										
	0.00	ft. EMBED	0	ft. EDGE										
Pile Capacity:	TYPE 14 X 73 STEEL HP													
ALLOWABLE LOAD	192	KIPS =		96	TONS									
UPLIFT	0	KIPS =												

WIND ON SUPERSTRUCTURE

AASHTO 3.15.2.1.1

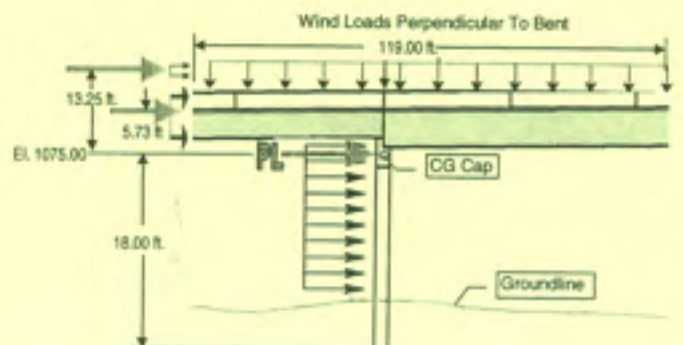
	Left Span	Right Span	
Parapet Height =	32 in.	32 in.	
Beam Height =	48 in.	48 in.	
'D' or 'H' Dimension =	9.5 in.	9.5 in.	
Beam + Coping + Slab =	4.79 ft.	4.79 ft.	
Total Height =	7.46 ft.	7.46 ft.	
Span Lengths =	123.00 ft.	115.00 ft.	TOTAL
Wind Force Area =	458.7 ft ²	428.9 ft ²	888 ft ²
Height of Cap =	4.00 ft.	4.00 ft.	
Wind Force Arm =	5.73 ft.		

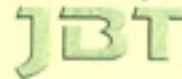


WIND ON SUBSTRUCTURE

AASHTO 3.15.2.2

Wind Force =	0.040	ksf	PARA. & PERP.
Length of Cap =	42.00	ft.	
Width of Cap =	4.75	ft.	
CG of Cap ELEV =	1075.00		
Ground Line ELEV =	1059.00		
100 YR Scour ELEV =	0.00		
Depth to Point of Fixity =	2.00		
Pt. of Fixity ELEV =	1057.00		
Bot. Cap to Pt. of Fixity =	16.00	ft.	CG Cap to Pt. of Fixity
Design Height of Column =	18.00	ft.	
Exposed Height of Column =	14.00	ft.	
Width of Column =	3.50	ft.	
Depth of Column =	3.50	ft.	
No. of Columns =	2	columns	
	PARA.	PERP.	
M _{cap} =	13.68	120.96	k-ft.
M _{col} =	17.64	35.28	k-ft.
M _{total} =	31.32	156.24	k-ft.
	PT = 1.74	PL = 8.68	kips





PIER DESIGN CALCULATIONS

BENT 3

WIND ON LIVE LOAD

AASHTO 3.15.2.1.2

Length = 119.00 ft
APT = APL = 12.79 ft Use → 13.25 ft

TRACTION FORCE: For One lane

AASHTO 3.9

LF = 8.00 k

TEMPERATURE FORCE:

AASHTO 3.16

Friction Force due to Temperature:

$$\Delta = \text{Temp. Deflection} = \text{ALPHA} \times \text{Length} \times \text{Change in Temp.}$$

T_{ASS} = 30 ° T_{FALL} = 40 ° (Fahrenheit)
Material (C or S): C ALPHA = 0.000006 / ° (Fahrenheit)

$$\text{Force in Pad} = F_s = [G \times L \times W \times \text{Deflection}] / (\text{Telas})$$

	LEFT	RIGHT	
Expansion Length =	0.00	115.00	ft
Δ =	0.000	0.331	in
G = Shear Modulus of Pad =	200	200	psi
L = Length of Pad =	10.50	10.50	in
W = Width of Pad =	12.00	12.00	in
Telas = Bearing Elastomer Depth =	4.250	4.250	in
F _s =	0.00	1.96	KIPS / pad
No. of Beams =	4	4	
Total Temperature Force =	0.00	7.86	kips @ top of seat
	0.00	8.73	kips @ center of cap
P _L =	0.00	4.75	kips
P _T =	0.00	7.32	kips
Difference =	P _L = 4.75 kips		AT CL CAP
	P _T = 7.32 kips		AT CL CAP
	P _L = 5.38 kips		AT CL CAP →
	P _T = 8.29 kips		AT CL CAP
Expansion of Concrete Cap =	0.00018	in/in	
Contraction of Concrete Cap =	0.00044	in/in	which includes 0.0002 for creep

Use Total Lateral Force
= P_L + Equiv. Lateral Force from MDL
due to eccentricity

STREAM FORCE:

AASHTO 3.16.1

100 yr Flood ELEV. = 0 ft
Point of Floxy = 18.00 ft
Bottom of Stream ELEV = 1056.00 ft
Pt. of Floxy ELEV = 1057.00 ft
V_{AVG} = 0 FPS @ 100 yr. Flood
K = 1.4 for square ended piers
P_{AVG} = K * (V_{AVG})² = 0.00 psf
P_{MAX} = 2 * P_{AVG} = 0.00 psf
Piers Aligned with stream flow;
P_L = 0.000 kips
M = 0.00 k-ft
P_{CL CAP} = 0.000 k

AASHTO Eq. (3-4)

BRIDGE: I-75 over Frey Road
COUNTY: COBB
P.I. NO: 713640
PROJECT: NH000-0575-01(02B)

J.B. TRIMBLE, INC.



JOB NO: 31-6036
DESIGNED BY: SHG
DATE: 10/27/2009

PIER DESIGN CALCULATIONS

BENT 3

DEAD LOAD:

AASHTO 3.3

LENGTH = 42.00 feet STEP HT = 0.000 ft
SKIEW = 33.00 degrees STEP WT = 2.292 ft

SPAN 2

BEAM	BEAM SPACING	DISTANCE BETWEEN	DISTANCE ALONG	R d	Addl DL	DL
1		1.492	1.492	111.0	0.00	111.0
2	7.083	13.005	14.497	111.0	0.00	111.0
3	7.083	13.005	27.503	111.0	0.00	111.0
4	7.083	13.005	40.508	111.0	0.0	111.0
		1.492	42.000			

TOTAL 42.000 443.9
CL Brg to CL Bent = 1.083

SPAN 3

BEAM	BEAM SPACING	DISTANCE BETWEEN	DISTANCE ALONG	R d	Addl DL	DL
1		1.492	1.492	97.5	0.00	97.5
2	7.083	13.005	14.497	97.5	0.0	97.5
3	7.083	13.005	27.503	97.5	0.0	97.5
4	7.083	13.005	40.508	97.5	0.00	97.5
		1.492	42.000			

TOTAL 42.000 390.0
CL Brg to CL Bent = 1.083
833.9

COMBINED LOADS

COLUMN = 1.750 FT - checking 1/4 points on column

	POINT	MEMBER		DISTANCE ALONG	R d	Addl DL	DL	CHECK POINT
7.50								
	G1	1	6.008	1.492	208.5	0.0	208.5	1
	EC	1	5.133	6.625				2
27.00								
	EC	2	0.875	8.375				3
	G2	2	6.122	14.497	208.5	0.0	208.5	4
	CHECK	2	6.503	21.000				5
	G5	2	6.503	27.503	208.5	0.0	208.5	6
	EC	2	6.122	33.625				7
7.50								
	EC	3	0.875	35.375				8
	G6	3	5.133	40.508	208.5	0.0	208.5	9
				1.492				
			42.000					

ADDITIONAL DL MOMENT DUE TO ECCENTRICITY:

$M_{DL} = 58.32$ KIP-FT
(EQUIV. LONG FORCE) $F_{DL} = M_{DL} / H_{top of column} = 3.24$ KIP
(TOTAL LONG FORCE) $F_L = F_{DL} + P_{L TOP} = 8.82$ KIP

LIVE LOADS:

AASHTO 3.4

Span Lengths = LEFT 123.00 RIGHT 115.00 ft
LIVE LOAD REACTION 67.38 KIPS AXLE LOAD NO IMPACT
102.16 KIPS LANE LOAD NO IMPACT
AVERAGE IMPACT 1.20
P-LOAD FOR BRLLCA INPUT 62 KIPS

VERIFY !!!

CENTRIFUGAL FORCE:

AASHTO 3.10

LIVE LOAD REACTION = 67.38 KIPS AXLE LOAD NO IMPACT
Speed (S) = 70 mph
Curve Radius (R) = 5890 ft
 $C = 6.68 S^2 / R = 5.56$ %
Cent. Force @ 6ft above Rdwy = 3.74 kips

CALCULATION COVER SHEET

PROJECT I-75 / I-575 NORTHWEST CORRIDOR	JOB NO. NH000-0073-03(242)	CALC NO. BR#33	SHEET 1
SUBJECT Live Load Case Output		DISCIPLINE STRUCTURAL	

CALCULATION STATUS DESIGNATION	PRELIMINARY <input type="checkbox"/>	CONFIRMED <input type="checkbox"/>	SUPSEDED <input type="checkbox"/>	VOIDED <input type="checkbox"/>	INCOMPLETE <input checked="" type="checkbox"/>
---	---	---------------------------------------	--------------------------------------	------------------------------------	---

COMPUTER PROGRAM/TYPE	SCP <input checked="" type="radio"/> YES <input type="radio"/> NO	MAINFRAME <input type="radio"/>	PC <input checked="" type="radio"/>	PROGRAM GDOT BRLLCA	VERSION/RELEASE NO. 06/26/2008
----------------------------------	--	--	--	-------------------------------	---------------------------------------

Note 1: Georgia Department of Transportation (GDOT) terminated Contract Number TOURDPPI60072 for its convenience the completion of all work under that contract and directed that the work with respect to these calculations be discontinued.

(a) These calculations were not completed at the time of GDOT's direction and the information contained herein is not and/or has not been fully verified or checked. These calculations are a work-in-progress and are presented only as such.

(b) Any user is cautioned that the use of these calculations and any related information or calculations, without access to factors and without proper regard for their purpose, could lead to erroneous conclusions.

(c) If any such calculations or any information contained herein is used in future work efforts or any follow on design work a complete confirmation of the information contained herein should be performed prior to any such use.

(d) GTP has no responsibility for the use of this information not under its direct control.

Live Load Case output is included for bent 3.

A	As per GDOT's termination for convenience direction	3	3	JCR			11/30/09
NO.	REASON FOR REVISION	TOTAL NO. OF SHEETS	LAST SHEET NO.	BY	CHECKED	APPROVED/ ACCEPTED	DATE
RECORD OF REVISIONS							

CALCULATION SHEET

PROJECT: I-75 / I-575 NORTHWEST CORRIDOR
JOB NUMBER NH000-0073-03(242)
CALC NO. BR#33

SUBJECT: Live Load Case Output - Bent 3
BY: JCR DATE: 11/30/2009

SHEET NO.
SHEET REV.

Sufficient sample calculations representative of the scope and conditions in the design calculation were performed and the results compared to demonstrate the computer program adequacy.

17-OCT-09
10:03:49

GEORGIA DEPARTMENT OF TRANSPORTATION
PRECONSTRUCTION DIVISION - OFFICE OF BRIDGE & STRUCTURAL DESIGN
SUMMARY OF THE LIVE LOAD CASE PROGRAM
REVISED: JUNE 26, 2008

PROB. NO.

I-75 OVER STEVE FREY RD

BRIDGE WIDTH		D1	D2	D3	D4	D5	D6	D7	D8	# OF BEAMS		REACTION FORCE	MAXIMUM # OF TRUCKS		# OF COLUMNS		COLUMN WIDTH		SKEW ANGLE	
X1	X2																			
27.625	2.625	7.000	7.000	7.000	7.000	3.500					5	62.000		2		0		0.000		0
							13.813													
<div> <div>NO. OF TRUCKS</div> <div>BEAM 1</div> <div>BEAM 2</div> <div>BEAM 3</div> <div>BEAM 4</div> <div>BEAM 5</div> <div>BEAM 6</div> <div>BEAM 7</div> <div>BEAM 8</div> <div>BEAM 9</div> <div>BEAM 10</div> </div>																				
LL CASE 1	1		73.435		50.565				0.000			0.000		0.000		0.000		0.000		0.000
LL CASE 2	2		73.435		88.571			70.857				15.137		0.000		0.000		0.000		0.000
LL CASE 3	1		0.000		0.000			20.292				41.708		62.000		0.000		0.000		0.000
LL CASE 4	2		0.000		46.863			91.149				47.988		62.000		0.000		0.000		0.000
LL CASE 5	1		0.000		26.571			70.857				26.571		0.000		0.000		0.000		0.000
LL CASE 6	2		53.143		97.429			70.857				26.571		0.000		0.000		0.000		0.000
LL CASE 7	2		36.341		80.627			87.659				43.373		0.000		0.000		0.000		0.000
LL CASE 8	2		73.435		50.565			20.292				41.708		62.000		0.000		0.000		0.000

CALCULATION COVER SHEET

PROJECT I-75 / I-575 NORTHWEST CORRIDOR	JOB NO. NH000-0073-03(242)	CALC NO. BR#33	SHEET 1
SUBJECT Intermediate Bent Design Output		DISCIPLINE STRUCTURAL	

CALCULATION STATUS DESIGNATION	PRELIMINARY <input type="checkbox"/>	CONFIRMED <input type="checkbox"/>	SUPSEDED <input type="checkbox"/>	VOIDED <input type="checkbox"/>	INCOMPLETE <input checked="" type="checkbox"/>
---	---	---------------------------------------	--------------------------------------	------------------------------------	---

COMPUTER PROGRAM/TYPE	SCP <input checked="" type="radio"/> YES <input type="radio"/> NO	MAINFRAME <input type="radio"/>	PC <input checked="" type="radio"/>	PROGRAM GDOT BRPIER	VERSION/RELEASE NO. 06/26/2008
----------------------------------	--	--	--	-------------------------------	---------------------------------------

Note 1: Georgia Department of Transportation (GDOT) terminated Contract Number TOURDPPI60072 for its convenience the completion of all work under that contract and directed that the work with respect to these calculations be discontinued.

(a) These calculations were not completed at the time of GDOT's direction and the information contained herein is not and/or has not been fully verified or checked. These calculations are a work-in-progress and are presented only as such.

(b) Any user is cautioned that the use of these calculations and any related information or calculations, without access to factors and without proper regard for their purpose, could lead to erroneous conclusions.

(c) If any such calculations or any information contained herein is used in future work efforts or any follow on design work a complete confirmation of the information contained herein should be performed prior to any such use.

(d) GTP has no responsibility for the use of this information not under its direct control.

Intermediate bent design output is included for bent 3.

A	As per GDOT's termination for convenience direction	7	7	JCR			11/30/09
NO.	REASON FOR REVISION	TOTAL NO. OF SHEETS	LAST SHEET NO.	BY	CHECKED	APPROVED/ ACCEPTED	DATE
RECORD OF REVISIONS							

CALCULATION SHEET

PROJECT: I-75 / I-575 NORTHWEST CORRIDOR
JOB NUMBER NH000-0073-03(242)
CALC NO. BR#33

SUBJECT: Bent Design Output - Bent 3
BY: JCR DATE: 11/30/2009

SHEET NO.
SHEET REV.

Sufficient sample calculations representative of the scope and conditions in the design calculation were performed and the results compared to demonstrate the computer program adequacy.

27-OCT-09
16:50:05

GEORGIA DEPARTMENT OF TRANSPORTATION
PRECONSTRUCTION DIVISION - OFFICE OF BRIDGE & STRUCTURAL DESIGN
THE ANALYSIS AND DESIGN OF PIERS FOR BRIDGES - V 4.2.07 - AASHTO SPECS 1984 INTERIM
REVISED: JUNE 30, 2008
I-75 OVER STEVE FREY RD - BENT 3

PROB. NO.

DESIGN DATA																										
DESIGN NO.	NO.	NO.	SKW	ANG	P/C	FC	N	FY	FS	EC	ES	CONC.	Z	* * * CAP REINFORCING STEEL * * *												
OPTIONS	CAN	COL	LLC	D	M	S	PSI	PSI	PSI	PSI	KSI	KSI	STRAIN	FACT												
														MAIN	STR	MAX	MAX	MIN	MIN	TOP	MIN	DEPTH	BOT			
														SIZE	SIZE	TOP	BOT	SIZE	NO.	CL.	S.P	INCR.	CL.			
D	D	D	L	2	2	8	57-00-00	3500	1400	8	60000	24000	3587	29000	0.0030	170	11	5	10	11	6	4	2.00	4.00	3.00	2.00

COLUMN REINFORCING STEEL															R	KL	OC	OF	CM	BD1	BD2	IMPACT	SOIL WT	ALL.S.P.	MIN	MAX	EDGE	PILE	REBAR	ALL.PILE	ALL.PILE I
MIN.P	MAX.P	CL.SP.	CLEAR	MODE	COEF								%	KCF	KSF	PL SP	FL SP	LP SP	DIST	DEPTH	CLEAR	CAPACITY	UPLIFT	P							
1.00	8.00	2.25	2.500	2	2.00	0.00	0.90	0.00	1.00	0.00	20.00	0.120	0.000	3.00	5.00	1.500	1.000	1.000	192.000	0.000											

CAP DATA																
CN	C	L	A	DE	BC	BE	DH	LH	XB1	XB2	XB3	XB4	XB5	XB6	XB7	XB8
11	C	7.500	0.000	4.000	4.750	0.000	0.000	0.000	6.008	5.133						
12	C	27.000	0.000	4.000	4.750		0.000	0.000	0.875	6.122	6.503	6.503	6.122			
13	C	7.500	0.000	4.000	4.750	0.000	0.000	0.000	0.875	5.133						

COLUMN DATA																											
CN	P	I	T	S	HT	A	DT	BT	DB	BB	DL	FLEX	ND	NS	SZ	ND	NS	SZ	ND	NS	SZ	ND	NS	SZ	SLOPE	EP	AP
21	O	C	T		18.000	0.000	3.500	3.500	0.000	0.000	2.000	0.000	2	4	11	0	0	99	99	11	0	0	0	0.000	0.000	0.000	
22	O	C	T		18.000	0.000	3.500	3.500	0.000	0.000	2.000	0.000	2	4	11	0	0	99	99	11	0	0	0	0.000	0.000	0.000	

FOOTING DATA															
CN	S/P	B	D	T	DEL.B	DEL.D	DEL.T	R.R/D	R.D/B	S.HT.	NP	SYM.	BP	DP	SET.
31	P	6.000	6.000	3.500	0.500	0.500	0.500	0.000	0.000	0.000	4	1	0.000	0.000	0.000
32	P	6.000	6.000	3.500	0.500	0.500	0.500	0.000	0.000	0.000	4	1	0.000	0.000	0.000

GROUP II WIND																	
SUPERSTRUCTURE AREA*STD.				WIND ON SUPERSTRUCTURE INTENSITIES										* WIND FORCE ARM		* WIND ON PIER	
TRANS.	LONG.	WIND	FT1	FL1	FT2	FL2	FT3	FL3	FT4	FL4	FT5	FL5	APT	APL	PT	PL	
444.	444.	1	50	0	44	6	41	12	33	16	17	19	6.104	6.104	1.836	9.848	

GROUP III WIND																										
WIND ON SUPERSTRUCTURE INTENSITIES											WIND ON LIVE LOAD INTENSITIES										LENGTHS OF LL * WIND ON LL ARMS					
AD	FT1	FL1	FT2	FL2	FT3	FL3	FT4	FL4	FT5	FL5	WIND	FT1	FL1	FT2	FL2	FT3	FL3	FT4	FL4	FT5	FL5	TRANS.	LONGI.	APT	APL	
1	50	0	44	6	41	12	33	16	17	19	1	100	0	88	12	82	24	66	32	34	38	119.0	119.0	13.250	13.250	

MISCELLANEOUS FORCES														
CENTRI.	TRACTION	FORCE	AND	ARMS	EXPANSION	SHRINKAGE	STREAM	FLOW						
FT	FL	APT	APL	COEFFICIENT	COEFFICIENT	PT	PL							
3.745	4.580	13.250	13.250	0.00018000	0.00044000	8.441	8.721							

DEAD LOAD SUPERSTRUCTURE AND LIVE LOAD CASES														
I.D.	NL	P1	P2	P3	P4	P5	P6	P7	P8	P9	P10	P11	P12	
D.L.	0	208.500	0.000	0.000	208.500	0.000	208.500	0.000	0.000	208.500				
LL 1	1	0.000	0.000	0.000	0.000	0.000	50.565	0.000	0.000	73.434				
LL 2	2	15.136	0.000	0.000	70.857	0.000	88.571	0.000	0.000	73.434				
LL 3	1	47.987	0.000	0.000	20.291	0.000	0.000	0.000	0.000	41.708				
LL 4	2	47.987	0.000	0.000	91.148	0.000	46.863	0.000	0.000	0.000				
LL 5	1	26.571	0.000	0.000	70.857	0.000	26.571	0.000	0.000	0.000				
LL 6	2	26.571	0.000	0.000	70.857	0.000	97.428	0.000	0.000	53.142				
LL 7	2	43.373	0.000	0.000	87.659	0.000	80.626	0.000	0.000	36.340				
LL 8	2	41.708	0.000	0.000	20.291	0.000	50.565	0.000	0.000	73.434				

① Wind Area reduced for loading with both taking portion of wind (see over the pier attached to existing structure)

② $FL = 1.25 \times \left[\left(2 \times \frac{11.5}{2} \right) \times (1 + 4\%) + 18^2 \right] = 4.58^E$
(AASHTO 5.9)

MEMBER PROPERTIES																
MEM	COLUMN PROPERTIES															
	KT KTM	COTB COTM	COTBM COTBM	TLR TRL	TRC TCR	TLC TCL	DPC DPL	KL PDF	FKBR FKUBR	PCBR PCUBR	PCL PLU	UFMT UFMB	EITTB EILTB	PSIT PSIB	RGTB RGL	
	1435397.9	0.5000	0.5000	0.5363	1.0000	0.4637	0.4637	0.077193	9.1	243952.0	13511.0	119616.5	315405.6	0.5	12.4	
	1435397.9	0.5000	0.3033	0.0000	1.0000	0.0000	0.0000	0.5000	18.5	58641.4	16.0	119616.5	315405.6	0.0	12.4	
2	1435397.9	0.5000	0.5000	0.0000	0.4637	1.0000	0.4637	0.077193	9.1	243952.0	13511.0	119616.5	315405.6	0.5	12.4	
	1435397.9	0.5000	0.3033	0.5363	0.0000	1.0000	0.5363	0.5000	18.5	58641.4	16.0	119616.5	315405.6	0.0	12.4	
CN	CAP PROPERTIES															
	CO K	KML KMR	COMLR COMRL	FMWT UFEM	FMLP1 FMRP1	FMLP2 FMRP2	FMLP3 FMRP3	FMLP4 FMRP4	FMLP5 FMRP5	FMLP6 FMRP6	FMLP7 FMRP7	FMLP8 FMRP8				
2	0.5000	1660113.9	0.2484	173.1375	0.8192	3.8404	3.3750	1.3434	0.0274							
	1938574.2	1660113.9	0.2484	107698.6	0.0274	1.3434	3.3750	3.8404	0.8192							
COLUMN MOMENTS (KIP-FEET), SHEARS (KIPS), REACTIONS (KIPS)																
LOAD	COL	PC	MT	TRANSVERSE					MF	LONGITUDINAL						
				V	MB	BP	ML	MR		MT	V	MB	MF			
UNIT F.A.T CL.CAP	1	0.297	4.006	0.500	4.994	0.297	0.000	-4.006	1.000	0.500	9.000	9.000				
	2	-0.297	4.006	0.500	4.994	-0.297	-4.006	0.000	1.000	0.500	9.000	9.000				
EXPANSION OF CAP	1	0.000	117.163	17.838	203.916	0.000	0.000	-117.163	0.000	0.000	0.000	0.000				
	2	0.000	-117.163	-17.838	-203.916	0.000	117.163	0.000	0.000	0.000	0.000	0.000				
SHRINKAGE OF CAP	1	0.000	-286.399	-43.603	-498.461	0.000	0.000	286.399	0.000	0.000	0.000	0.000				
	2	0.000	286.399	43.603	498.461	0.000	-286.399	0.000	0.000	0.000	0.000	0.000				
DEAD LOAD TOTAL	1	476.850	-47.083	-3.924	-23.541	506.250	1332.824	-1285.741	0.000	0.000	0.000	0.000				
		506.250														
	2	476.850	47.083	3.924	23.541	506.250	1285.741	-1332.824	0.000	0.000	0.000	0.000				
		506.250														
STREAM FLOW	1	2.505	33.812	4.220	42.157	2.505	0.000	-33.812	8.721	4.360	78.489	78.489				
	2	-2.505	33.812	4.220	42.157	-2.505	-33.812	0.000	8.721	4.360	78.489	78.489				
VC. FORCE 1 LN	1	3.025	15.386	1.921	19.184	3.025	0.000	-15.386	-19.020	-1.247	-38.976	-38.976				
	2	-3.025	15.386	1.921	19.184	-3.025	-15.386	0.000	-19.020	-1.247	-38.976	-38.976				
CENT. FORCE 1 LN	1	1.606	8.170	1.020	10.187	1.606	0.000	-8.170	23.949	1.570	49.075	49.075				
	2	-1.606	8.170	1.020	10.187	-1.606	-8.170	0.000	23.949	1.570	49.075	49.075				
WIND ON SUBSTR.	1	0.545	7.354	0.918	9.170	0.545	0.000	-7.354	-9.848	-4.924	-88.632	-88.632				
	2	-0.545	7.354	0.918	9.170	-0.545	-7.354	0.000	-9.848	-4.924	-88.632	-88.632				
GROUP 2 WIND 1 1	1	6.866	55.787	6.963	69.556	6.866	0.000	-55.787	65.594	4.385	135.758	135.758				
	2	-6.866	55.787	6.963	69.556	-6.866	-55.787	0.000	65.594	4.385	135.758	135.758				
GROUP 2 WIND 1 2	1	6.866	55.787	6.963	69.556	6.866	0.000	-55.787	65.290	14.233	313.022	313.022				
	2	-6.866	55.787	6.963	69.556	-6.866	-55.787	0.000	65.290	14.233	313.022	313.022				
GROUP 2 WIND 2 1	1	7.275	58.925	7.355	73.468	7.275	0.000	-58.925	50.662	2.543	91.345	91.345				
	2	-7.275	58.925	7.355	73.468	-7.275	-58.925	0.000	50.662	2.543	91.345	91.345				
GROUP 2 WIND 2 2	1	4.939	41.026	5.121	51.151	4.939	0.000	-41.026	82.116	13.842	303.582	303.582				
	2	-4.939	41.026	5.121	51.151	-4.939	-41.026	0.000	82.116	13.842	303.582	303.582				
GROUP 2 WIND 3 1	1	8.064	64.968	8.110	81.003	8.064	0.000	-64.968	40.256	1.259	60.395	60.395				
	2	-8.064	64.968	8.110	81.003	-8.064	-64.968	0.000	40.256	1.259	60.395	60.395				
GROUP 2 WIND 3 2	1	3.392	29.170	3.641	36.370	3.392	0.000	-29.170	83.469	14.008	307.605	307.605				
	2	-3.392	29.170	3.641	36.370	-3.392	-29.170	0.000	83.469	14.008	307.605	307.605				
GROUP 2 WIND 4 1	1	7.831	63.185	7.887	78.780	7.831	0.000	-63.185	24.266	-0.714	12.835	12.835				
	2	-7.831	63.185	7.887	78.780	-7.831	-63.185	0.000	24.266	-0.714	12.835	12.835				
GROUP 2 WIND 4 2	1	1.602	15.454	1.929	19.269	1.602	0.000	-15.454	75.317	13.003	283.360	283.360				
	2	-1.602	15.454	1.929	19.269	-1.602	-15.454	0.000	75.317	13.003	283.360	283.360				
GROUP 2 WIND 5 1	1	6.393	52.162	6.511	65.036	6.393	0.000	-52.162	-2.815	-4.056	-67.713	-67.713				
	2	-6.393	52.162	6.511	65.036	-6.393	-52.162	0.000	-2.815	-4.056	-67.713	-67.713				
GROUP 2 WIND 5 2	1	-1.005	-4.519	-0.564	-5.634	-1.005	0.000	4.519	54.116	10.386	220.298	220.298				
	2	1.005	-4.519	-0.564	-5.634	1.005	4.519	0.000	54.116	10.386	220.298	220.298				
UP 3 WIND 1 1	1	7.163	42.698	5.330	53.236	7.163	0.000	-42.698	95.777	6.306	196.668	196.668				
	2	-7.163	42.698	5.330	53.236	-7.163	-42.698	0.000	95.777	6.306	196.668	196.668				
GROUP 3 WIND 1 2	1	7.163	42.698	5.330	53.236	7.163	0.000	-42.698	101.686	9.260	249.847	249.847				
	2	-7.163	42.698	5.330	53.236	-7.163	-42.698	0.000	101.686	9.260	249.847	249.847				

LOAD	COL	COLUMN MOMENTS (KIP-FeET), SHEARS (KIPS), REACTIONS (KIPS)									LONGITUDINAL		
		PC	MT	TRANSVERSE				MR	MT				
				V	MB	RF	ML		V	MB	MF		
GROUP 3 WIND 2 1	1	7.617	45.321	5.657	56.507	7.617	0.000	-45.321	76.235	4.765	152.479	152.479	
	2	-7.617	45.321	5.657	56.507	-7.617	-45.321	0.000	76.235	4.765	152.479	152.479	
GROUP 3 WIND 2 2	1	5.030	30.357	3.789	37.849	5.030	0.000	-30.357	97.532	8.933	240.454	240.454	
	2	-5.030	30.357	3.789	37.849	-5.030	-30.357	0.000	97.532	8.933	240.454	240.454	
GROUP 3 WIND 3 1	1	8.490	50.374	6.288	62.806	8.490	0.000	-50.374	62.617	3.692	121.685	121.685	
	2	-8.490	50.374	6.288	62.806	-8.490	-50.374	0.000	62.617	3.692	121.685	121.685	
GROUP 3 WIND 3 2	1	3.316	20.445	2.552	25.491	3.316	0.000	-20.445	99.302	9.072	244.457	244.457	
	2	-3.316	20.445	2.552	25.491	-3.316	-20.445	0.000	99.302	9.072	244.457	244.457	
GROUP 3 WIND 4 1	1	8.233	48.883	6.102	60.948	8.233	0.000	-48.883	41.691	2.042	74.365	74.365	
	2	-8.233	48.883	6.102	60.948	-8.233	-48.883	0.000	41.691	2.042	74.365	74.365	
GROUP 3 WIND 4 2	1	1.334	8.978	1.121	11.194	1.334	0.000	-8.978	88.635	8.231	220.335	220.335	
	2	-1.334	8.978	1.121	11.194	-1.334	-8.978	0.000	88.635	8.231	220.335	220.335	
GROUP 3 WIND 5 1	1	6.639	39.667	4.951	49.457	6.639	0.000	-39.667	6.250	-0.752	-5.776	-5.776	
	2	-6.639	39.667	4.951	49.457	-6.639	-39.667	0.000	6.250	-0.752	-5.776	-5.776	
GROUP 3 WIND 5 2	1	-1.553	-7.720	-0.964	-9.625	-1.553	0.000	7.720	60.888	6.044	157.591	157.591	
	2	1.553	-7.720	-0.964	-9.625	1.553	7.720	0.000	60.888	6.044	157.591	157.591	
LIVE LOAD LL 1	1	-1.955	-36.149	-4.454	-44.021	-1.955	0.000	36.149	0.000	0.000	0.000	0.000	
	2	125.954	70.744	4.454	9.426	125.954	370.447	-441.191	0.000	0.000	0.000	0.000	
LIVE LOAD LL 2	1	78.856	104.646	7.320	27.111	78.856	90.937	-195.583	0.000	0.000	0.000	0.000	
	2	169.142	-71.029	-7.320	-60.727	169.142	512.221	-441.191	0.000	0.000	0.000	0.000	
LIVE LOAD LL 3	1	64.469	-128.732	-10.787	-65.432	64.469	288.306	-159.574	0.000	0.000	0.000	0.000	
	2	45.517	130.154	10.787	64.010	45.517	120.428	-250.582	0.000	0.000	0.000	0.000	
LIVE LOAD LL 4	1	137.614	117.712	10.623	71.499	137.614	288.306	-406.018	0.000	0.000	0.000	0.000	
	2	48.384	-137.235	-10.623	-53.975	48.384	137.235	0.000	0.000	0.000	0.000	0.000	
LIVE LOAD LL 5	1	91.664	100.394	8.591	54.239	91.664	159.639	-260.033	0.000	0.000	0.000	0.000	
	2	32.335	-105.783	-8.591	-48.850	32.335	105.783	0.000	0.000	0.000	0.000	0.000	
LIVE LOAD LL 6	1	98.781	122.547	9.785	53.587	98.781	159.639	-282.185	0.000	0.000	0.000	0.000	
	2	149.217	-112.299	-9.785	-63.835	149.217	431.574	-319.277	0.000	0.000	0.000	0.000	
LIVE LOAD LL 7	1	130.674	116.066	9.785	60.068	130.674	260.585	-378.651	0.000	0.000	0.000	0.000	
	2	117.324	-118.779	-9.785	-57.355	117.324	337.110	-218.331	0.000	0.000	0.000	0.000	
LIVE LOAD LL 8	1	63.253	-90.525	-8.070	-54.738	63.253	250.582	-160.057	0.000	0.000	0.000	0.000	
	2	122.745	103.159	8.070	42.104	122.745	338.032	-441.191	0.000	0.000	0.000	0.000	

CAP ANALYSIS AND DESIGN DATA
CAP MOMENTS AND SHEARS

POINT	D.L.TOT.	MOMENTS (KIP-FeET)						SHEARS (KIPS)					
		G1 MAX. +	G1 MAX. -	G2 MAX. +	G2 MAX. -	G3 MAX. +	G3 MAX. -	DL T. LT	DL T. RT	G1 + LT	G1 + RT	G1 - LT	G1 - RT
P 1	-4.124	-4.124	-4.124	-4.124	-4.124	-4.124	-4.124	-5.528	-276.578	-5.528	-276.578	-5.528	-380.758
P 2	-1472.607	-1472.607	-2007.362	-1472.607	-1472.607	-1472.607	-1792.819	-295.596	-295.596	-295.596	-295.596	-399.775	-399.775
C 1L	-1732.671	-1732.671	-2358.583	-1732.671	-1732.671	-1732.671	-2107.469	-298.837		-298.837		-403.017	
C 1R	-1671.464	-1592.984	-2618.127	-1598.941	-1787.942	-1538.982	-2369.975		321.068		520.476		316.823
P 3	-1391.948	-1317.182	-2164.129	-1324.125	-1500.877	-1267.231	-1977.446	317.826	317.826	517.234	517.234	313.581	313.581
P 4	484.351	1027.681	362.005	519.285	428.243	860.513	359.361	295.144	24.094	494.552	31.860	290.899	8.600
P 5	562.691	1066.069	412.864	562.691	562.691	864.115	472.974	0.000	0.000	7.767	7.767	-15.494	-15.494
P 6	484.351	1038.234	280.755	540.459	449.416	879.433	321.257	-24.094	-295.144	-16.327	-295.144	-39.588	-503.723
P 7	-1391.948	-1391.948	-2322.171	-1283.019	-1459.770	-1355.692	-2047.620	-317.826	-317.826	-317.826	-317.826	-526.405	-526.405
C 2L	-1671.464	-1671.464	-2783.495	-1554.985	-1743.987	-1668.917	-2442.841	-321.068		-321.068		-529.647	
C 2R	-1732.671	-1732.671	-2490.498	-1732.671	-1732.671	-1732.671	-2306.220		298.837		458.263		298.837
P 8	-1472.607	-1472.607	-2290.937	-1472.607	-1472.607	-1472.607	-1962.625	295.596	295.596	455.021	455.021	295.596	295.596
	-4.124	-4.124	-4.124	-4.124	-4.124	-4.124	-4.124	276.578	5.528	436.003	5.528	276.578	5.528

PT.	M+ UNF. K-FT.	M- UNF. K-FT.	TOP REINFORCE. AS NO.SIZE		BOT.REINFORCE. AS NO.SIZE		CAP DESIGN DATA								D IN.	PC PSI	PS %	FS/FF RATIO	FS/PZ RATIO
							LEFT STIRRUPS				RIGHT STIRRUPS								
							M.SP.	AV/IN	BAR&SPAC		M.SP.	AV/IN	BAR&SPAC						
	-3.172	-3.172	1.76	4 # 11	1.76	4 # 11	0.00	0.000	#5@ 0.00		21.98	0.057	#5@10.80	48.00		0.07	0.000	0.007	
P 2	-1132.775	-1379.092	10.33	7 # 11	1.76	4 # 11	22.50	0.062	#5@10.03		22.50	0.062	#5@10.03	48.00		0.43	0.484	1.129	
C 1	-1249.592	-1741.912	13.62	9 # 11	1.76	4 # 11	22.50	0.063	#5@ 9.81		22.50	0.114	#5@ 5.42	48.00		0.57	0.691	1.030	
P 3	-1036.291	-1445.226	11.17	8 # 11	1.76	4 # 11	22.50	0.113	#5@ 5.49		22.50	0.113	#5@ 5.49	48.00		0.47	0.617	0.995	
P 4	622.845	308.108	1.76	4 # 11	5.18	4 # 11	22.50	0.103	#5@ 6.01		0.00	0.000	#5@ 0.00	48.00		0.20	0.763	1.057	
P 5	664.704	363.826	1.76	4 # 11	5.38	4 # 11	0.00	0.000	#5@ 0.00		0.00	0.000	#5@ 0.00	48.00		0.21	0.764	1.128	
P 6	637.398	278.798	1.76	4 # 11	5.24	4 # 11	0.00	0.000	#5@ 0.00		22.50	0.107	#5@ 5.79	48.00		0.20	0.849	1.082	
P 7	-1070.729	-1499.206	12.02	8 # 11	1.76	4 # 11	22.50	0.117	#5@ 5.30		22.50	0.117	#5@ 5.30	48.00		0.50	0.658	1.032	
C 2	-1285.741	-1797.962	14.53	10 # 11	1.76	4 # 11	22.50	0.118	#5@ 5.24		22.50	0.087	#5@ 7.10	48.00		0.61	0.624	0.927	
P 8	-1132.775	-1509.711	11.85	8 # 11	1.76	4 # 11	22.50	0.086	#5@ 7.22		22.50	0.086	#5@ 7.22	48.00		0.50	0.598	1.040	
P 9	-3.172	-3.172	1.76	4 # 11	1.76	4 # 11	21.98	0.082	#5@ 7.56		0.00	0.000	#5@ 0.00	48.00		0.07	0.000	0.007	

NOTE: *** PS/PZ RATIO EXCEEDS 1.0! ***

COLUMN ANALYSIS AND DESIGN OUTPUT

CRITICAL COLUMN LOADS

CN	T B	GR	LLC	WC	R	E C S		PF	MTF	MLF	PM	MTM	MLM	PU	MTU	MLU	PU/PM	B	D
						S	F												
1	T	4	LL 3	0.0		S	C	S	709.1	-546.3	42.5	709.1	546.3	268.9	2255.0	1737.9	855.3	3.181	42.00
1	B	5		1.2	R	S			624.2	-739.4	-391.3	624.2	739.4	418.1	1494.0	1775.5	1003.8	2.398	42.00
2	T	4	LL 8	0.0		S	C	S	772.0	632.8	73.6	772.0	632.8	294.9	2176.5	1784.4	831.5	2.819	42.00
2	B	5		1.2		S		S	621.1	792.1	489.4	621.1	792.1	522.7	1308.6	1669.0	1101.3	2.107	42.00

COLUMN DESIGN DATA

CN	T B	FACE 1		FACE 2		FACE 3		FACE 4		AS	PS	BD12	BD	SUMPU	SUMPC	DEL.T	DEL.L	CM	R	PHIC
		NO. SIZE	NO. SIZE	NO. SIZE	NO. SIZE	NO. SIZE	NO. SIZE	NO. SIZE	NO. SIZE											
1	T	4 # 11	4 # 11	2 # 11	2 # 11	18.72	1.061	1.00	0.078					1421.	76622.	1.000	1.083	0.400	2	0.70
1	B	4 # 11	4 # 11	2 # 11	2 # 11	18.72	1.061	1.00	0.080					1229.	74950.	1.000	1.068	0.400	2	0.70
2	T	4 # 11	4 # 11	2 # 11	2 # 11	18.72	1.061	1.00	0.067					1520.	76269.	1.000	1.091	0.400	2	0.70
2	B	4 # 11	4 # 11	2 # 11	2 # 11	18.72	1.061	1.00	0.074					1229.	74694.	1.000	1.068	0.400	2	0.70

FOOTING 1 DESIGN LOADS

PG	LLID	WC	ES	C	S	P	MT	VT	ML	VL	P4	P3	P2	P1	MTF	VBF	VPP	LOAD
4	LL 8	0.0	S	C	S	564.678	-505.087	-47.992	176.640	7.501	62.407	14.099	174.351	222.659	18.401	0.000	-0.384	MAX.P1
1 4	LL 3	0.0	S	C	S	733.311	-681.440	-66.658	165.834	7.710	67.795	21.886	239.682	285.591	24.366	0.000	-0.499	MAX.MT
1 1	LL 4	0.0		C	S	914.523	183.657	22.256	229.632	9.752	190.244	127.443	189.718	252.518	20.330	0.000	-0.499	MAX.VT
1 1	LL 4	0.0		C	S	914.523	183.657	22.256	229.632	9.752	190.244	127.443	189.718	252.518	20.330	0.000	-0.499	MAX.VP
1 3	LL 4	1.2		C	S	816.086	149.638	16.481	655.769	25.033	234.110	57.114	106.476	283.473	23.992	0.000	-0.499	MAX.ML
1 1	LL 4	0.0		C	S	914.523	183.657	22.256	229.632	9.752	190.244	127.443	189.718	252.518	20.355	0.000	-0.499	MAX.VL
1 4	LL 8	0.0	S	C	S	564.678	-505.087	-47.992	176.640	7.501	62.407	14.099	174.351	222.659	18.401	0.000	-0.384	MAX.P3

FOOTING 1 ANALYSIS/DESIGN RESULTS

FOOTING SIZE				* BAR REINFORCEMENT STEEL *				SECTION CAPACITIES				*	
B	D	T	P1/PA	AS	NO.	SIZE	SPAC.	PLACEMENT	MT.	VB	VP	DS	FC
7.200	7.200	3.500	0.928	0.25	10	# 4	@ 8.625	TOP LONG	35.021	34.094	68.189	28.250	0.000
				0.25	10	# 4	@ 8.625	BOT.TRAN	35.646	34.698	69.396	28.750	0.000

NUMBER OF PILES = 5 BP = 2.100 DP = 2.100

FOOTING 2 DESIGN LOADS

PG	LLID	WC	ES	C	S	P	MT	VT	ML	VL	P4	P3	P2	P1	MTF	VBF	VPP	LOAD
2 4	LL 8	0.0	S	C	S	602.821	619.619	60.512	176.640	7.501	78.765	46.040	180.138	212.863	55.537	-0.244	13.342	MAX.P1
2 4	LL 8	0.0	S	C	S	783.667	805.505	78.666	229.632	9.752	102.394	59.851	234.180	276.722	72.197	-0.317	17.345	MAX.MT
2 4	LL 8	0.0	S	C	S	783.667	805.505	78.666	229.632	9.752	102.394	59.851	234.180	276.722	72.197	-0.317	17.345	MAX.VT
2 1	LL 1	0.0		C	S	880.653	115.704	19.971	165.834	7.710	188.266	157.166	187.102	218.202	56.702	-0.317	19.511	MAX.VP
	LL 2	3.2		C	S	837.483	29.367	3.633	648.763	24.788	234.972	116.340	123.127	241.760	67.183	-0.317	18.547	MAX.ML
2 4	LL 8	0.0	S	C	S	783.667	805.505	78.666	229.632	9.752	102.394	59.851	234.180	276.722	52.859	-0.317	17.345	MAX.VL
2 5		1.2	S		S	496.880	633.715	58.711	391.511	18.594	77.407	3.764	139.119	212.763	49.503	-0.244	10.976	MAX.P3

FOOTING 2 ANALYSIS/DESIGN RESULTS

FOOTING SIZE				* BAR REINFORCEMENT STEEL *				SECTION CAPACITIES				*	
B	D	T	P1/PA	AS	NO.	SIZE	SPAC.	PLACEMENT	MT.	VB	VP	DS	FC
9.200	9.200	3.500	0.887	0.64	20	# 5	@ 5.500	TOP LONG	83.385	33.868	67.736	28.062	0.000
				0.63	19	# 5	@ 5.750	BOT.TRAN	81.098	34.622	69.245	28.688	0.000

NUMBER OF PILES = 5 BP = 3.100 DP = 3.100

CALCULATION COVER SHEET

PROJECT	JOB NO.	CALC NO.	SHEET
I-75 / I-575 NORTHWEST CORRIDOR	NH000-0073-03(242)	BR#33	1
SUBJECT	DISCIPLINE		
References for Design	STRUCTURAL		

CALCULATION STATUS DESIGNATION	PRELIMINARY	CONFIRMED	SUPSEDED	VOIDED	INCOMPLETE
	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>

COMPUTER PROGRAM/TYPE	SCP	MAINFRAME	PC	PROGRAM	VERSION/RELEASE NO.
	<input type="radio"/> YES <input type="radio"/> NO	<input type="radio"/>	<input type="radio"/>	NONE	

Note 1: Georgia Department of Transportation (GDOT) terminated Contract Number TOURDPPI60072 for its convenience the completion of all work under that contract and directed that the work with respect to these calculations be discontinued

- (a) These calculations were not completed at the time of GDOT's direction and the information contained herein is not and/or has not been fully verified or checked. These calculations are a work-in-progress and are presented only as such.
- (b) Any user is cautioned that the use of these calculations and any related information or calculations, without access to factors and without proper regard for their purpose, could lead to erroneous conclusions.
- (c) If any such calculations or any information contained herein is used in future work efforts or any follow on design work a complete confirmation of the information contained herein should be performed prior to any such use.
- (d) GTP has no responsibility for the use of this information not under its direct control.

Included Reference Information:

- Roadway information
- Bridge Survey Shots
- Existing Bridge Plans
- Existing Bridge Maintenance Reports

A	As per GDOT's termination for convenience direction	55	55	JCR			11/30/09
NO.	REASON FOR REVISION	TOTAL NO. OF SHEETS	LAST SHEET NO.	BY	CHECKED	APPROVED/ ACCEPTED	DATE

RECORD OF REVISIONS

CALCULATION SHEET

PROJECT: I-75 / I-575 NORTHWEST CORRIDOR

JOB NUMBER NH000-0073-03(242)

CALC NO. BR#33

SUBJECT: Roadway Information

BY: JCR

DATE: 11/30/2009

SHEET NO.

SHEET REV.

I-75 ALIGN

Element: Linear

PI	()	890+82.1065	1467607.2270	2172269.7940
PI	()	905+54.2556	1469042.1850	2171940.9800
Tangential Direction:		N 12°54'22.5001" W		
Tangential Length:		1472.1491		

Element: Linear

PI	()	905+54.2556	1469042.1850	2171940.9800
PC	()	909+48.6002	1469426.3636	2171852.0166
Tangential Direction:		N 13°02'16.9626" W		
Tangential Length:		394.3446		

Element: Circular

PC	()	✓ 909+48.6002	✓ 1469426.3636	✓ 2171852.0166
PI	()	921+84.8998	✓ 1470630.7919	✓ 2171573.1099
CC	()		1468097.5914	2166113.8580
PCC	()	✓ 933+85.8181	✓ 1471621.4280	✓ 2170833.4635
Radius:		✓ 5890.0000		
Delta:		23°42'30.1308" Left		
Degree of Curvature (Arc):		0°58'21.9492"		
Length:		2437.2179		
Tangent:		1236.2996		
Chord:		2419.8674		
Middle Ordinate:		125.6127		
External:		128.3500		
Tangent Direction:		N 13°02'16.9626" W		
Radial Direction:		N 76°57'43.0375" E		
Chord Direction:		N 24°53'32.0281" W		
Radial Direction:		N 53°15'12.9065" E		
Tangent Direction:		N 36°44'47.0936" W		

BR#33

Element: Circular

PCC	()	933+85.8181	1471621.4280	2170833.4635
PI	()	958+23.3359	1473574.5896	2169375.1588
CC	()		1462677.2247	2158854.1593
PT	()	982+18.3313	1474963.3729	2167371.9679
Radius:		14950.0000		
Delta:		18°31'14.0737" Left		
Degree of Curvature (Arc):		0°22'59.6977"		
Length:		4832.5132		
Tangent:		2437.5178		
Chord:		4811.5016		
Middle Ordinate:		194.8361		
External:		197.4088		
Tangent Direction:		N 36°44'47.0936" W		
Radial Direction:		N 53°15'12.9065" E		
Chord Direction:		N 46°00'24.1304" W		
Radial Direction:		N 34°43'58.8330" E		
Tangent Direction:		N 55°16'01.1671" W		

PROJECT:	NW Corridor
COUNTY:	COBB
BRIDGE:	33
DESCRIPTION:	I-75 over Frey Rd

VERTICAL GRADE DATA FOR NEW ALIGNMENT, ADJUSTED FOR SURVEY DIFF.:

PVC =	923+39.81
PVI EL. =	1077.7500

PVI =	929+39.81
PVI EL. =	1089.75
VC Length (ft) =	1200

PVT =	935+39.81
PVI EL. =	1094.2500

ELEVATION COMPARISON, ADJUSTED FOR SURVEY DIFF.

BENT 1R LEFT SIDE

Geomath Rdy EL. =	1086.022
Survey EL. =	1086.059
DIFFERENCE =	-0.037

BENT 1R RIGHT SIDE

Geomath Rdy EL. =	1088.969
Survey EL. =	1088.944
DIFFERENCE =	0.025

BENT 2R LEFT SIDE

Geomath Rdy EL. =	1087.467
Survey EL. =	1087.413
DIFFERENCE =	0.054

BENT 2R RIGHT SIDE

Geomath Rdy EL. =	1090.500
Survey EL. =	1090.448
DIFFERENCE =	0.052

BENT 3R LEFT SIDE

Geomath Rdy EL. =	1089.117
Survey EL. =	1089.062
DIFFERENCE =	0.055

BENT 3R RIGHT SIDE

Geomath Rdy EL. =	1091.971
Survey EL. =	1091.904
DIFFERENCE =	0.067

BENT 4R LEFT SIDE

Geomath Rdy EL. =	1090.481
Survey EL. =	1090.567
DIFFERENCE =	-0.086

BENT 4R RIGHT SIDE

Geomath Rdy EL. =	1093.317
Survey EL. =	1093.424
DIFFERENCE =	-0.107

Mean EL. Difference =	0.003
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		Station	Northing	Easting
Element: Linear				
POB	()	✓ 97+41.5134	✓ 1471037.5280	✓ 2171056.5920
POE	()	✓ 103+04.8493	✓ 1471600.8130	✓ 2171064.1640
Tangential Direction:		✓ N 0°46'12.5628" E		
Tangential Length:		563.3359		

Alignment Name: XR 1041+50 Hickory Grove
Alignment Description: Hickory Grove Road
Alignment Style: MAIN_P_SIDECL

		Station	Northing	Easting
Element: Linear				
POB	()	✓ 91+22.3408	✓ 1478728.2692	✓ 2162057.1835
PC	()	103+61.2410	✓ 1478859.6912	✓ 2163289.0933
Tangential Direction:		✓ N 83°54'38.2814" E		
Tangential Length:		1238.9002		

Element: Circular				
PC	()	103+61.2410	1478859.6912	2163289.0933
PI	()	106+51.0094	1478890.4297	2163577.2267
CC	()		1478282.9637	2163350.6195
PT	()	108+98.7016	1478678.4923	2163774.8330
Radius:		580.0000		
Delta:		53°05'36.5529" Right		
Degree of Curvature (Arc):		9°52'42.8976"		
Length:		537.4606		
Tangent:		289.7684		
Chord:		518.4362		
Middle Ordinate:		61.1494		
External:		68.3562		
Tangent Direction:		N 83°54'38.2814" E		
Radial Direction:		S 6°05'21.7185" E		
Chord Direction:		S 69°32'33.4421" E		
Radial Direction:		S 47°00'14.8344" W		
Tangent Direction:		S 42°59'45.1657" E		

Element: Linear				
PT	()	108+98.7016	1478678.4923	2163774.8330
POE	()	109+99.9882	1478604.4110	2163843.9050
Tangential Direction:		S 42°59'45.1657" E		
Tangential Length:		101.2866		

FREY
 RD
 ALIGN

PVC	61+60.0000	962.6296
PVI	63+10.0000	963.6800
PVT	64+60.0000	968.4783
Length:	300.0000	
Entrance Grade:	0.70%	
Exit Grade:	3.20%	
$r = (g2 - g1) / L$:	0.8328	
$K = 1 / (g2 - g1)$:	120.0700	
Middle Ordinate:	0.9370	

Element: Linear

PVT	64+60.0000	968.4783
PVI	70+07.4400	985.9900
Tangent Grade:	3.20%	
Tangent Length:	547.4400	

Element: Linear

PVI	70+07.4400	985.9900
POE	571+58.3447	973.4185
Tangent Grade:	-0.03%	
Tangent Length:	50150.9047	

Horizontal Alignment: XR 930+00 Frey/Barrett Lakes
Horizontal Description: I-75 Frey/Barret Lakes Blvd
Horizontal Style: MAIN_P_SIDECL

Vertical Alignment: Point Profile
Vertical Description: Frey/Barrett Lakes Point Profile
Vertical Style: MAIN_P_SIDECL

Element: Linear

POB	97+41.5134	1063.9017
PVI	97+50.0000	1063.8355
Tangent Grade:	-0.78%	
Tangent Length:	8.4866	

Element: Linear

PVI	✓ 97+50.0000	✓ 1063.8355
PVI	✓ 98+00.0000	✓ 1063.4695
Tangent Grade:	-0.73%	
Tangent Length:	50.0000	

Element: Linear

PVI	98+00.0000	1063.4695
PVI	98+50.0000	1063.2343
Tangent Grade:	-0.47%	
Tangent Length:	50.0000	

Element: Linear

PVI	✓ 98+50.0000	✓ 1063.2343
PVI	✓ 99+00.0000	✓ 1063.0571

Tangent Grade: -0.35%
Tangent Length: 50.0000

Element: Linear

PVI 99+00.0000 1063.0571
PVI 99+50.0000 1062.8992
Tangent Grade: -0.32%
Tangent Length: 50.0000

Element: Linear

PVI ✓ 99+50.0000 ✓ 1062.8992
PVI ✓ 100+00.0000 ✓ 1062.7017
Tangent Grade: -0.39%
Tangent Length: 50.0000

Element: Linear

PVI 100+00.0000 1062.7017
PVI 100+50.0000 1062.4749
Tangent Grade: -0.45%
Tangent Length: 50.0000

Element: Linear

PVI ✓ 100+50.0000 ✓ 1062.4749
PVI ✓ 101+00.0000 ✓ 1062.2298
Tangent Grade: -0.49%
Tangent Length: 50.0000

Element: Linear

PVI 101+00.0000 1062.2298
PVI 101+50.0000 1061.9666
Tangent Grade: -0.53%
Tangent Length: 50.0000

Element: Linear

PVI ✓ 101+50.0000 ✓ 1061.9666
PVI ✓ 102+00.0000 ✓ 1061.7844
Tangent Grade: -0.36%
Tangent Length: 50.0000

Element: Linear

PVI 102+00.0000 1061.7844
PVI 102+50.0000 1061.6161
Tangent Grade: -0.34%
Tangent Length: 50.0000

Element: Linear

PVI ✓ 102+50.0000 ✓ 1061.6161
PVI ✓ 103+00.0000 ✓ 1061.3864
Tangent Grade: -0.46%
Tangent Length: 50.0000

Element: Linear

CALCULATION SHEET

PROJECT: I-75 / I-575 NORTHWEST CORRIDOR

JOB NUMBER NH000-0073-03(242)

CALC NO. BR#33

SUBJECT: Bridge Survey Shots

BY: JCR

DATE: 11/30/2009

SHEET NO.

SHEET REV.

I-75 over Frey Rd (Existing Right Bridge)						
BENT 1 LEFT SIDE						
SVXA45045	N	1471135.270200	E	2171145.979100	Z	1086.044 TBRDG
"ZEP"						
SVXA45046	N	1471135.243800	E	2171145.910400	Z	1086.042 TBAS
"ZAS553"						
SVXB53557	N	1471135.160500	E	2171146.430200	Z	1086.059 TBRDG
BENT 1 RIGHT SIDE						
SVXA45049	N	1471234.526700	E	2171154.606400	Z	1088.944 TBRDG
"ZEP"						
SVXA45050	N	1471234.770700	E	2171154.506000	Z	1088.950 TBRDG
"ZEP"						
SVXB53545	N	1471235.366400	E	2171154.609600	Z	1089.048 TBRDG
BENT 2 LEFT SIDE						
SVXA45042	N	1471220.064200	E	2171093.372800	Z	1087.413 TBRDG
"ZEJ549"						
BENT 2 RIGHT SIDE						
SVXA45053	N	1471329.249800	E	2171094.585800	Z	1090.448 TBRDG
"ZEJ548"						
BENT 3 LEFT SIDE						
SVXA45039	N	1471323.447600	E	2171026.741700	Z	1089.062 TBRDG
"ZEJ546"						
BENT 3 RIGHT SIDE						
SVXA45056	N	1471428.826000	E	2171027.789100	Z	1091.904 TBRDG
"ZEJ546"						
BENT 4 LEFT SIDE						
SVXA45035	N	1471416.659600	E	2170963.917200	Z	1090.413 TBAS
"ZAS552"						
SVXA45036	N	1471416.566400	E	2170963.941000	Z	1090.384 TBRDG
"ZEP"						
SVXB53616	N	1471416.601600	E	2170963.761800	Z	1090.567 TBRDG
BENT 4 RIGHT SIDE						
SVXA45058	N	1471528.028300	E	2170958.499600	Z	1093.389 TBRDG
"ZEP"						
SVXA45061	N	1471528.052300	E	2170958.412000	Z	1093.320 TBAS
"ZAS552"						
SVXB53632	N	1471528.401800	E	2170958.286500	Z	1093.424 TBRDG

CALCULATION SHEET

PROJECT: I-75 / I-575 NORTHWEST CORRIDOR

JOB NUMBER NH000-0073-03(242)

CALC NO. BR#33

SUBJECT: Existing Bridge Plans

BY: JCR

DATE: 11/30/2009

SHEET NO.

SHEET REV.

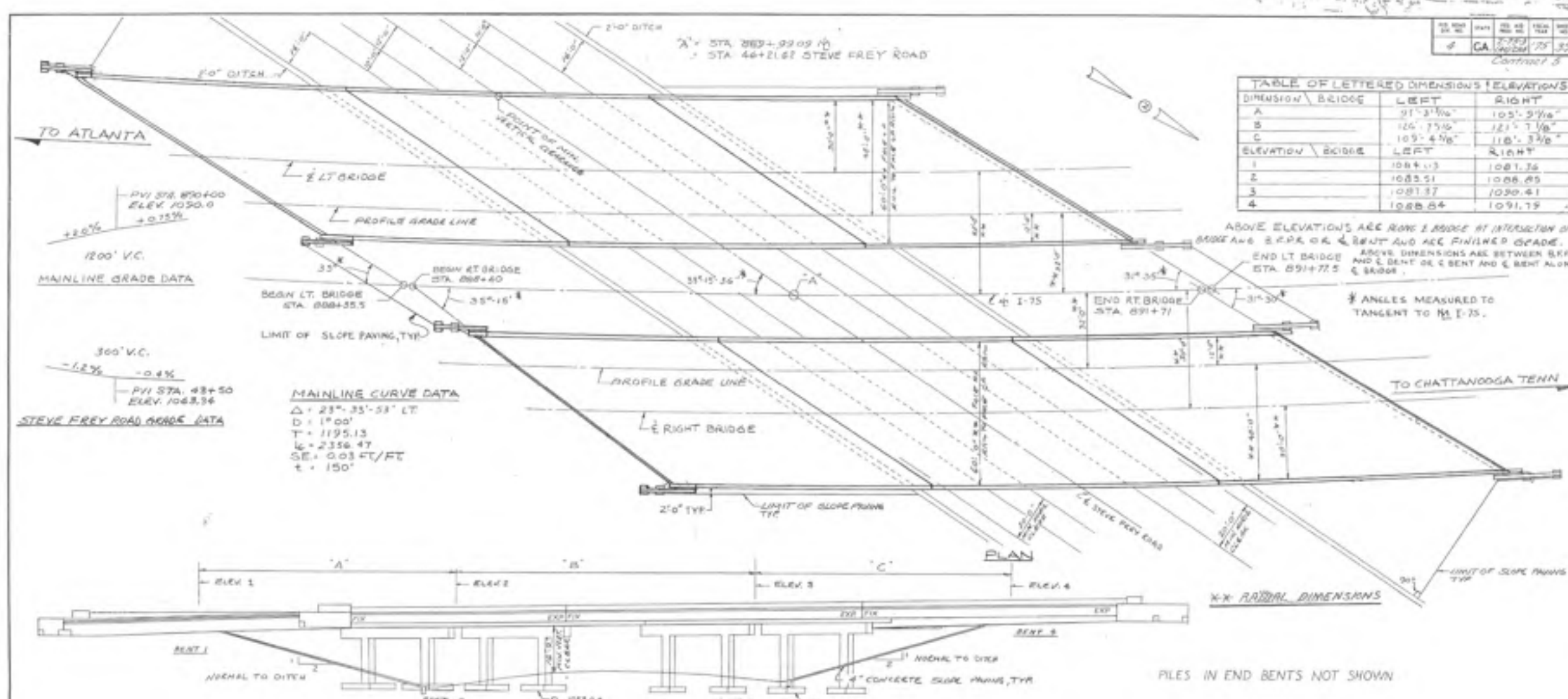


TABLE OF LETTERED DIMENSIONS & ELEVATIONS		
DIMENSION / BRIDGE	LEFT	RIGHT
A	21'-3 1/8"	105'-3 1/8"
B	126'-7 1/2"	121'-7 1/2"
C	109'-4 1/8"	118'-3 1/8"
ELEVATION / BRIDGE	LEFT	RIGHT
1	1084.13	1081.36
2	1083.51	1088.89
3	1081.37	1090.41
4	1088.84	1091.79

ABOVE ELEVATIONS ARE ROW 1 BRIDGE AT INTERSECTION OF E. BRIDGE AND S.F.R. OR E. BENT AND ARE FINISHED GRADE.
 END LT BRIDGE STA. 891+77.5
 END RT BRIDGE STA. 891+71
 * ANGLES MEASURED TO TANGENT TO H.I. 75.

ELEVATION LEFT BRIDGE
 RIGHT BRIDGE SIMILAR

DESIGN DATA
 SPECIFICATIONS - A.A.S.H.O., 1973
 TYPICAL HS20-44 AND/OR MILITARY LOADING - IMPACT ALLOWED
 FUTURE PAVING ALLOWANCE = 15 LBS. PER SQ. FT.
 ALLOWANCE SOIL PRESSURE - SEE SUBSTRUCTURE DETAILS

BRIDGE No 3LT & 3RT.
 GEORGIA
 DEPARTMENT OF TRANSPORTATION
 HIGHWAY DIVISION - BRIDGE DESIGN
 PLAN AND ELEVATION
 I-75 OVER STEVE FREY ROAD
 COBB COUNTY I-75-3 (4) 284-CT5
 SCALE: 1"=20'-0" JULY, 1973

BRIDGE CONSISTS OF

- 3 - SIMPLE COMPOSITE PLATE GIRDER (48" WIDE) SPANS ----- SPECIAL DESIGN
- 2 - CONCRETE END BENTS ----- SPECIAL DESIGN
- 4 - CONCRETE INTERMEDIATE BENTS (SEE SHEET 15) ----- SPECIAL DESIGN
- ALUMINUM HANDRAILING ----- GA. STD. NO. 3626 (M00.1) (8-29-74)
- BAR BENDING DETAILS ----- GA. STD. NO. 3901
- TYPICAL FILL DETAIL AT END OF BRIDGE ----- GA. STD. NO. 9037 (9-1-75)
- END POST AND END POST GUARDRAIL ATTACHMENT DETAILS ----- GA. STD. NO. 9053 (M00.1)

GENERAL NOTES

- SPECIFICATIONS - GEORGIA STANDARD SPEC 1972.
- CHAMFER - ALL EXPOSED EDGES SHALL CHAMFER 3/4" UNLESS OTHERWISE NOTED.
- PROTECTIVE SURFACE TREATMENT - PER SECTION 500.13C WILL BE REQUIRED AT THIS SITE.
- REINFORCEMENT - ALL REINFORCEMENT SHALL BE PLACED AND TIED IN ACCORDANCE WITH THE STANDARD SPECIFICATIONS. WELDING OF REINFORCEMENT WILL NOT BE PERMITTED, EXCEPT AS SHOWN ON THE PLANS.
- DRIVING DATA PILES - ONE REQUIRED AT EACH OF BENTS 1 LT. AND 4 RT.
- PLAN DRIVING OBJECTIVE - SEE SUBSTRUCTURE DETAILS.

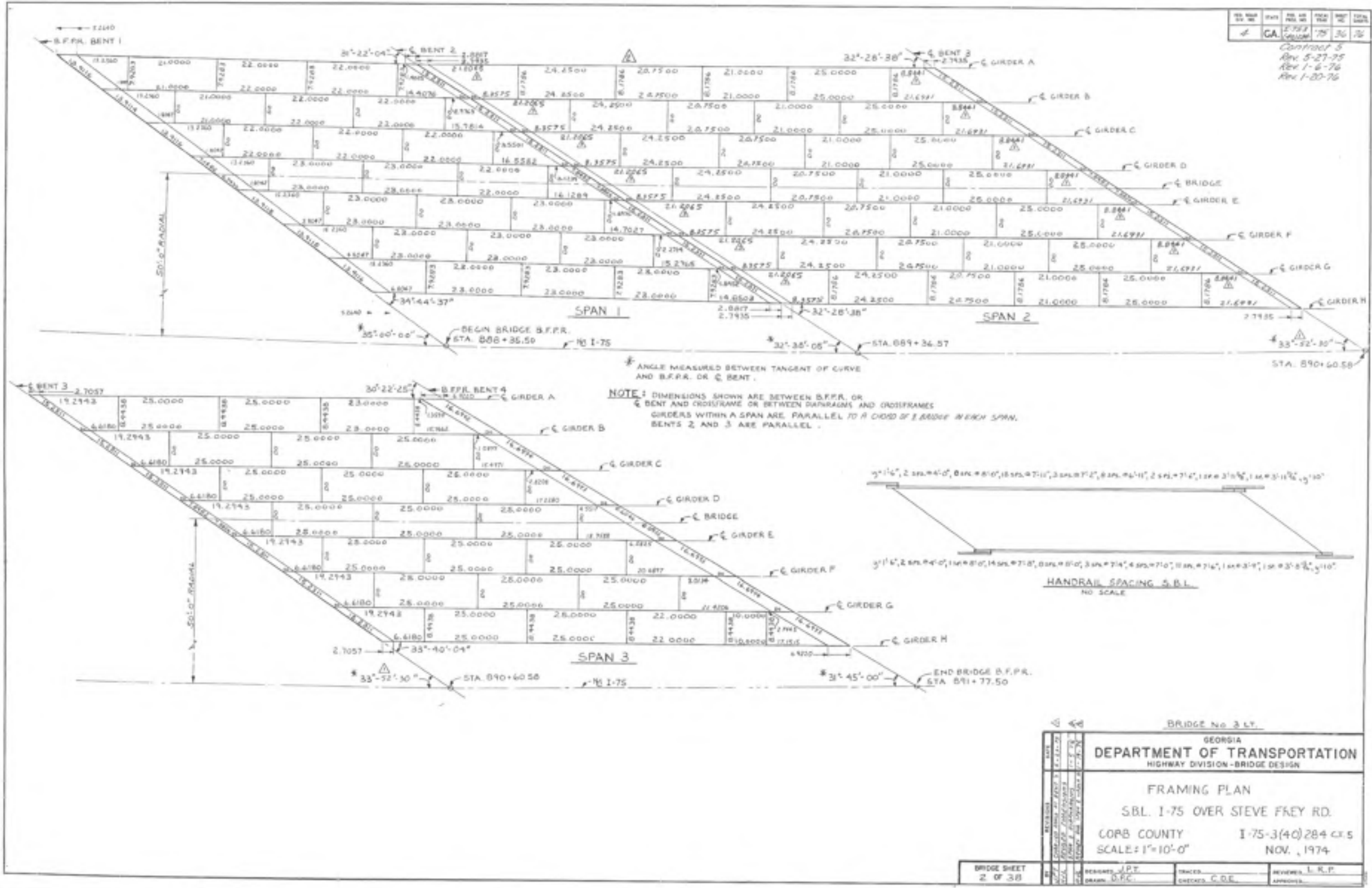
SUMMARY OF QUANTITIES

ITEM	QTY	UNIT	DESCRIPTION
484	573	CU YD	CU TO BR EROSION, GR SEP
413	412	CU YD	CU TO BR INFILL
2,075	2,150	CU YD	CONC SLOPE PSV, 4 IN
LUMP	---	---	SUPERSTR CONC (CL 44) - BR NO 3 LT
---	LUMP	---	SUPERSTR CONC (CL 44) - BR NO 3 RT
607	614	CU YD	CU TO CL & CONC
LUMP	---	---	STR STEEL - BR NO 3 LT
---	LUMP	---	STR STEEL - BR NO 3 RT
96,480	93,486	LB	BAR REINF STEEL
LUMP	---	---	SUPERSTR REINF STEEL - BR NO 3 LT
---	LUMP	---	SUPERSTR REINF STEEL - BR NO 3 RT
446	489	LN FT	ALUM HANDRAIL, STD 3626
1,438	1,937	LN FT	PIILING IN PLACE, STEEL H, 10 BP 42
1	1	---	CRCH LOAD TEST, STEEL H, 10 BP 42 (IF REQD)

BRIDGE SHEET
 1 OF 38

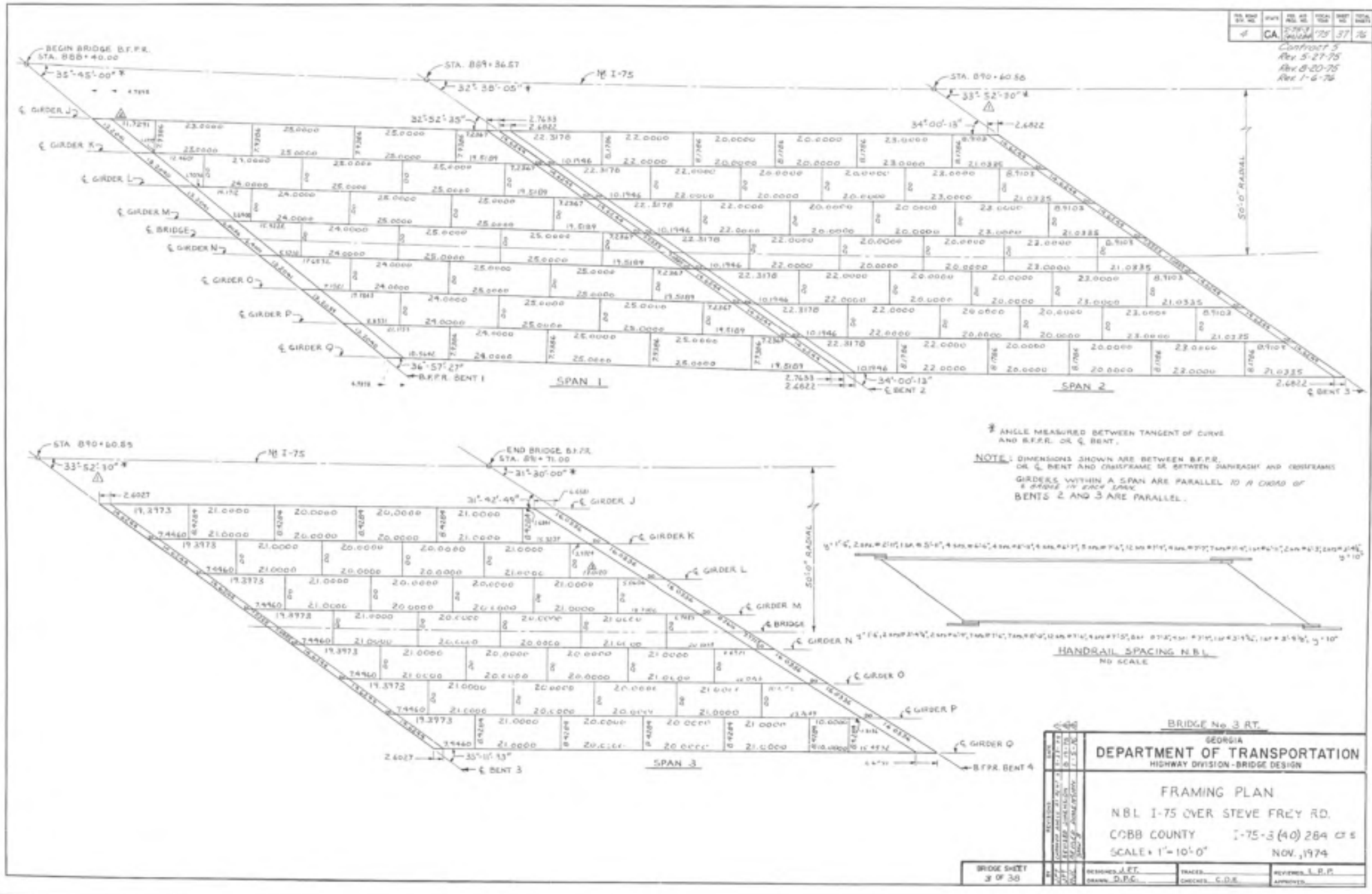
DESIGNED: F.E.H.	TRACED: J.P.T.	REVIEWED: L.R.P.
DRAWN: C.D.E.	CHECKED: J.P.T.	APPROVED: _____

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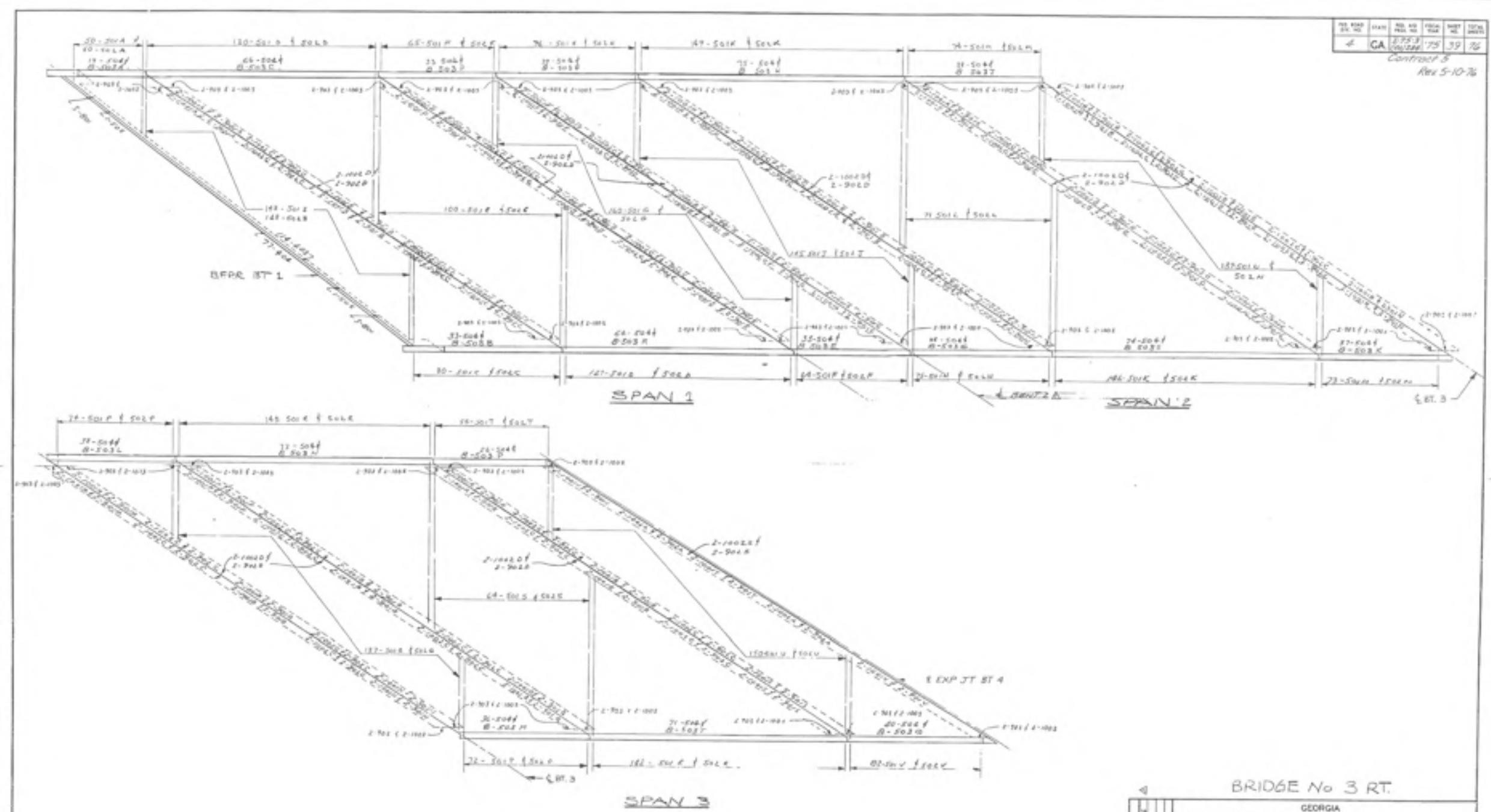


BRIDGE No. 3 LT.	
GEORGIA	
DEPARTMENT OF TRANSPORTATION	
HIGHWAY DIVISION - BRIDGE DESIGN	
FRAMING PLAN	
S.B.L. 1-75 OVER STEVE FREY RD.	
CORB COUNTY	
I-75-3(40)284 CX 5	
SCALE: 1"=10'-0"	
NOV. 1974	
BRIDGE SHEET	2 OF 38
DESIGNED: J.P.T.	TRACED: C.R.E.
DRAWN: D.F.C.	APPROVED: L.R.P.

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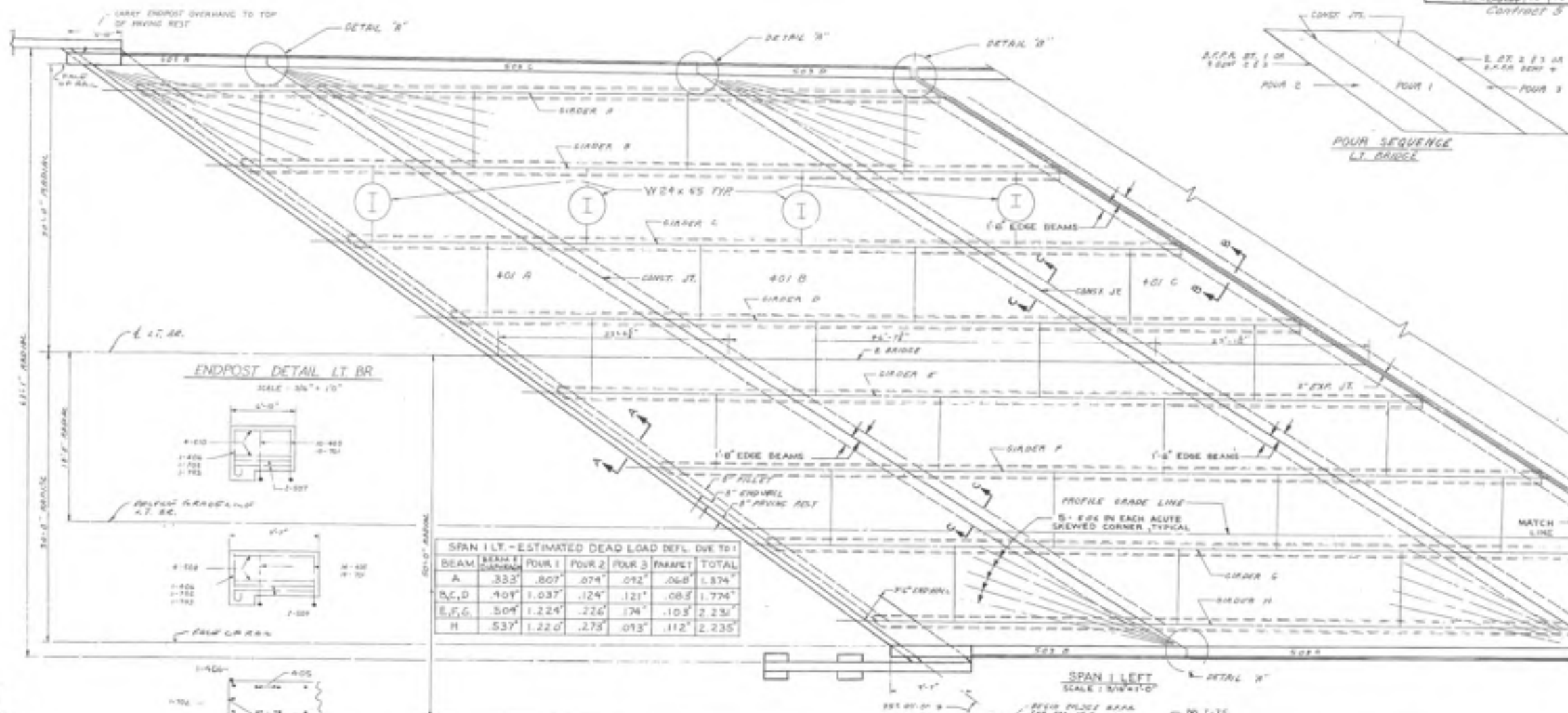
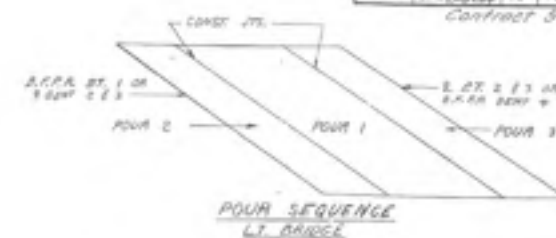
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BRIDGE No 3 RT.		
GEORGIA		
DEPARTMENT OF TRANSPORTATION		
HIGHWAY DIVISION-BRIDGE DESIGN		
SUPERSTRUCTURE REINFORCING		
N.B.L. I-75 OVER STEVE FREY RD.		
COBB COUNTY T-75-3 (+) 28+00		
NO SCALE JULY 1973		
BRIDGE SHEET 5 OF 38	DESIGNED: FEH CHECKED: C.D.E.	TRACED: J.A.T. APPROVED: L.R.B.

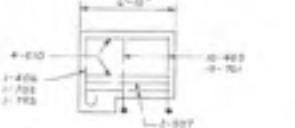
NO.	DATE	BY	CHKD.	APPD.	REMARKS
1	CA	1-75	1-75	40	75

Contract 5



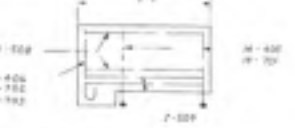
ENDPOST DETAIL LT BR

SCALE - 3/8" = 1'-0"



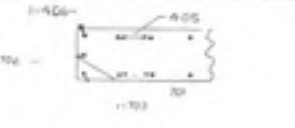
ENDPOST DETAIL LT BR

SCALE - 3/8" = 1'-0"



ENDPOST DETAIL LT BR

SCALE - 3/8" = 1'-0"



ENDPOST DETAIL LT BR

SCALE - 3/8" = 1'-0"



ENDPOST DETAIL LT BR

SCALE - 3/8" = 1'-0"



ENDPOST DETAIL LT BR

SCALE - 3/8" = 1'-0"

HALF SECTION @ END BENT 1

LOOKING BACK

SCALE - 3/8" = 1'-0"

BRIDGE NO. 3 LT - RT.

GEORGIA
DEPARTMENT OF TRANSPORTATION
HIGHWAY DIVISION-BRIDGE DESIGN

SUPERSTRUCTURE DETAILS SHEET NO. 1

SBL I-75 OVER STEVE FLY RD.

COBB CO.

I-75-314012B4C1

SCALE AS SHOWN

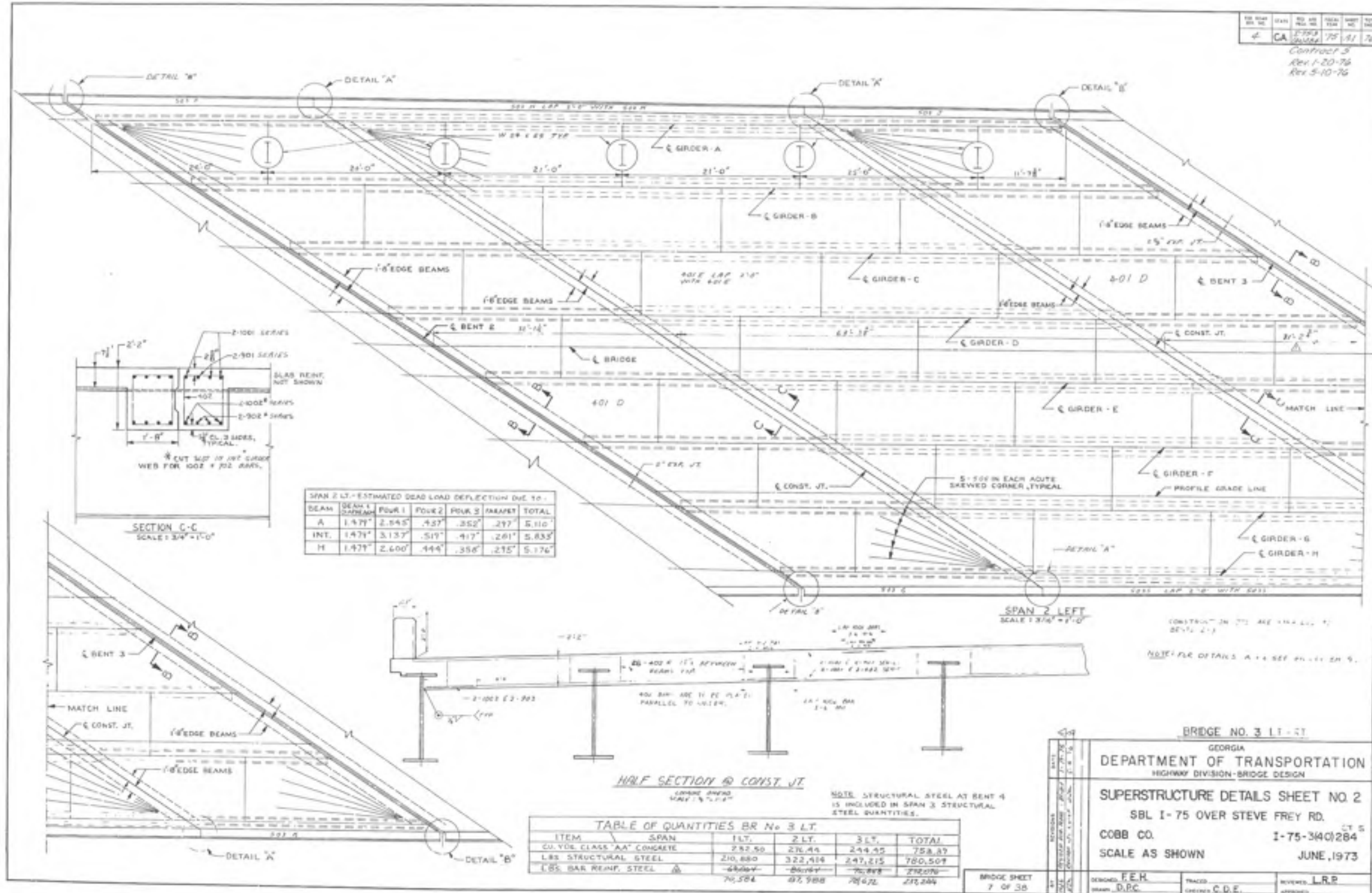
JUNE, 1973

BRIDGE SHEET
6 OF 30

DESIGNED: FEN
CHECKED: CDE
REVIEWED: LRP
APPROVED:

NO.	DATE	BY	CHKD.	APPD.	TOTAL
1	CA	1-20-76	75	1	76

Contract 3
Rev. 1-20-76
Rev. 5-10-76



BRIDGE NO. 3 LT-RT

GEORGIA
DEPARTMENT OF TRANSPORTATION
HIGHWAY DIVISION-BRIDGE DESIGN
SUPERSTRUCTURE DETAILS SHEET NO. 2
SBL I-75 OVER STEVE FREY RD.
COBB CO. I-75-340/284
SCALE AS SHOWN JUNE, 1973

BRIDGE SHEET
7 OF 38

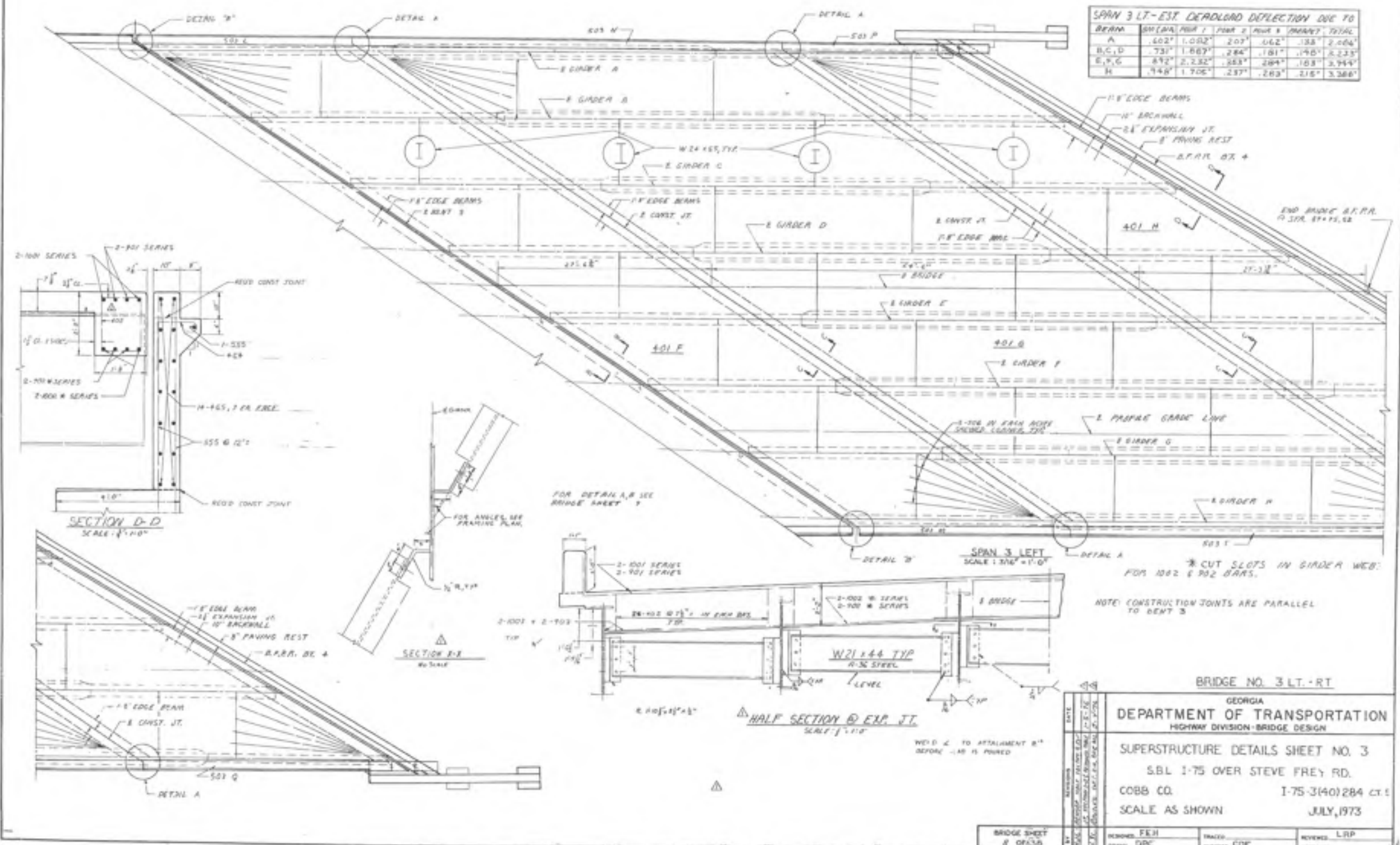
DESIGNED: F.E.H.
CHECKED: D.P.C.
TRACED: C.D.E.
REVIEWED: L.R.P.

Rev. 1-6-76
Rev. 5-10-76

NO.	REV.	DATE	BY	CHKD.	APP'D.
1	CA	5-10-76	75	42	76

SPAN 3 LT-EST DEADLOAD DEFLECTION DUE TO

BEAM	SPAN 1	SPAN 2	SPAN 3	TOTAL
A	.602"	1.002"	.207"	.811"
B,C,D	.731"	1.667"	.284"	2.682"
E,F,G	.872"	2.232"	.284"	3.388"
H	.948"	1.705"	.237"	2.890"



* CUT SLOTS IN GIRDER WEB:
FOR 1002 & 902 BARS.

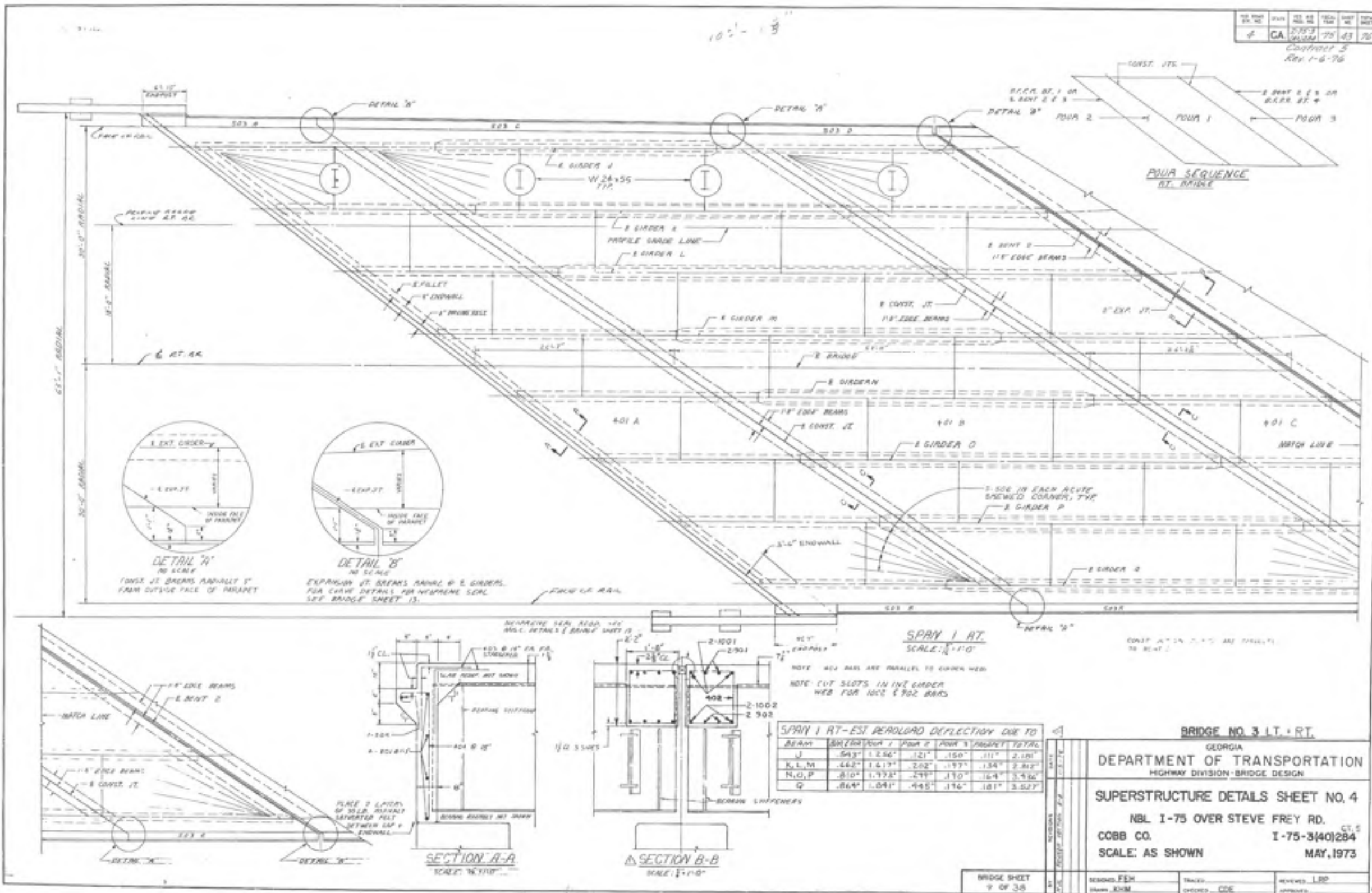
NOTE: CONSTRUCTION JOINTS ARE PARALLEL
TO BENT 3

BRIDGE NO. 3 LT-RT

GEORGIA
DEPARTMENT OF TRANSPORTATION
HIGHWAY DIVISION-BRIDGE DESIGN

SUPERSTRUCTURE DETAILS SHEET NO. 3
S.B.L. 1-75 OVER STEVE FREY RD.
COBB CO. I-75 (140) 284 CT. 1
SCALE AS SHOWN JULY, 1973

BRIDGE SHEET 8 OF 10	DESIGNED: FEH CHECKED: DPC	TRACED: CHECKED: SDE	REVIEWED: LRP APPROVED:
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SPAIN I RT-EST READLOAD DEFLECTION DUE TO						
Beam	SPAIN I	SPAIN I	SPAIN I	SPAIN I	SPAIN I	TOTAL
J	54.3	1.256	121	150	111	2.181
K, L, M	44.3	1.113	262	177	134	2.182
N, O, P	81.0	1.772	477	170	164	3.166
Q	86.6	1.041	445	176	181	3.52

NO.	DATE	BY	CHKD	APPD	REVISION
1	CA	2/7/73	7/5	44	76
Contract 5					
Rev 5-10-76					

SPRAY 2 RT-EST. DEADLOAD DEFLECTION DUE TO

BEAM	BM (IN) OVER 1	SPAN 2	SPAN 3	PARAPET TOTAL
J	1.254"	2.163"	37"	2.19"
INT.	1.256"	2.444"	441"	354"
Q	1.256"	2.222"	37"	304"

TABLE OF QUANTITIES BR. No. 3 RT.

ITEM	SPRAY	1 RT.	2 RT.	3 RT.	TOTAL
CU. YDS. CLASS A CONCRETE		250.19	265.92	257.60	774.01
LBS. STRUCTURAL STEEL		235,318	312,209	304,924	852,446
LBS. BAR ADHESIVE STEEL		74,447	81,905	86,988	243,340

NOTE: STRUCTURAL STEEL RT BENT 4 IS INCLUDED IN SPAN 3 STRUCTURAL STEEL QUANTITIES

NOTE: FOR S&I E 502 BAR DESIGNATION SEE BRIDGE SHEET 6.

* RAILROAD DIMENSIONS

NOTE: CENTERLINE JOINTS ARE 11' 11" TO BENT 2 AT 1/2

HALF SECTION @ MIDSPAN
LOOKING AHEAD
SCALE: 1/4"=1'-0"
LT. BRIDGE SIMILAR

BRIDGE NO. 3 LT-RT.

GEORGIA
DEPARTMENT OF TRANSPORTATION
HIGHWAY DIVISION-BRIDGE DESIGN

SUPERSTRUCTURE DETAILS SHEET NO. 5

NBL I-75 OVER STEVE FREY RD.

COBB CO. I-75-3(40)284

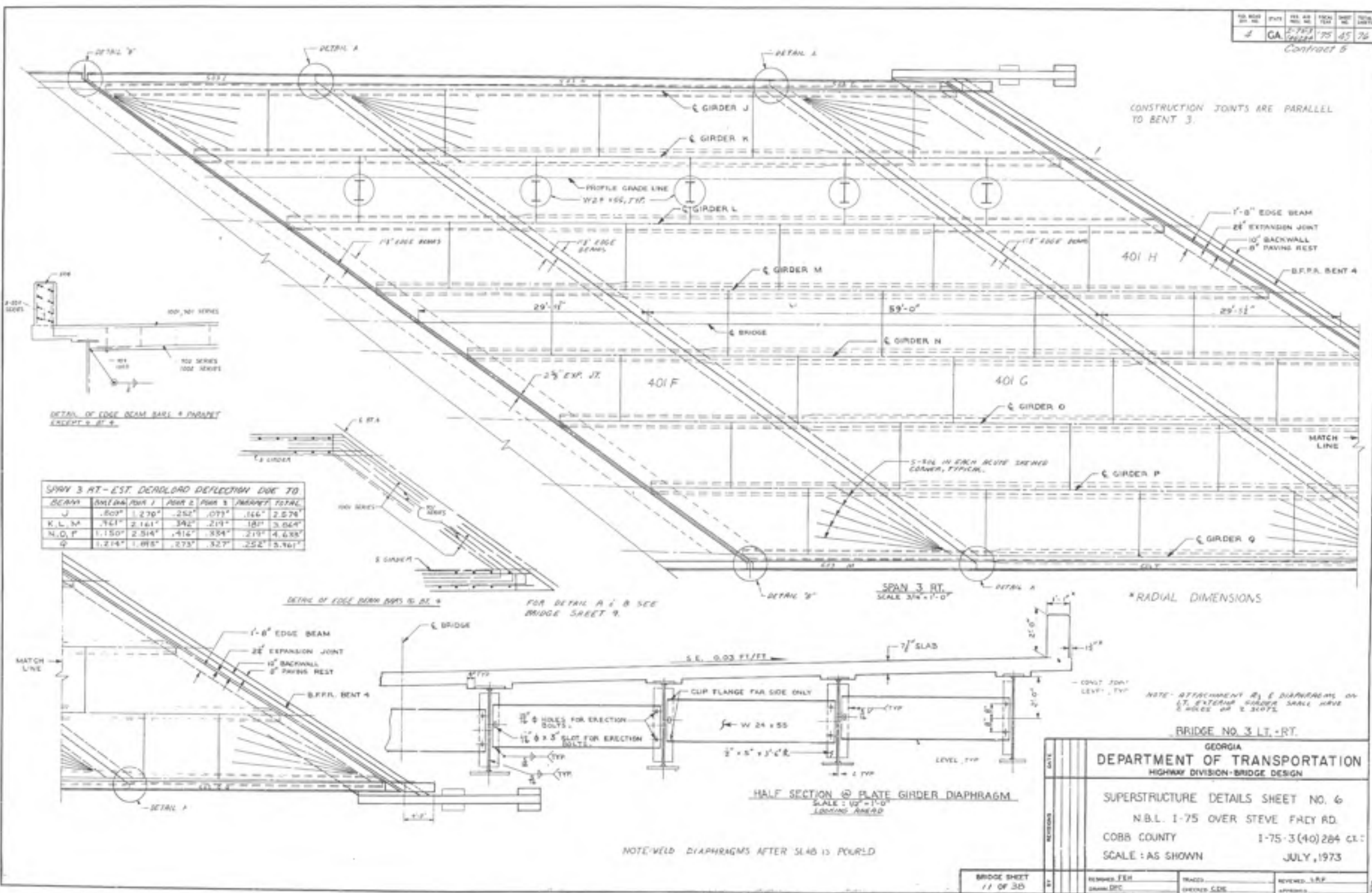
SCALE AS SHOWN MAY, 1973

BRIDGE SHEET
78 OF 30

DESIGNED: FEH
CHECKED: CDE
REVIEWED: LRP
APPROVED:

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TO	BY	DATE	REVISION
GA	GA	75	65
Contract 5			



SPRAY 3 RT. - EST. DEADLOAD DEFLECTION DUE TO

BEAM	SPAN 1	SPAN 2	SPAN 3	SPAN 4	TOTAL
J	.809"	1.270"	.252"	.073"	2.576"
K, L, M	.741"	2.161"	.342"	.219"	3.664"
N, O, P	1.150"	2.514"	.416"	.354"	4.635"
Q	1.214"	1.698"	.273"	.327"	3.961"

BRIDGE NO. 3 LT. RT.

GEORGIA
DEPARTMENT OF TRANSPORTATION
HIGHWAY DIVISION-BRIDGE DESIGN

SUPERSTRUCTURE DETAILS SHEET NO. 6
N.B.L. 1-75 OVER STEVE FACY RD.
COBB COUNTY 1-75-3(40)284 CL.
SCALE: AS SHOWN JULY, 1973

BRIDGE SHEET 11 OF 35	DESIGNED BY DANIEL D. C.	TRACED CHECKED C.D.	REVIEWED S.B.P.
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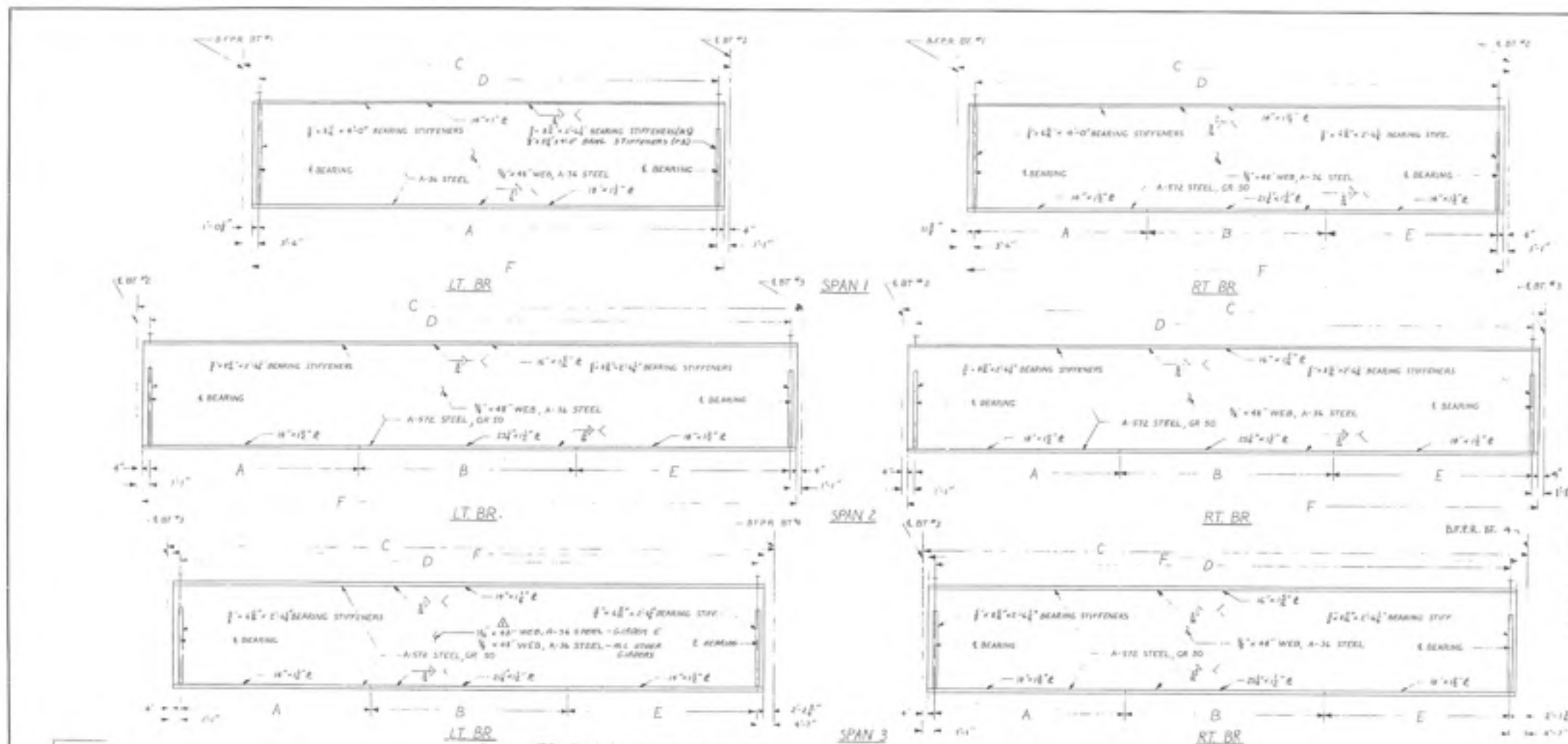
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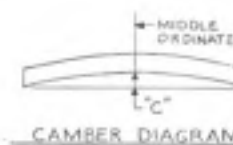
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BRIDGE NO.	SPAN	SECTION	DATE	BY	CHKD.
4	GA	179	46	76	

Contract 3
Rev. 1-6-76



CAMBER DIAGRAM

TABLE OF "C"			
BRIDGE NO.	SPAN	SECTION	DATE
4	GA	179	46
5	GA	179	46
6	GA	179	46
7	GA	179	46
8	GA	179	46
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11	GA	179	46
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94	GA	179	46
95	GA	179	46
96	GA	179	46
97	GA	179	46
98	GA	179	46
99	GA	179	46
100	GA	179	46

NOTE: ABOVE CAMBER INCLUDES WEIGHT OF GIRDER, SLAB, COPING, PARAPET, AND HANDRAILING.

TABLE OF LETTERED DIMENSIONS

LT. BRIDGE	RT. BRIDGE	SPAN	SECTION	DATE	BY	CHKD.
4	GA	179	46	76		
5	GA	179	46	76		
6	GA	179	46	76		
7	GA	179	46	76		
8	GA	179	46	76		
9	GA	179	46	76		
10	GA	179	46	76		
11	GA	179	46	76		
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13	GA	179	46	76		
14	GA	179	46	76		
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31	GA	179	46	76		
32	GA	179	46	76		
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35	GA	179	46	76		
36	GA	179	46	76		
37	GA	179	46	76		
38	GA	179	46	76		
39	GA	179	46	76		
40	GA	179	46	76		
41	GA	179	46	76		
42	GA	179	46	76		
43	GA	179	46	76		
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45	GA	179	46	76		
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95	GA	179	46	76		
96	GA	179	46	76		
97	GA	179	46	76		
98	GA	179	46	76		
99	GA	179	46	76		
100	GA	179	46	76		

NOTE: 1. ALL GIRDER WEBS AND BOTTOM FLANGES ARE WELD LOAD CARRYING MEMBER COMPONENTS. ALL "C" TENSILE STRENGTH SHALL MEET THE CHARTERED SECTION 1001 REQUIREMENTS AS SPECIFIED BY THE SPECIAL PROVISIONS SUPPLEMENTING SECTION 1001 OF THE STANDARD SPECIFICATIONS.

NOTE: 2. ALL GIRDER WEBS AND BOTTOM FLANGES SHALL BE THE SAME DESIGNATION AND IN THE ELEVATION VIEW OF THE GIRDER ALL DIMENSIONS SHALL BE AS SHOWN IN THIS DETAIL.

NOTE: 3. ALL GIRDER WEBS AND BOTTOM FLANGES SHALL BE THE SAME DESIGNATION AND IN THE ELEVATION VIEW OF THE GIRDER ALL DIMENSIONS SHALL BE AS SHOWN IN THIS DETAIL.

NOTE: 4. FOR DETAILS OF CONNECTION PLATES, SEE ADDITIONAL SHEET.

BRIDGE NO. 179-46

GEORGIA
DEPARTMENT OF TRANSPORTATION
HIGHWAY DIVISION-BRIDGE DESIGN

STRUCTURAL STEEL DETAILS
NBL & SBL OVER STEVE FREY RD
COBB COUNTY I-75-3(40) 284 CT 6
NO. 5.4E NOVEMBER, 1974

BRIDGE SHEET 12 OF 38	DESIGNED BY TWO	TRACED BY TWO	CHECKED BY TWO	REVIEWED BY TWO
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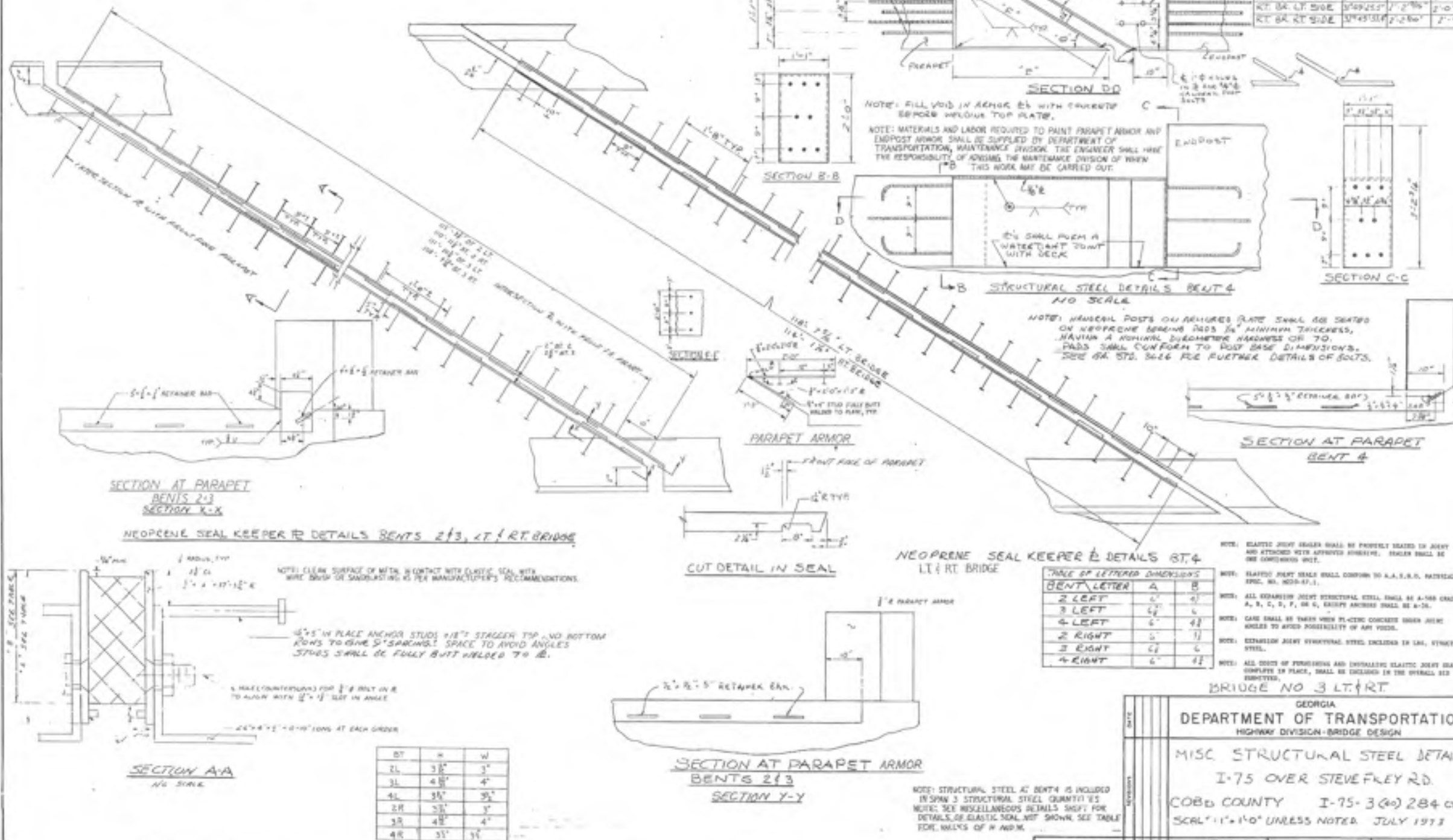
NOTE: PARAPET ARMOR IS REQD. AT ALL CORNERS AND EXPANSION JOINTS IN ARMS CORNERS

NOTE: STEEL IV'S USED TO ARMOR ELDS OF PARAPET END POST SHALL BE AT LEAST A-36

* FILL WITH WELD AND GRIND SMOOTH

NO.	REV.	BY	DATE	REASON
1	GA	7/75	47	76

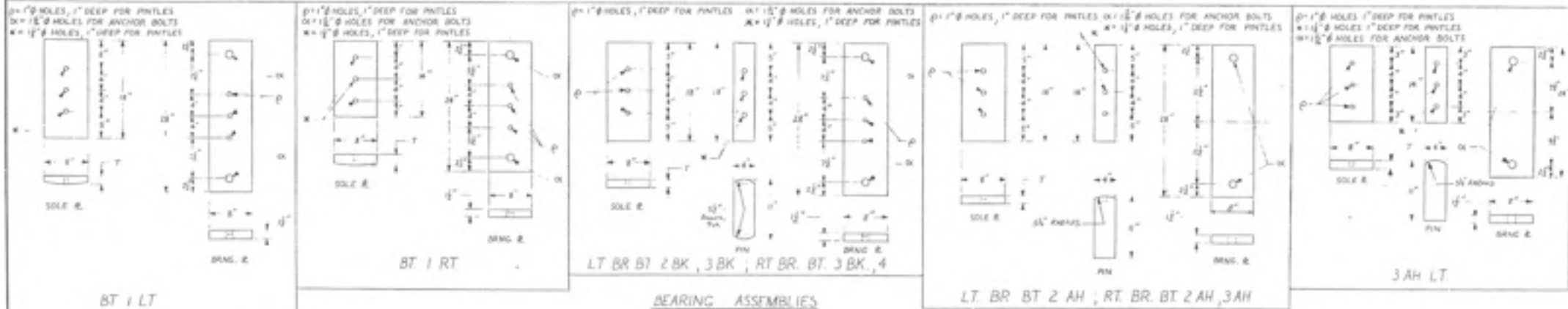
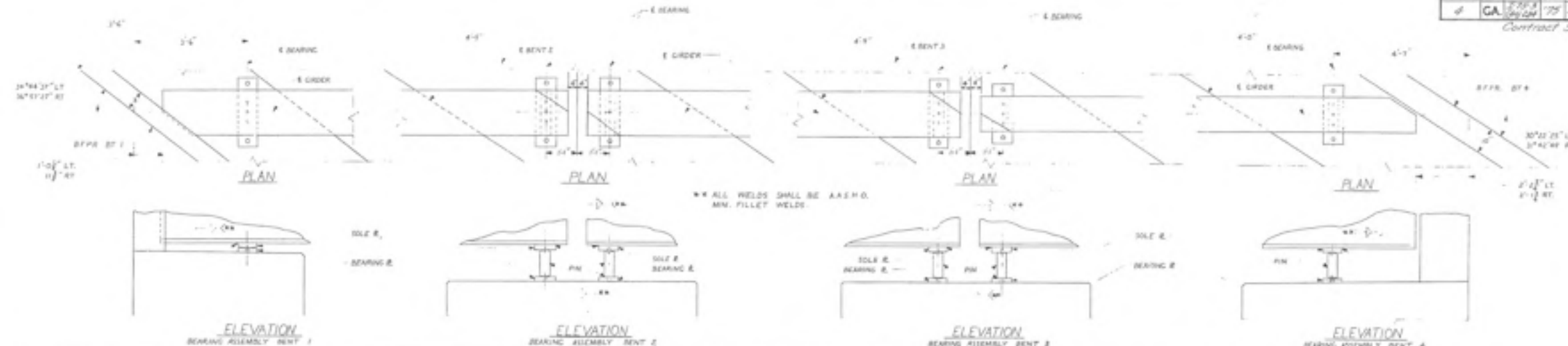
LOCATION, DIM.	Q	R	P
LT. BE. LT. SIDE	30'6" x 40"	2'-3 1/2"	2'-1 1/2"
LT. BE. RT. SIDE	37'2 1/2" x 27"	2'-7 1/4"	2'-0 1/2"
RT. BE. LT. SIDE	37'4 1/2" x 27"	2'-7 1/4"	2'-0 1/2"
RT. BE. RT. SIDE	37'4 1/2" x 27"	2'-7 1/4"	2'-0 1/2"



BT	H	W
2L	3 1/2"	3"
3L	4 1/2"	4"
4L	5 1/2"	5"
2R	3 1/2"	3"
3R	4 1/2"	4"
4R	5 1/2"	5"

NO.	DATE	BY	CHKD	APP'D	REVISION
1	11/15/74	J. H. P.			1

Contract 5



NOTE: ALL ANCHOR BOLTS SHALL BE 1/2" DIA. 4744 HEX NUT AND 1/2" x 1/2" E WALKER ANCHOR BOLT SHALL BE SET IN CONCRETE.

NOTE: PINTLE DETAILS SEE SIDE ELEVATION SHEET.

NOTE: RADIUS FOR ALL CURVED SOLE PLATES IS 1/8".

NOTE: ALL STEEL ELEMENTS OF BEARING ASSEMBLY SHALL BE A572M (EQUIV. A 36).

T DIMENSIONS													
LT BR							RT BR						
ORDER	BT	1	2 BK	2 AH	3 BK	3 AH	ORDER	BT	1	2 BK	2 AH	3 BK	3 AH
A	1/4"	1/4"	1/4"	1/4"	1/4"	1/4"	7	1/4"	1/4"	1/4"	1/4"	1/4"	1/4"
B	2"	2"	2"	2"	2"	2"	8	1/4"	1/4"	1/4"	1/4"	1/4"	1/4"
C	2 1/2"	2 1/2"	2 1/2"	2 1/2"	2 1/2"	2 1/2"	9	1/4"	1/4"	1/4"	1/4"	1/4"	1/4"
D	2"	2"	2"	2"	2"	2"	10	1/4"	1/4"	1/4"	1/4"	1/4"	1/4"
E	2 1/2"	2 1/2"	2 1/2"	2 1/2"	2 1/2"	2 1/2"	11	1/4"	1/4"	1/4"	1/4"	1/4"	1/4"
F	2 1/2"	2 1/2"	2 1/2"	2 1/2"	2 1/2"	2 1/2"	12	1/4"	1/4"	1/4"	1/4"	1/4"	1/4"
G	2 1/2"	2 1/2"	2 1/2"	2 1/2"	2 1/2"	2 1/2"	13	1/4"	1/4"	1/4"	1/4"	1/4"	1/4"
H	2 1/2"	2 1/2"	2 1/2"	2 1/2"	2 1/2"	2 1/2"	14	1/4"	1/4"	1/4"	1/4"	1/4"	1/4"

BR NC 3 L AND 3 RT

GEORGIA
DEPARTMENT OF TRANSPORTATION
HIGHWAY DIVISION-BRIDGE DESIGN

BEARING DETAILS

NO. 1034 L & R STEVE FREY PCAL

COBB COUNTY I-75-3440 284 CT. 5

NO SCALE NOVEMBER 1974

DESIGNED: JET	CHECKED: J. H. P.	REVIEWED: J. H. P.
DRAWN: JET	CHECKED: J. H. P.	APPROVED:

BRIDGE SHEET
19 OF 35

REV	DATE	BY	CHK	APP	REMARKS
4	CA	J.P.T.	J.P.T.	J.P.T.	Contract 3 Rev. 5-27-75

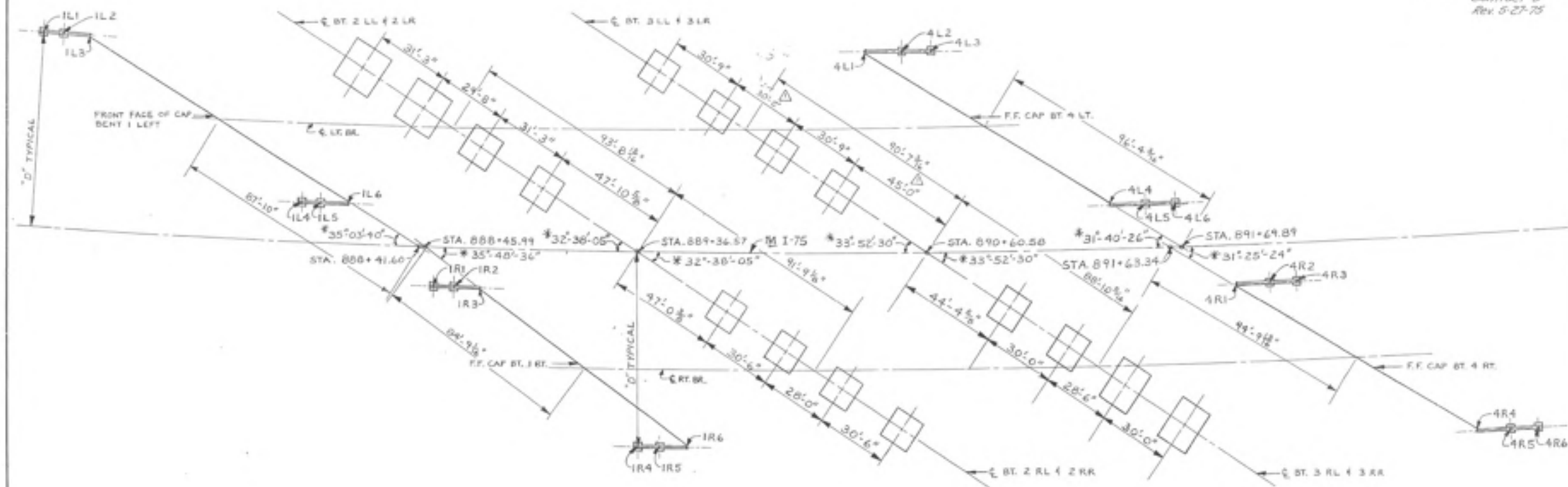


TABLE OF STATIONS AND "D" (NOTE: ALL DIMENSIONS "D" ARE RADIAL)

POINT	IL1	IL2	IL3	IL4	IL5	IL6	4L1	4L2	4L3	4L4	4L5	4L6
STATION	887+01.14	887+09.51	887+21.94	887+34.56	888+02.83	888+15.12	890+53.16	890+18.76	890+61.06	891+39.75	891+55.17	891+67.34
"D"	82'-0 1/2"	82'-0 1/2"	81'-6 1/2"	17'-11 1/2"	17'-11 1/2"	18'-5 1/2"	81'-6 1/2"	82'-0 1/2"	82'-0 1/2"	18'-5 1/2"	17'-11 1/2"	17'-11 1/2"
POINT	IR1	IR2	IR3	IR4	IR5	IR6	4R1	4R2	4R3	4R4	4R5	4R6
STATION	888+51.47	888+59.70	888+71.41	889+34.24	889+44.28	889+55.96	891+93.32	892+08.02	892+19.44	892+52.55	893+07.09	893+18.43
"D"	17'-11 1/2"	17'-11 1/2"	18'-5 1/2"	82'-0 1/2"	82'-0 1/2"	81'-6 1/2"	18'-5 1/2"	17'-11 1/2"	17'-11 1/2"	81'-6 1/2"	82'-0 1/2"	82'-0 1/2"

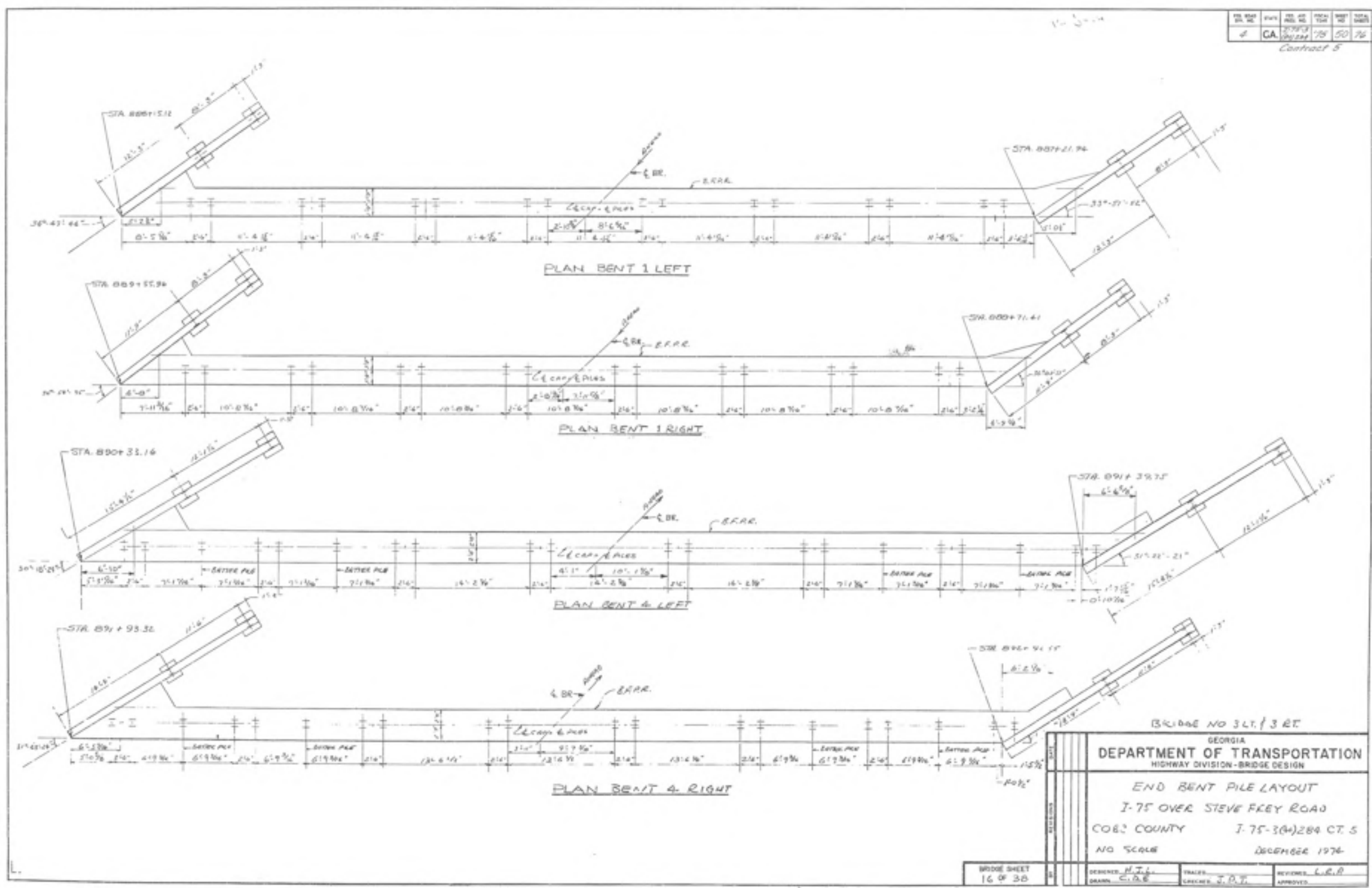
* ANGLES ARE MEASURED BETWEEN FRONT FACE OF CAP OR BENT AND TANGENT TO M AT POINT OF INTERSECTION.

NOTE: BENTS 2 AND 3 ARE PARALLEL.

BRIDGE No. 3LT. & 3RT.

GEORGIA
DEPARTMENT OF TRANSPORTATION
HIGHWAY DIVISION-BRIDGE DESIGN
SUBSTRUCTURE LAYOUT SHEET
I-75 OVER STEVE FREY ROAD
COLS COUNTY I-75-3(40)284 CT 5
SCALE: 1"=20'-0" FEB, 1975

BRIDGE SHEET 15 OF 38	DESIGNED: H.J.L. DRAWN: D.P.C.	CHECKED: J.P.T.	APPROVED: L.R.P.
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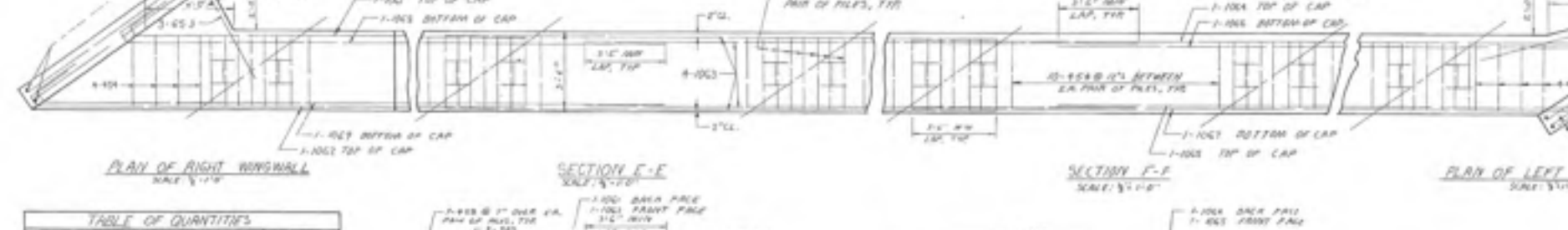
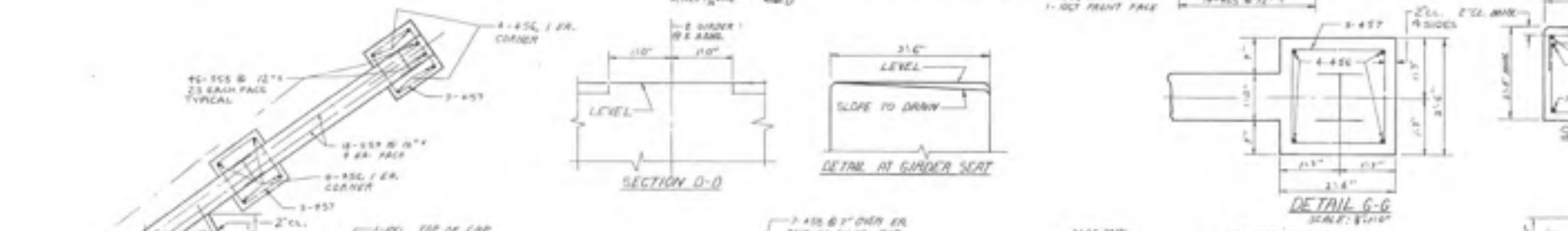
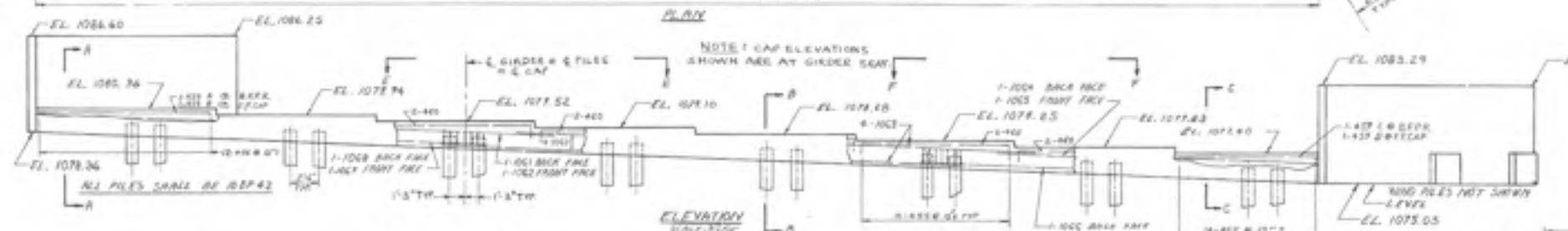
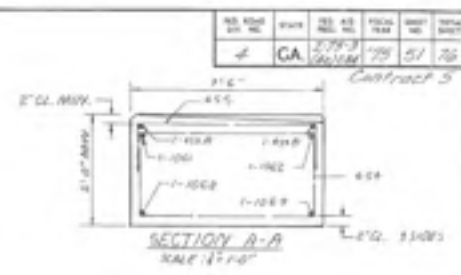
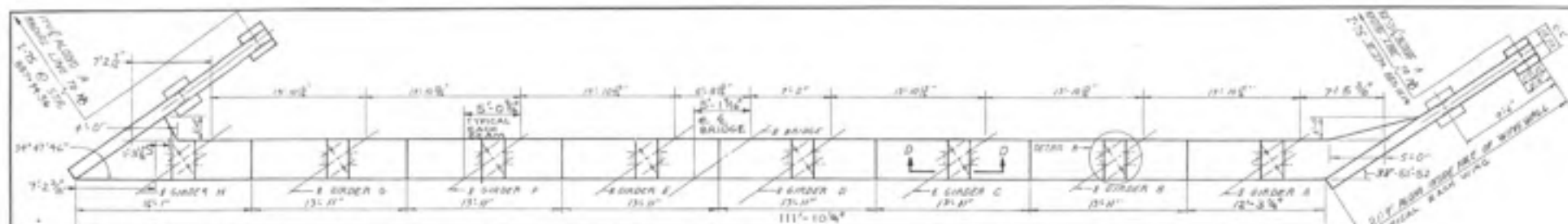
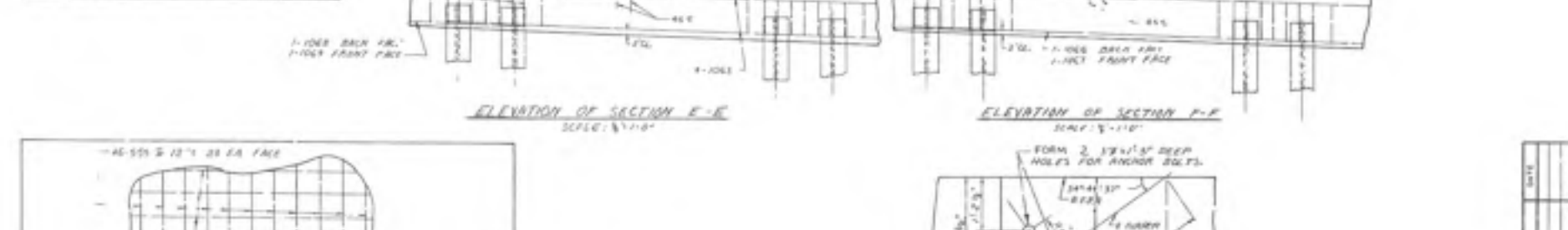


TABLE OF QUANTITIES	
CU 205 CLASS "A" CONCRETE	46.29
185 BARS REINFORCEMENT STEEL	5.00



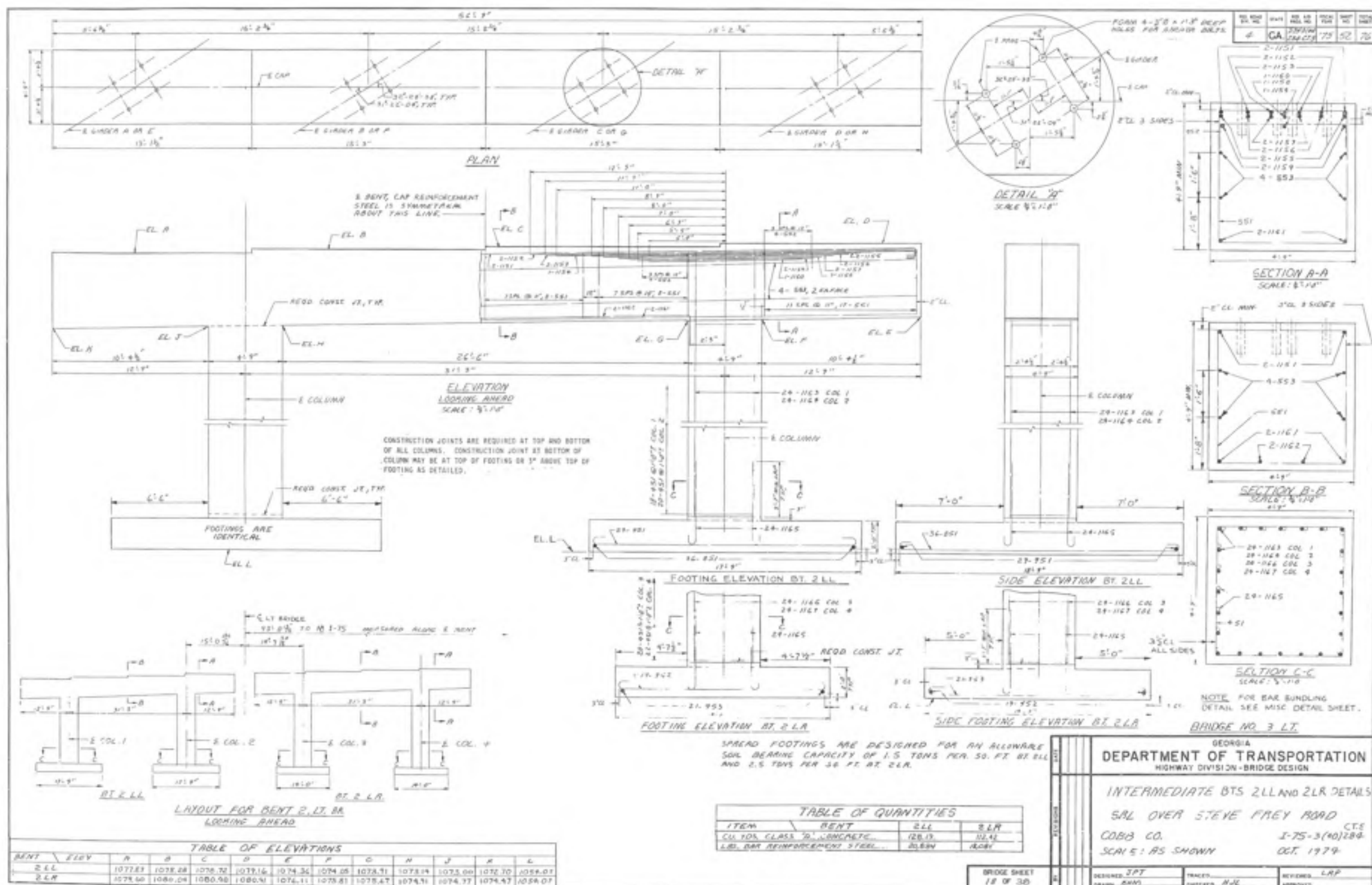
PLAN DRIVING OBJECTIVE
PLAN DRIVING OBJECTIVE SHALL BE A DRIVING
RESISTANCE OF 45 TONS AFTER A MIN
THE ELEVATION OF 1045 IS REACHED.

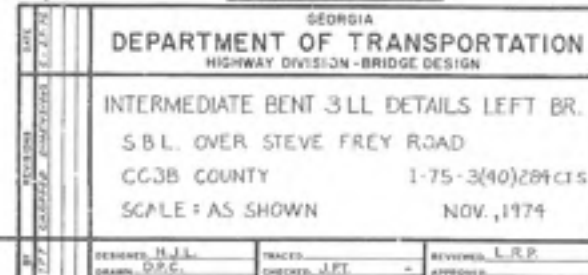
BRIDGE NO. 3 LT.
GEORGIA
DEPARTMENT OF TRANSPORTATION
HIGHWAY DIVISION-BRIDGE DESIGN
BENT 1 LT. BR. DETAILS
SBL OVER STEVE FREY RD.
COBB COUNTY I-75-3(40)284
SCALE AS SHOWN JULY 1973

DATE	REVISION	BY	CHKD	APPD

BRIDGE SHEET
17 OF 38

DESIGNED: P.E.M.	TRACED: C.D.E.	REVIEWED: L.R.P.
DRAWN: A.H.M.	CHECKED: C.D.E.	APPROVED:





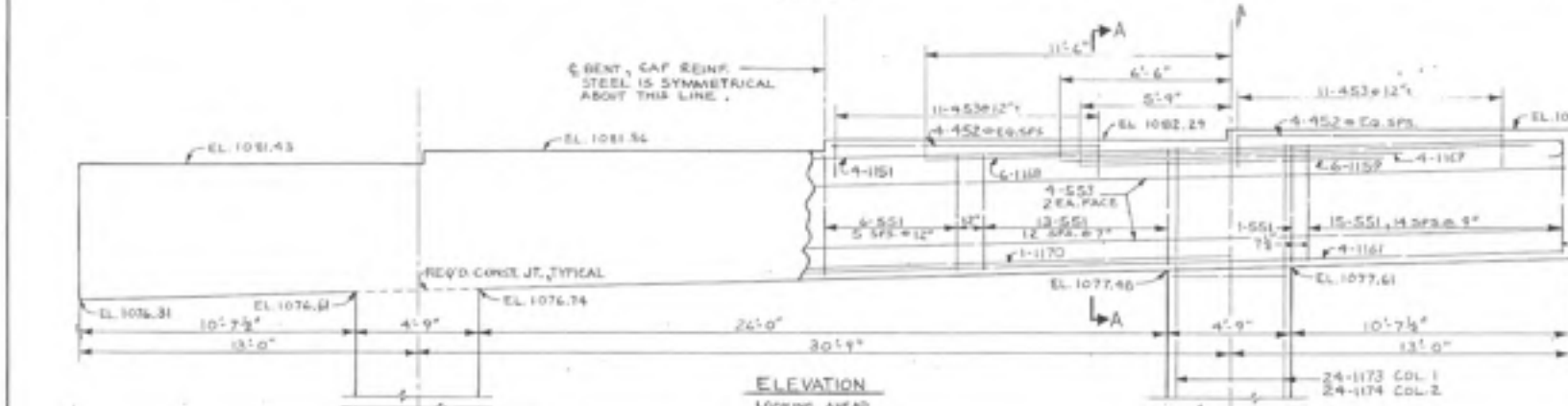
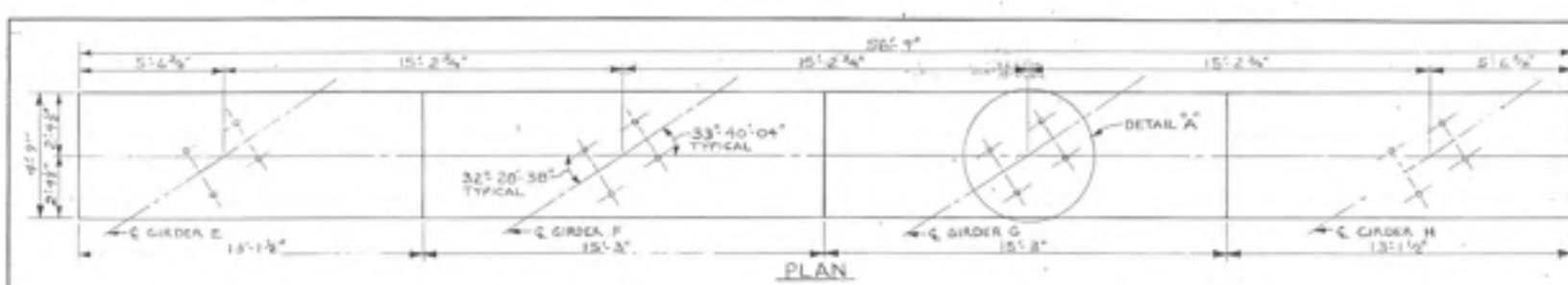
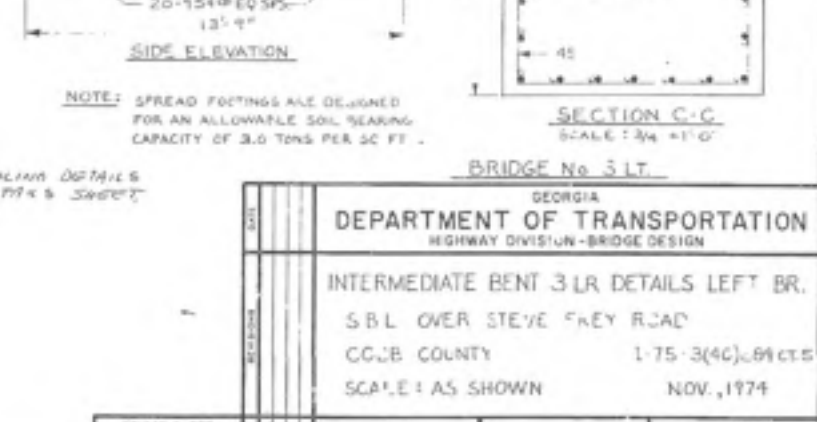
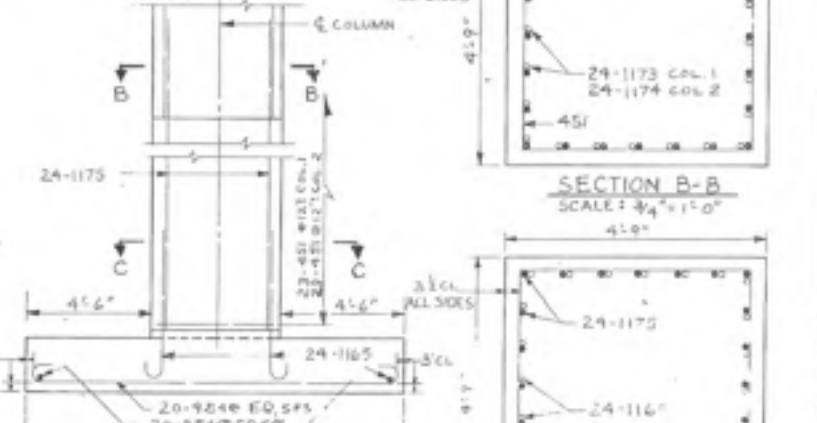
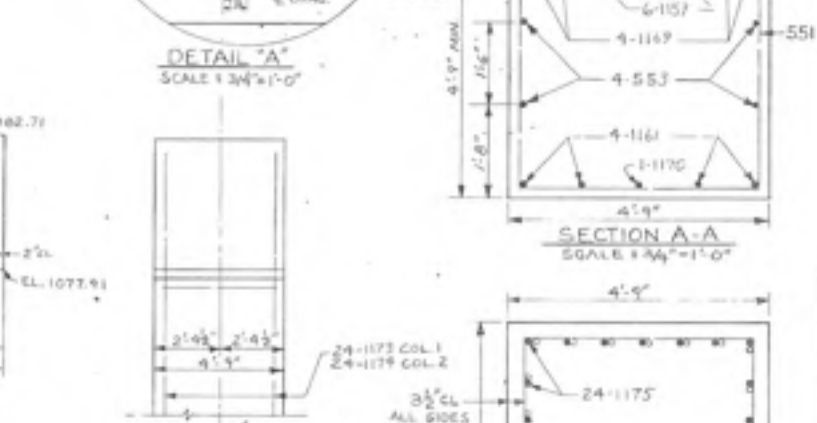
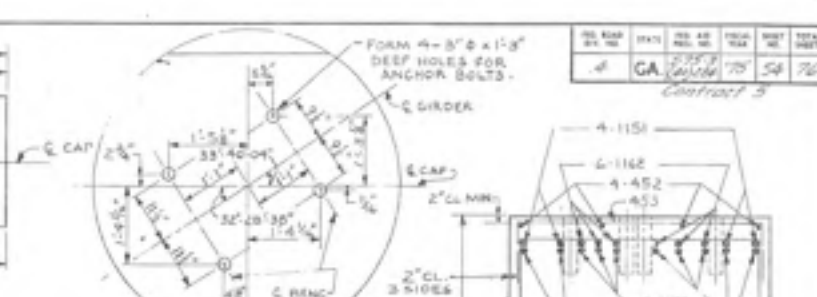
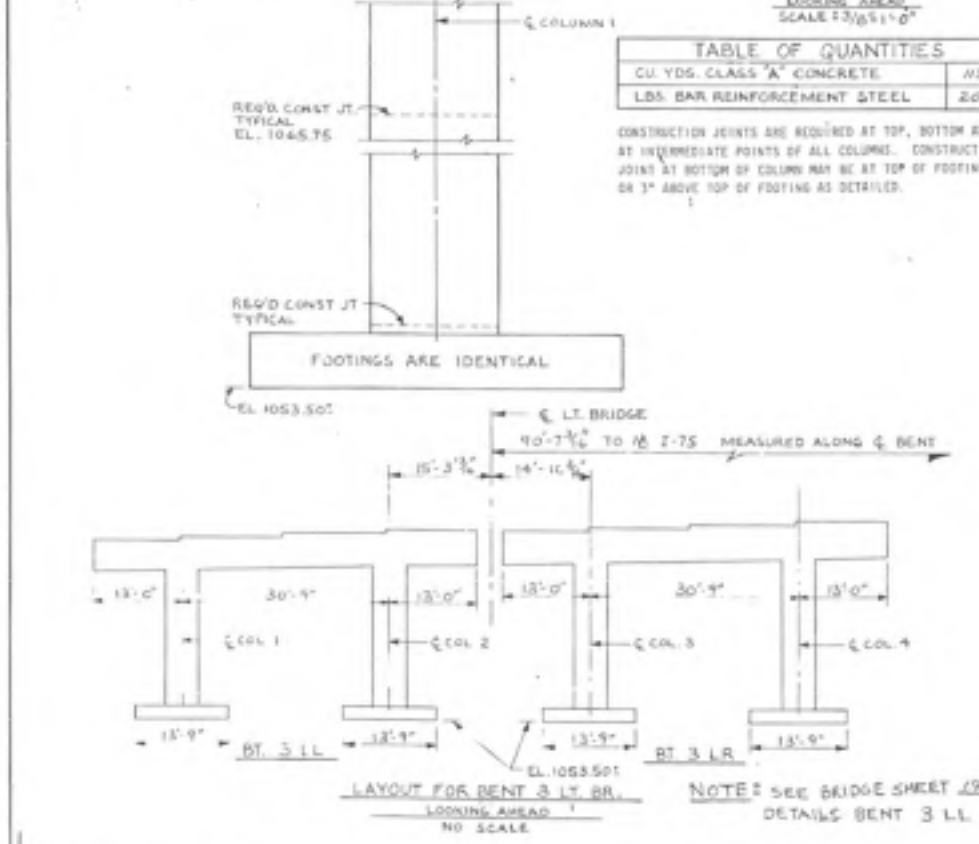


TABLE OF QUANTITIES	
CU. YDS. CLASS "A" CONCRETE	13.67
LBS. BAR REINFORCEMENT STEEL	20,886

CONSTRUCTION JOINTS ARE REQUIRED AT TOP, BOTTOM AND AT INTERMEDIATE POINTS OF ALL COLUMNS. CONSTRUCTION JOINT AT BOTTOM OF COLUMN MAY BE AT TOP OF FOOTING OR 3" ABOVE TOP OF FOOTING AS DETAILED.



NOTE: SPREAD FOOTINGS ARE DESIGNED FOR AN ALLOWABLE SOIL BEARING CAPACITY OF 3.0 TONS PER SQ. FT.

NOTE: FOR BAR BUNDLING DETAILS SEE MISC. DETAILS SHEET.

BRIDGE No. 3 L.T.			
GEORGIA			
DEPARTMENT OF TRANSPORTATION			
HIGHWAY DIVISION - BRIDGE DESIGN			
INTERMEDIATE BENT 3 L.R. DETAILS LEFT BR.			
SBL OVER STEVE FINEY ROAD			
CO. B. COUNTY			
1-75-3(40) 0.89 CT. S			
SCALE: AS SHOWN			
NOV. 1974			
BRIDGE SHEET	DESIGNED BY	TRACED	REVIEWED
20 OF 38	M.J.L.	J.P.T.	L.R.P.
	BAW. D.P.S.		

FILE NO.	DATE	BY	CHKD	APPD	REV	TOTAL
4	GA	3/79	3/79	3/79	3/79	3/79
Contract 3						

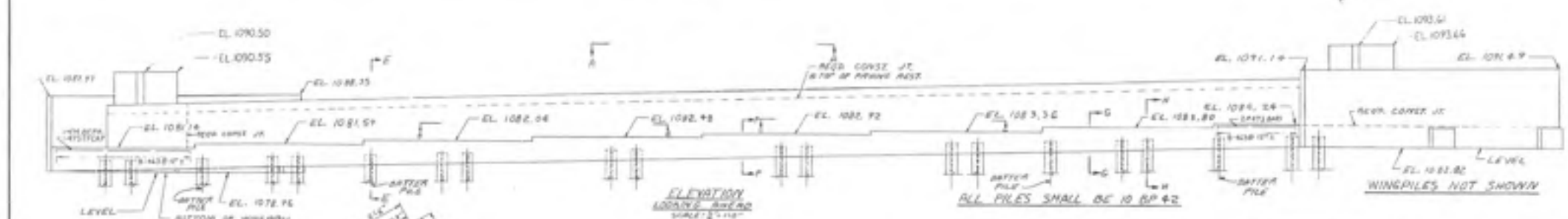
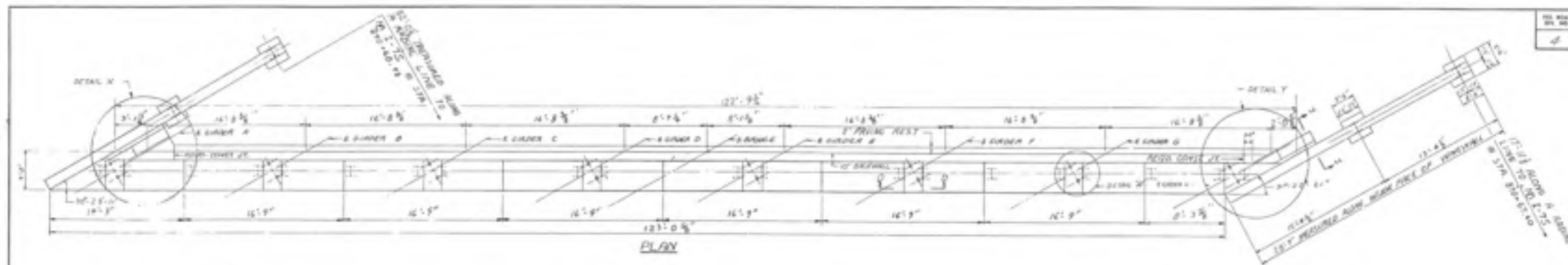
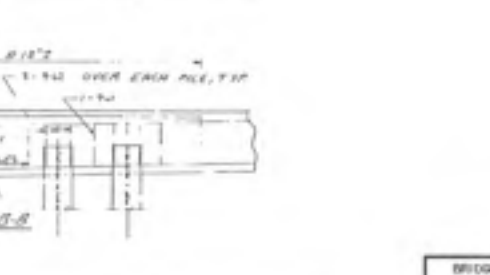
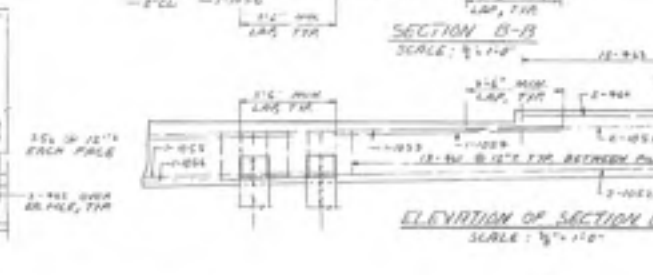
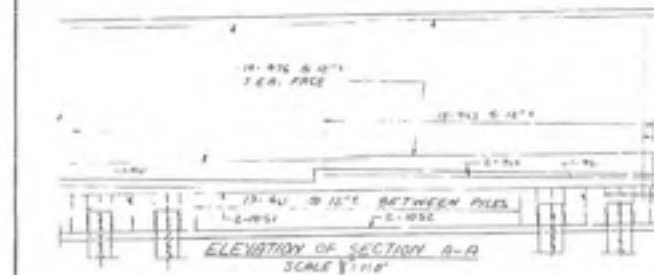
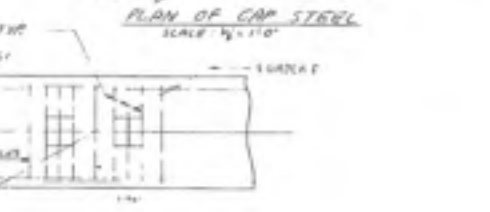
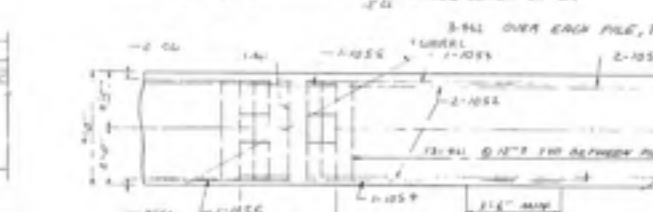
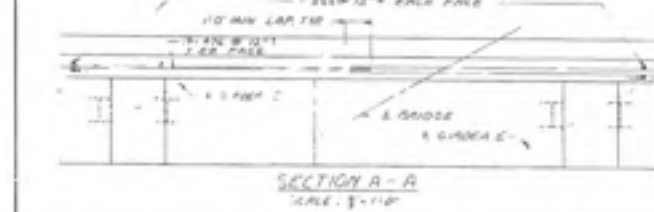
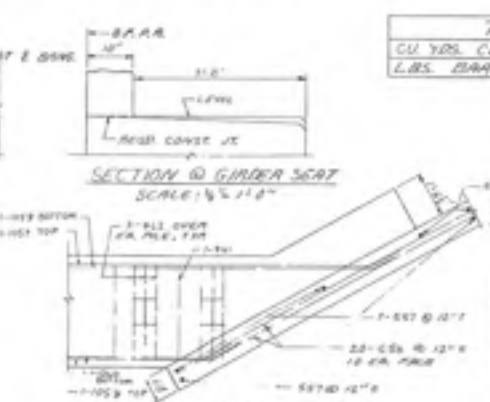
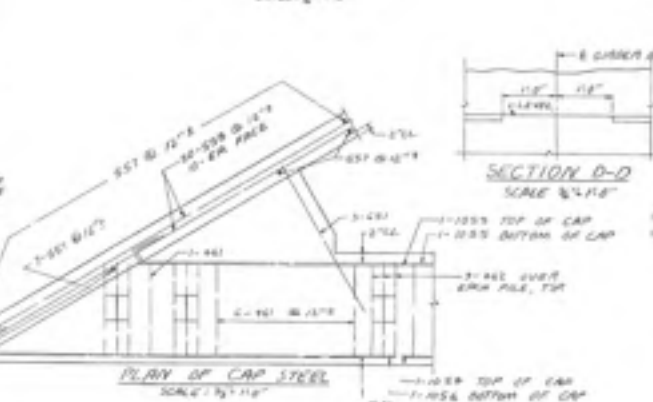
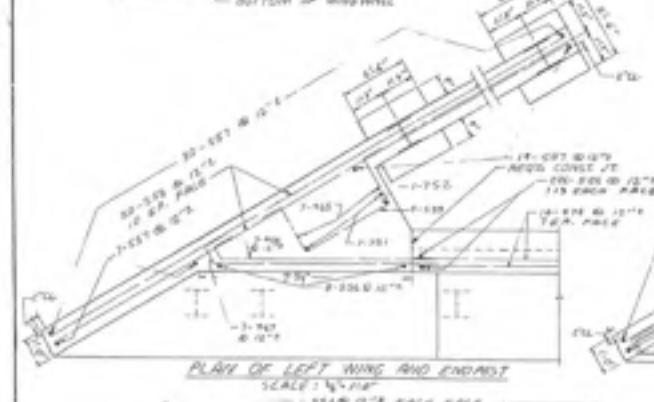


TABLE OF QUANTITIES	
CU YDS. CLASS B CONCRETE	14.76
LBS. BAA REINFORCEMENT	10,489



PLAN DRAWING OBJECTIVE
PLAN DRAWING OBJECTIVE SHALL BE A
DESIGNED RESISTANCE OF 45 TONS AFTER A
MAX. DIP ELEVATION OF 105.0 IS ACHIEVED
BRIDGE NO. 3 LT.

GEORGIA
DEPARTMENT OF TRANSPORTATION
HIGHWAY DIVISION - BRIDGE DESIGN

END BENT 4 LEFT

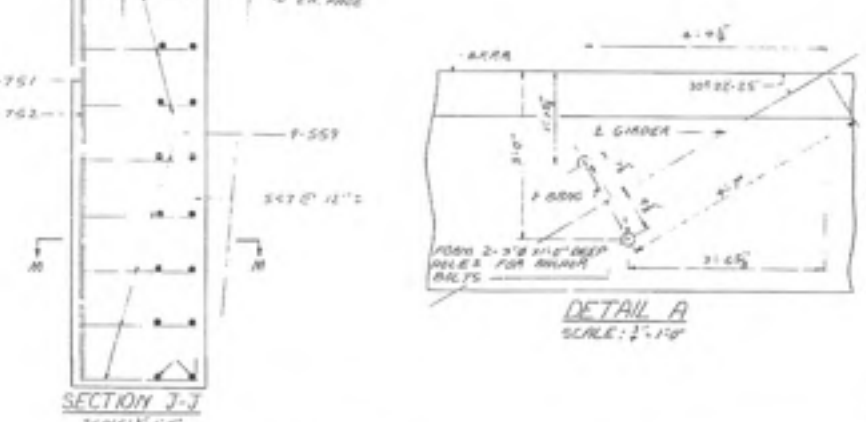
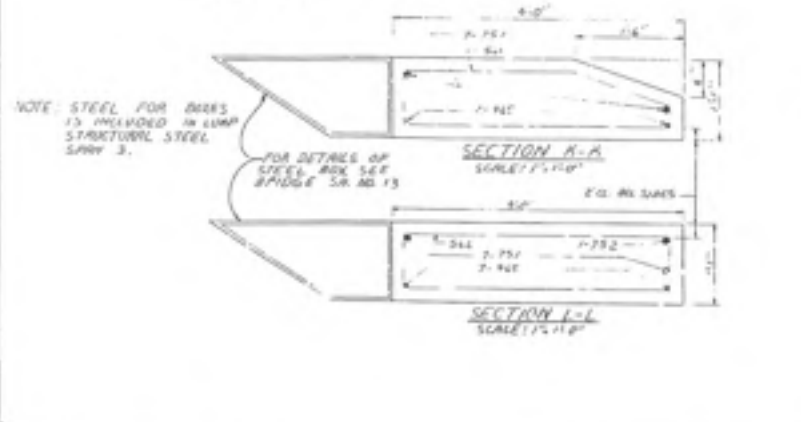
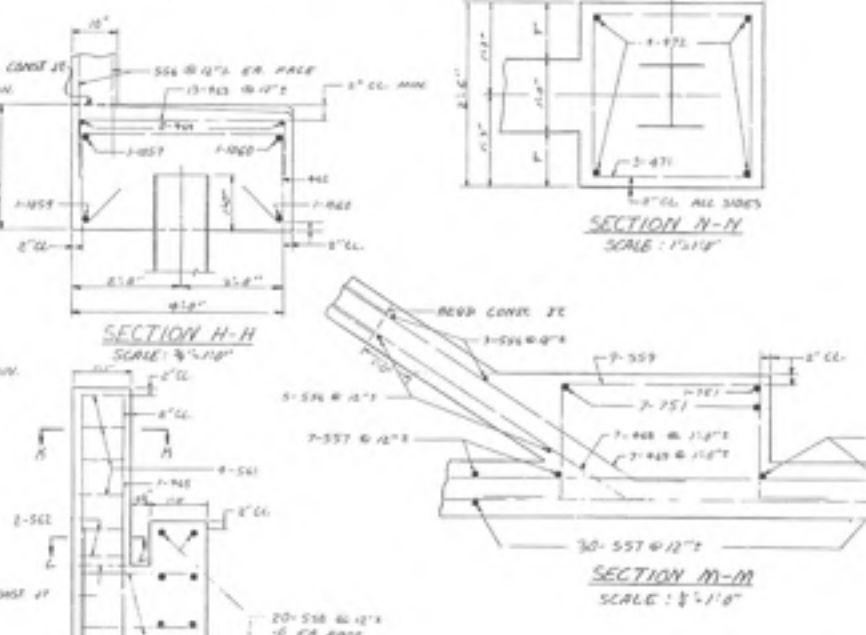
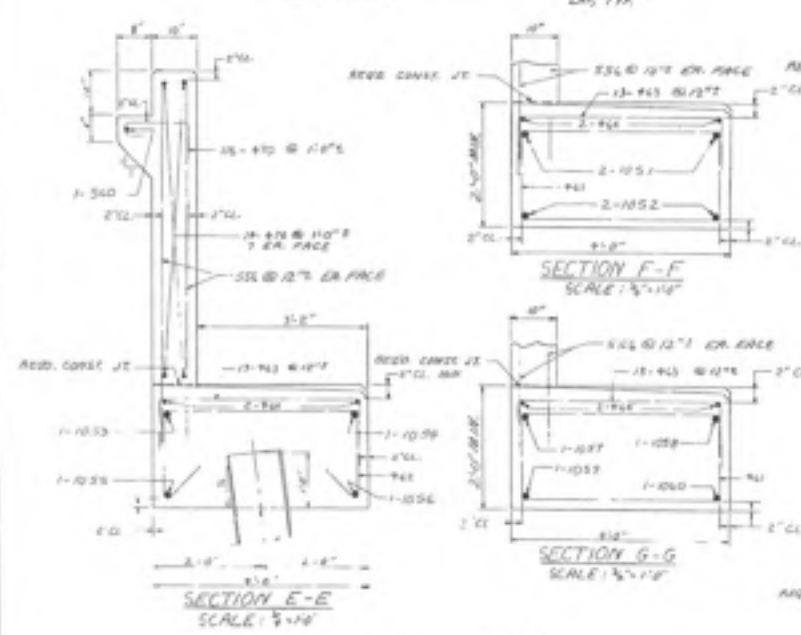
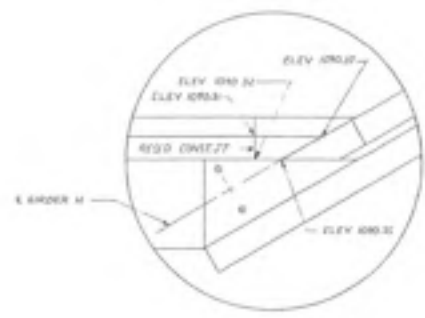
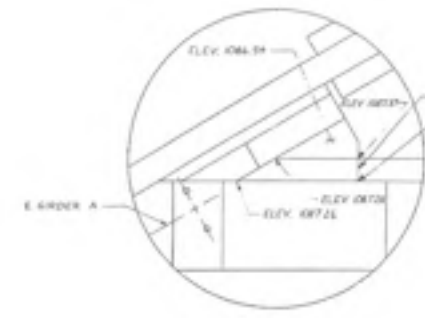
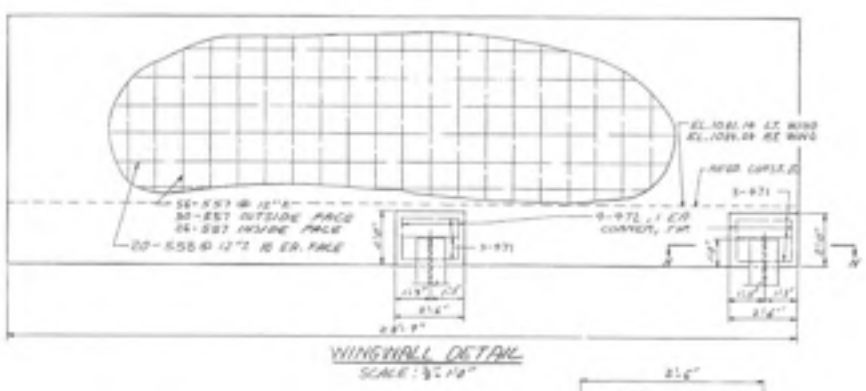
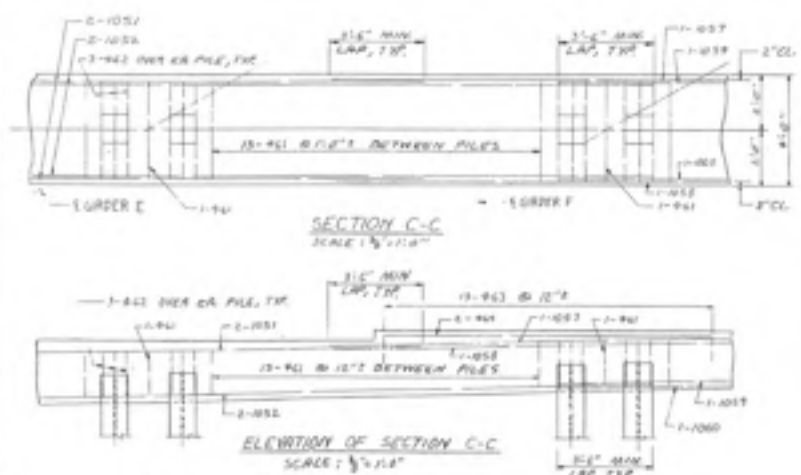
I-75 (SBL) OVER STEVE PACE RD

COBB CO. I-75-3(6)284

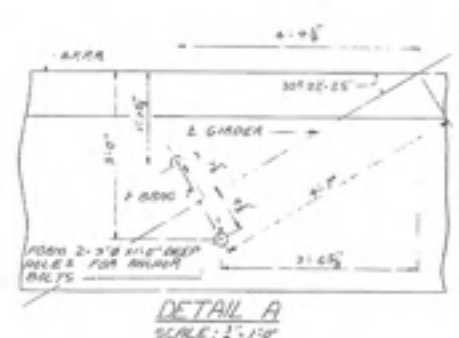
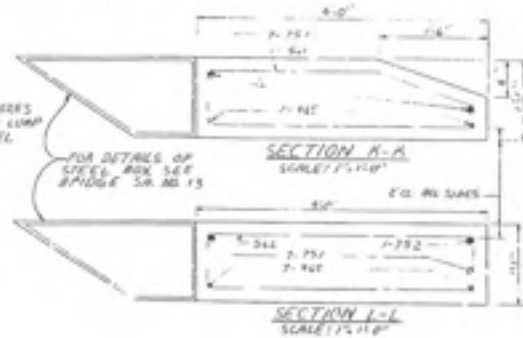
SEA 51 AS SHOWN DEC. 1974

BRIDGE SHEET	DESIGNED	DRAWN	CHECKED	APPROVED
2.1 OF 3.8	JPT	PLD	PLD	LAP

DES. NO.	DATE	REV. NO.	REV. DATE	REV. BY	REV. DESCRIPTION
GA 275-3	12/1/74	1			
GA 275-3	12/1/74	2			



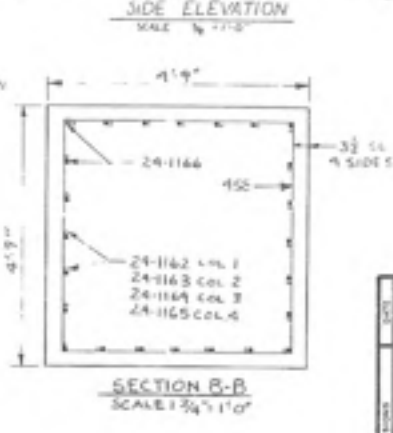
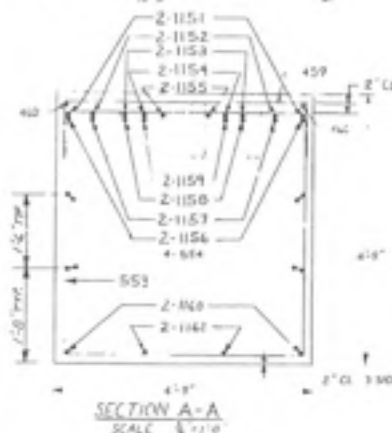
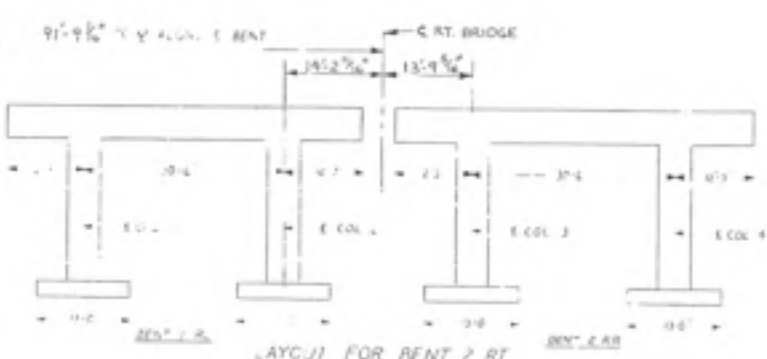
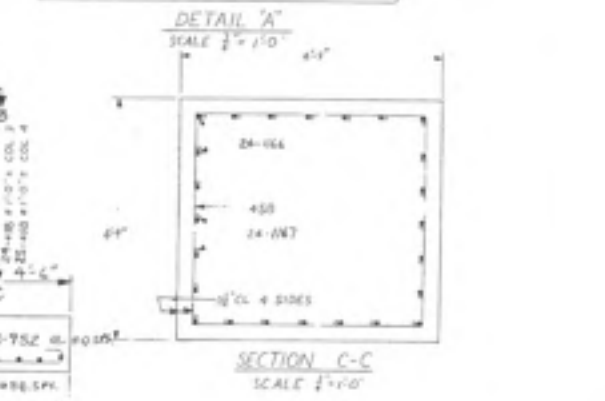
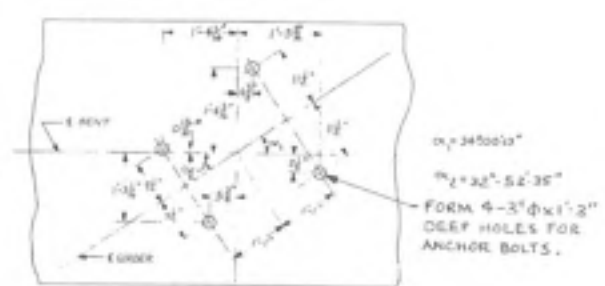
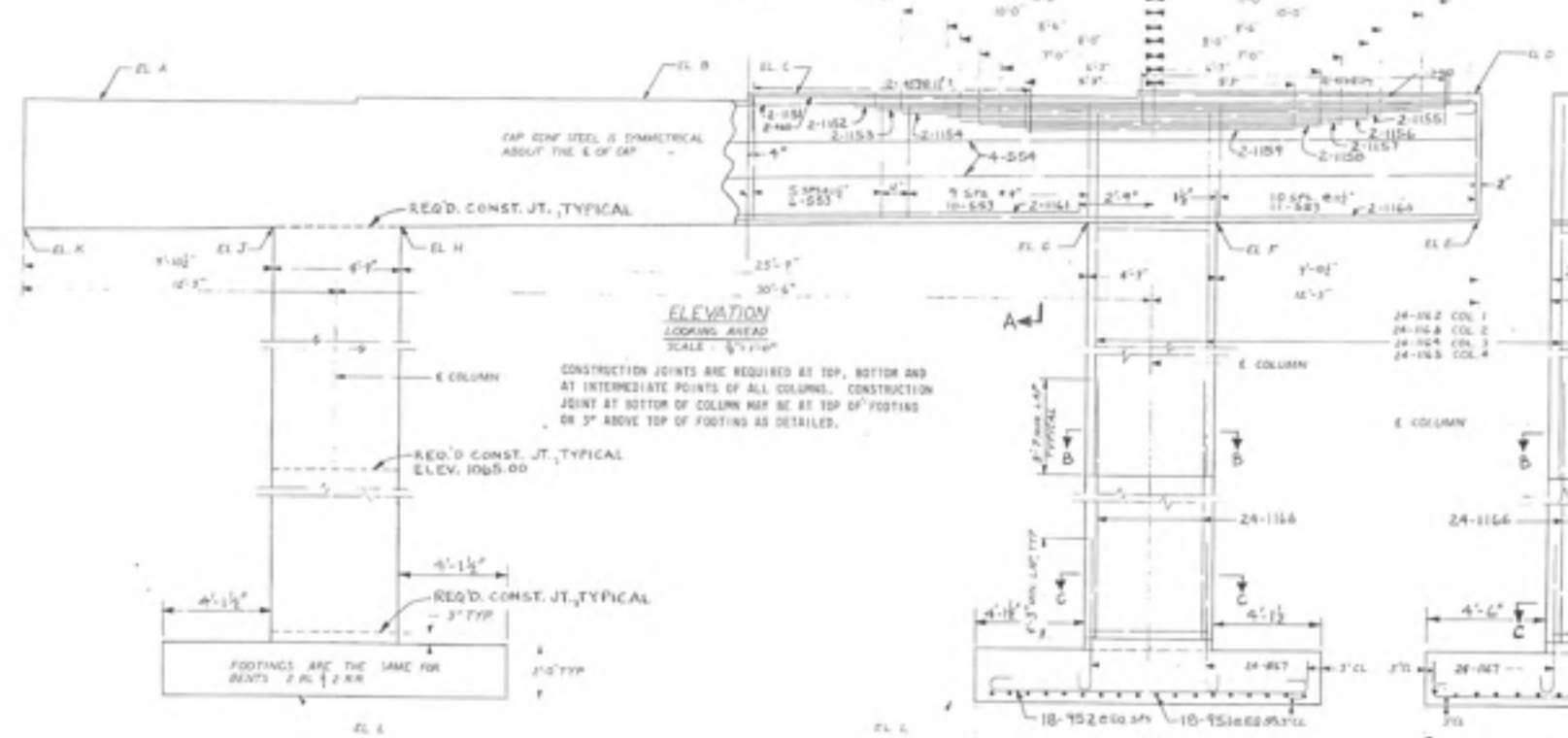
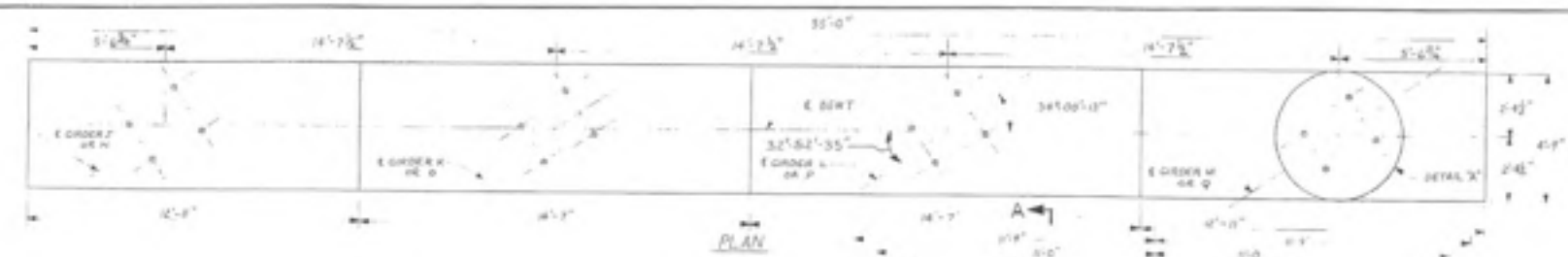
NOTE: STEEL FOR BARS IS PROVIDED IN LUMP STRUCTURAL STEEL SPLY 3.



BRIDGE NO. 3 LT.	
GEORGIA	
DEPARTMENT OF TRANSPORTATION	
HIGHWAY DIVISION - BRIDGE DESIGN	
END BENT & LT. SECTIONS & DETAILS	
I-75 SBL OVER STEVE FREY ROAD	
COBB COUNTY	
I-75-7 (NO) 284	
SCALE: AS SHOWN	
DEC. 1974	
BRIDGE SHEET	DESIGNED: JPT
22 OF 36	TRACED: JPT
	CHECKED: HPL
	APPROVED:

NO.	DATE	BY	CHKD.	REVISION
1	11/7/74	JPT	CDE	REVISED

Contract 5



NOTE: FOR BAR BENDING DETAILS SEE MISC. DETAIL SHEET.

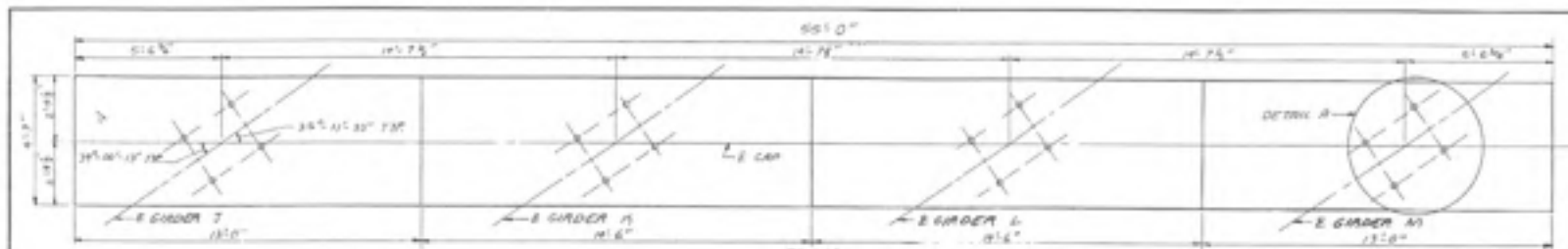
SPREAD PLATING PROVIDED FOR 4 SOLE PLATE. CAPACITY OF 3 TONS PER SQ. FT.

BRIDGE NO. 3 RT.	
GEORGIA	
DEPARTMENT OF TRANSPORTATION	
HIGHWAY DIVISION - BRIDGE DESIGN	
INTERMEDIATE BTS 2RL AND 2RR DETAILS	
NB. OVER STOVE FREY ROAD	
COBB COUNTY	I-75-3400284 C.E.S.
SCALE: AS SHOWN	NOV 1974
DESIGNED: JPT	CHECKED: C.D.E.
DRAWN: FWG	APPROVED: L.R.P.

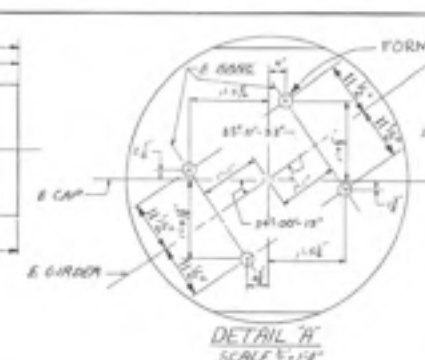
TABLE OF ELEVATIONS										
BENT	ELEVATION	A	B	C	D	E	F	G	H	I
2 RL	1081.29	1081.70	1082.11	1082.52	1077.73	1077.45	1077.32	1076.58	1076.45	1076.17
2 RR	1082.12	1082.53	1082.94	1083.35	1078.56	1078.28	1078.15	1077.41	1077.28	1076.99

TABLE OF QUANTITIES			
ITEM	BENT	2 RL	2 RR
CONCRETE CLASS X	110.28	112.95	
REINFORCEMENT STEEL	78.37	78.38	

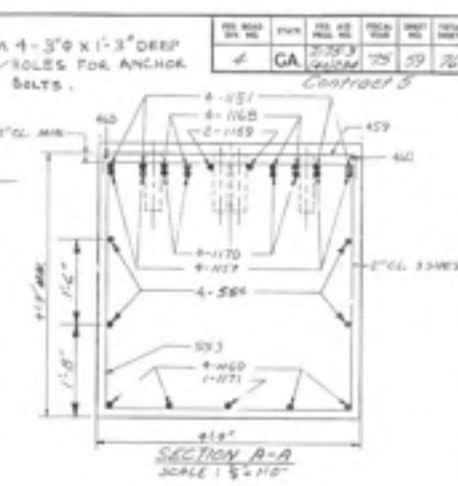
BRIDGE SHEET
24 OF 36



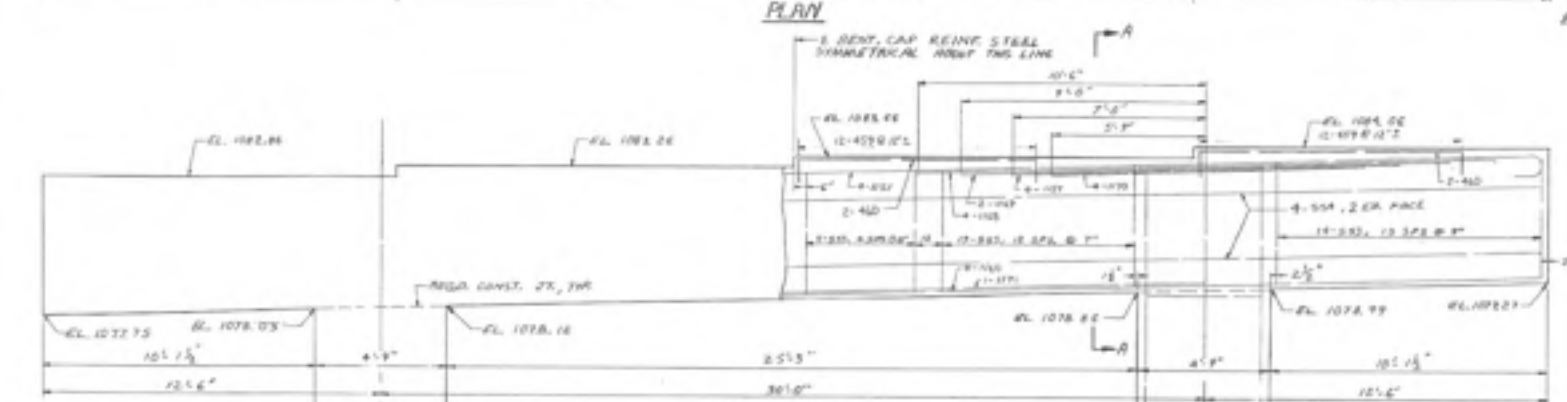
PLAN



DETAIL A
SCALE: 1/4" = 1'-0"



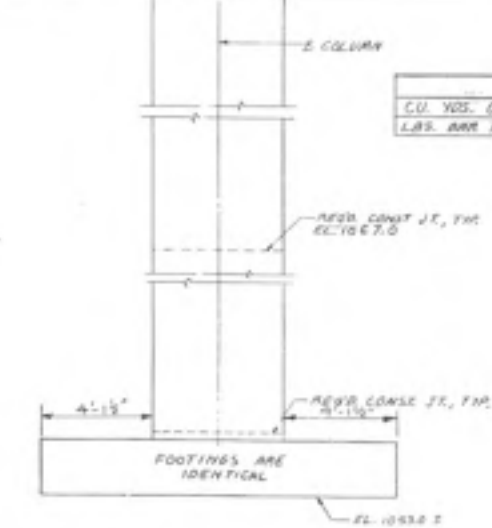
SECTION A-A
SCALE: 1/4" = 1'-0"



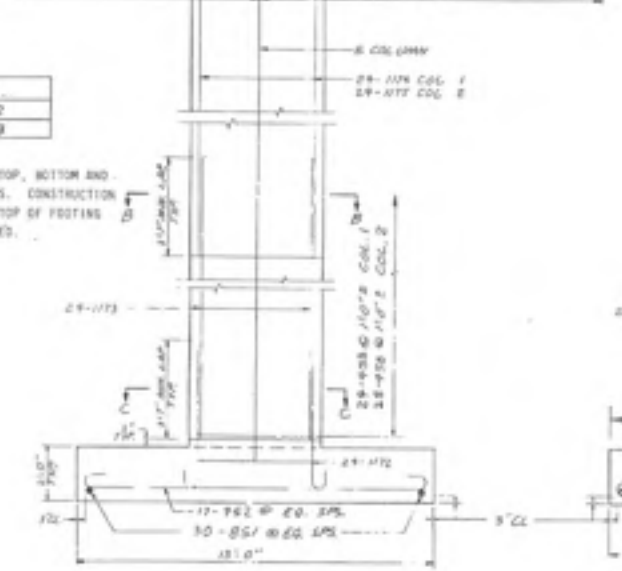
ELEVATION
LOOKING AHEAD
SCALE: 1/4" = 1'-0"

TABLE OF QUANTITIES	
CU. YDS. CLASS "A" CONCRETE	117.52
LBS. BAR REINFORCEMENT STEEL	21,033

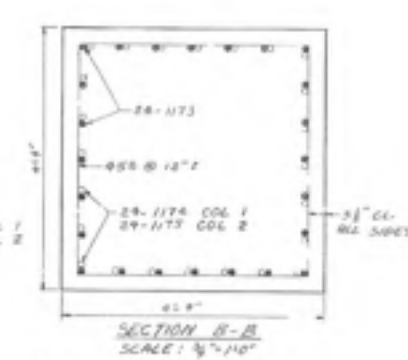
CONSTRUCTION JOINTS ARE REQUIRED AT TOP, BOTTOM AND AT INTERMEDIATE POINTS OF ALL COLUMNS. CONSTRUCTION JOINT AT BOTTOM OF COLUMN MAY BE AT TOP OF FOOTING OR 3" ABOVE TOP OF FOOTING AS DETAILED.



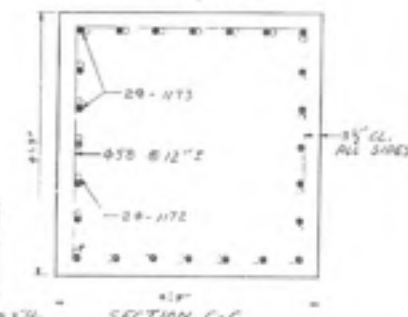
FOOTINGS ARE IDENTICAL



SIDE ELEVATION



SECTION B-B
SCALE: 1/4" = 1'-0"



SECTION C-C
SCALE: 1/4" = 1'-0"

SPREAD FOOTINGS ARE DESIGNED FOR AN ALLOWABLE SOIL BEARING CAPACITY OF 2.5 TONS PER SQ. FT.

NOTE: FOR BAA BUNDLING DETAILS SEE REIN. DETAIL SHEET.

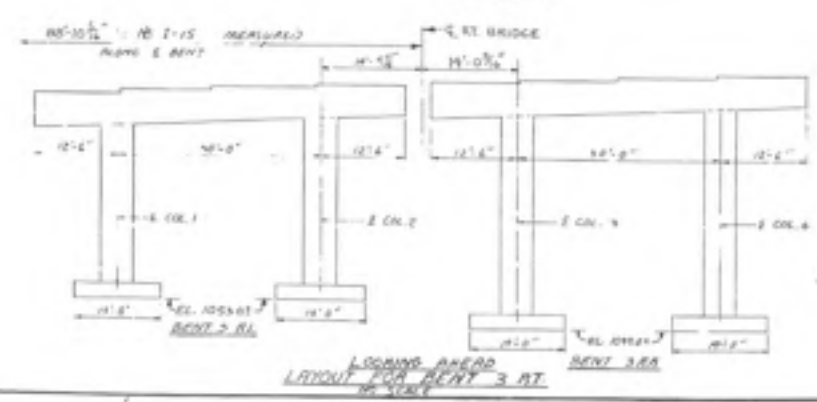
BRIDGE NO. 3 AT

GEORGIA
DEPARTMENT OF TRANSPORTATION
HIGHWAY DIVISION - BRIDGE DESIGN

INTERMEDIATE BENT 3 RL DETAILS AT BS
NBL OVER STEVE PACEY ROAD
COB & CO. CTB
SCALE: AS SHOWN
DEC. 1979

BRIDGE SHEET 25 OF 38	DESIGNED BY DRAWN BY	CHECKED BY APPROVED
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NOTE: SEE BRIDGE SHEET 26 FOR DETAILS BENT 3 R.A.



LAYOUT FOR BENT 3 AT

22

11

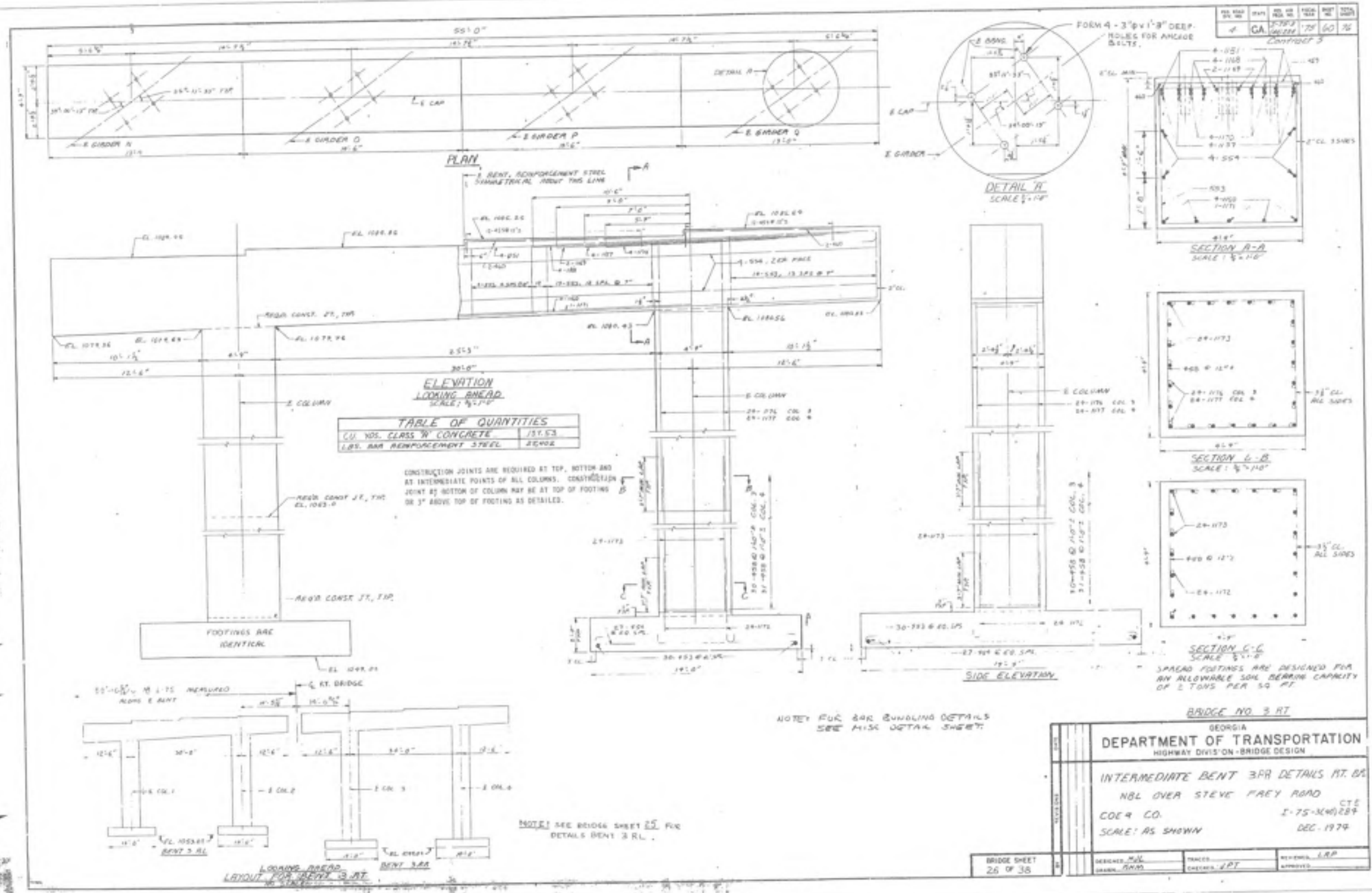
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58

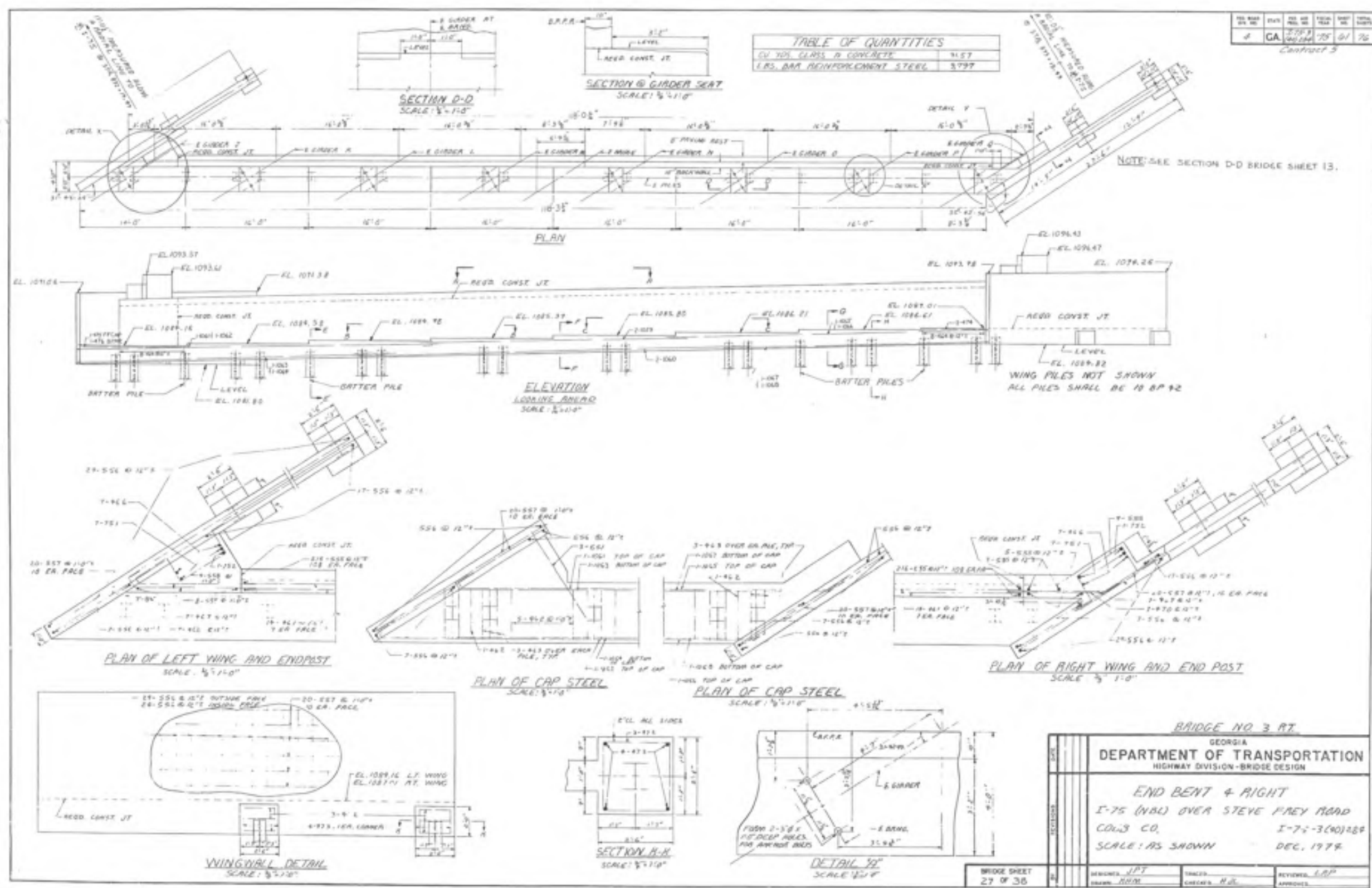
8.5

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58
8.5
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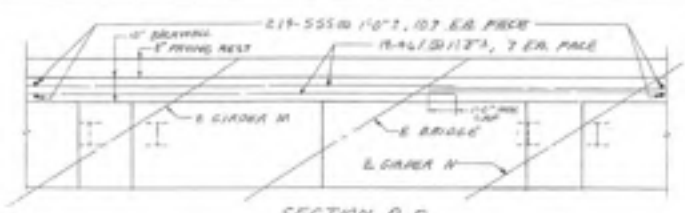
58

8.5

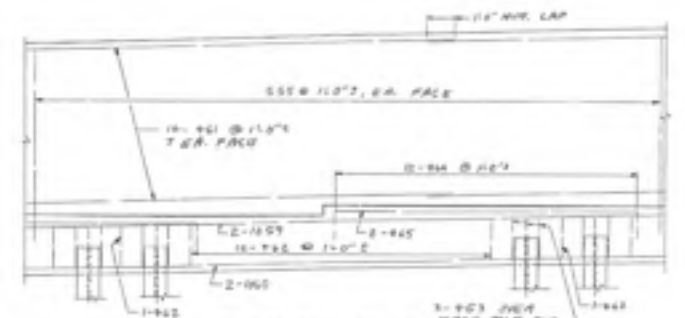
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17

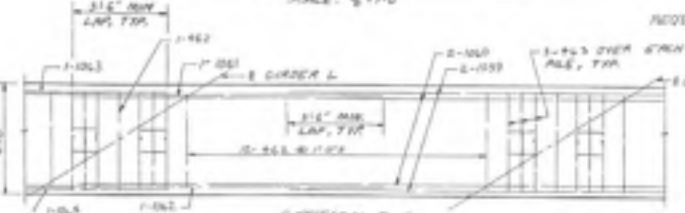
22



SECTION A-A
SCALE: 1/4"



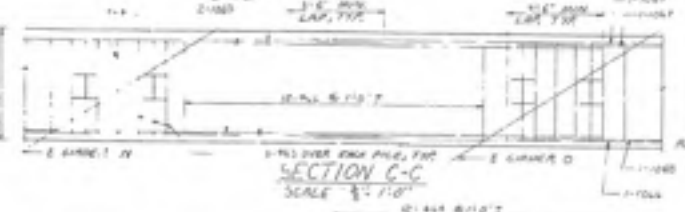
ELEVATION OF SECTION A-A
SCALE: 1/4"



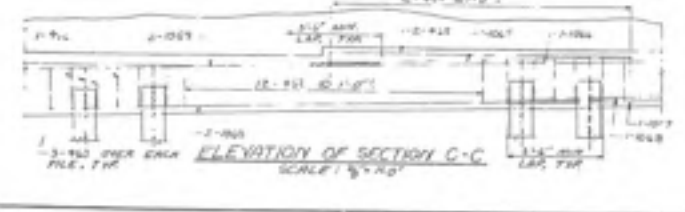
SECTION B-B
SCALE: 1/4"



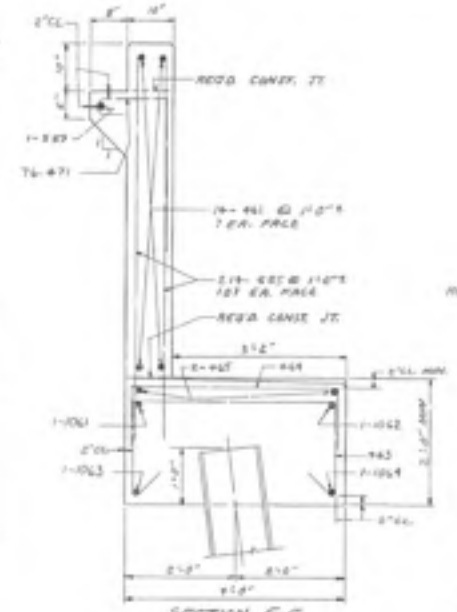
ELEVATION OF SECTION B-B
SCALE: 1/4"



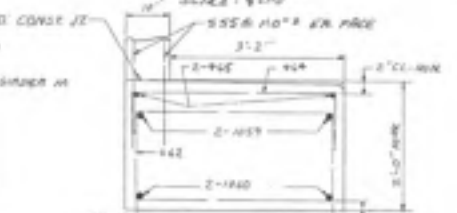
SECTION C-C
SCALE: 1/4"



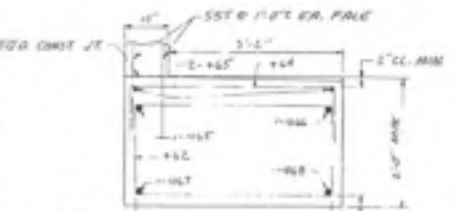
ELEVATION OF SECTION C-C
SCALE: 1/4"



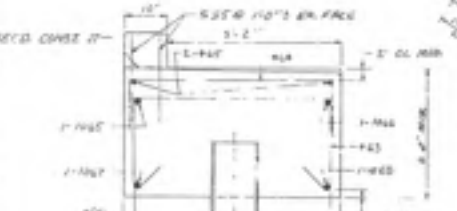
SECTION E-E
SCALE: 1/4"



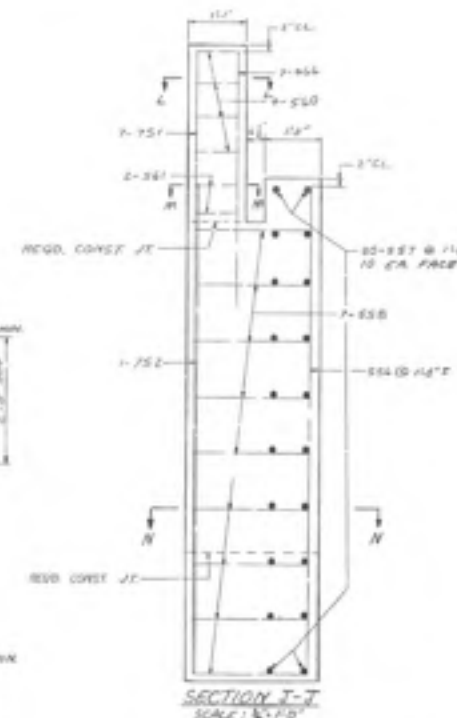
SECTION F-F
SCALE: 1/4"



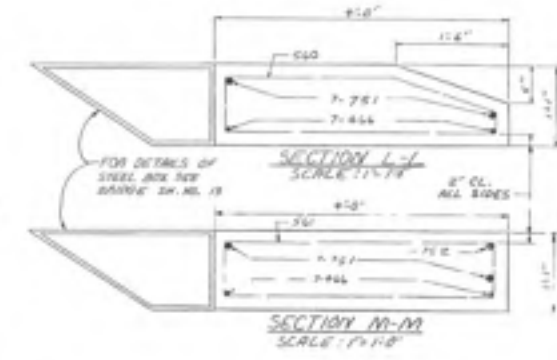
SECTION G-G
SCALE: 1/4"



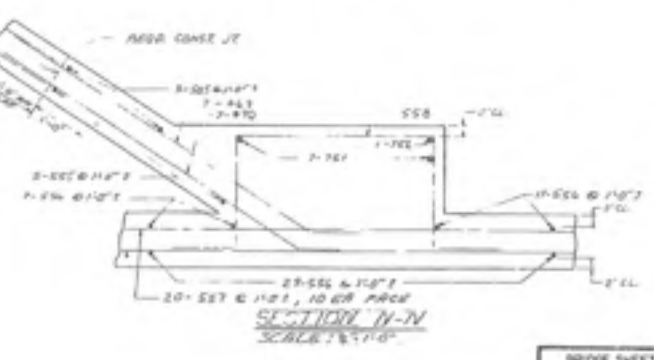
SECTION H-H
SCALE: 1/4"



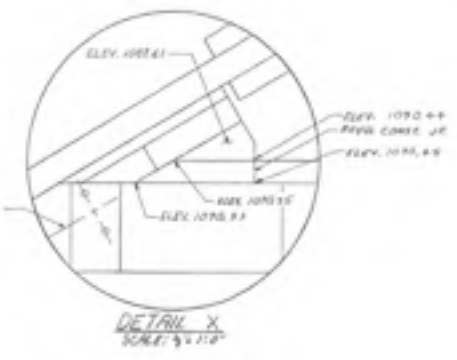
SECTION I-I
SCALE: 1/4"



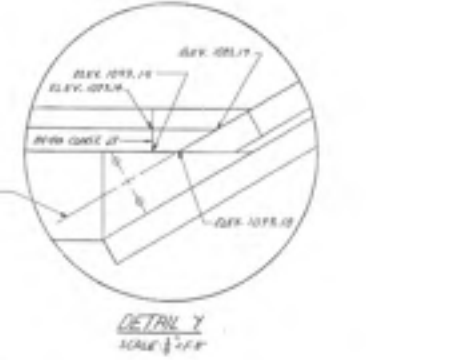
SECTION J-J
SCALE: 1/4"



SECTION K-K
SCALE: 1/4"



DETAIL X
SCALE: 1/4"



DETAIL Y
SCALE: 1/4"

PLAY DRIVING OBJECTIVE
PLAY DRIVING OBJECTIVE SHALL BE A DRIVING
RESISTANCE OF 95 TONS AFTER A MAX. TIP
ELEVATION OF 1055.0 IS ACHIEVED.

BRIDGE NO. 3 RT.

GEORGIA
DEPARTMENT OF TRANSPORTATION
HIGHWAY DIVISION - BRIDGE DESIGN

END BENT 4 RT. SECTIONS AND DETAILS
I-75 (NBL) OVER STEVE FREY ROAD
COB CO. I-75-3 (40) 284
SCALE: AS SHOWN DEC. 1978

BRIDGE SHEET 28 OF 38	DESIGNED: JPT DRAWN: MMS	TRACED: CHECKED: HCL	REVIEWED: LRP APPROVED:
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LOCATION	NO. OF LOC.	MARK	LENGTH	NO. BARS	AG	B	C	D	E	F	H	J	K	LOCATION	NO. OF LOC.	MARK	LENGTH	NO. BARS	AG	B	C	D	E	F	H	J	K
402														1001													
501K VARY	328	3				2-0								1002K	32-5	8	1										
502K 40-1	76	1												1002B	40-5	4	1										
502K VARY	308	1												1003	3-5	8	1										
502K 40-1	76	1												401K	30-10	150	1										
503K 35-0	18	1												402		364											
503K 33-2	16	1												501L	20-5	144	1										
504	4-3	156	40											501K VARY	154	3			2-0								
506	22-0	10	1											502L	20-5	144	1										
														502K VARY	154	1											
501K 33-5	4	1												503K	30-11	8	1										
501K 44-5	2	3				2-0								504	3-3	76	40										
501K 45-1	2	3				2-0								506	22-0	10	1										
501K 45-5	2	3				2-0																					
501K 46-2	2	3				2-0								501K 33-3	4	1											
502K 31-10	8	1												501K 43-5	2	3											
502K 40-6	4	1												501L	40-2	2	3										
503	3-6	8	1											501K 43-4	2	3			2-0								
														501K 43-5	2	3			2-0								
1001K 34-0	4	1												501K 43-6	2	3			2-0								
1001K 44-5	2	3				2-0								501K 43-7	2	3			2-0								
1001K 45-0	2	3				2-0								501K 43-8	2	3			2-0								
1001K 43-8	2	3				2-0								501K 43-9	2	3			2-0								
1001K 44-5	2	3				2-0								501K 43-10	2	3			2-0								
1001K 45-5	2	3				2-0								501K 43-11	2	3			2-0								
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1001K 47-5	2	3				2-0								501K 43-13	2	3			2-0								
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1001K 49-5	2	3				2-0								501K 43-15	2	3			2-0								
1001K 50-5	2	3				2-0								501K 43-16	2	3			2-0								
1001K 51-5	2	3				2-0								501K 43-17	2	3			2-0								
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1001K 53-5	2	3				2-0								501K 43-19	2	3			2-0								
1001K 54-5	2	3				2-0								501K 43-20	2	3			2-0								
1001K 55-5	2	3				2-0								501K 43-21	2	3			2-0								
1001K 56-5	2	3				2-0								501K 43-22	2	3			2-0								
1001K 57-5	2	3				2-0								501K 43-23	2	3			2-0								
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1001K 100-5	2	3				2-0								501K 43-66	2	3			2-0								
1001K 101-5	2	3				2-0								501K 43-67	2	3			2-0								
1001K 102-5	2	3				2-0								501K 43-68													

LOCATION																LOCATION															
NO. OF LOC.	MARK	LENGTH	NO. BARS	T	A	B	C	D	E	F	H	J	K	N	NO. OF LOC.	MARK	LENGTH	NO. BARS	T	A	B	C	D	E	F	H	J	K	N		
FT. IN.		FT. IN.													FT. IN.		FT. IN.														
SPAN 1 AT ROAD 1																															
4028	32	9	1025	1											702	4	5	2	5	2	3	7	5/8								
402	36	9	1025	1											703	2	4	2	5	2	1	8	5/8								
4023	36	9	1025	1											801	34	0	6	1												
4024	36	9	1025	1											9018	54	8	2	3												
4025	36	9	1025	1											9019	32	0	4	1												
4026	36	9	1025	1											9020	45	1	2	3												
4027	36	9	1025	1											9021	30	8	4	3												
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4053	36	9	1025	1											1021	34	8	4	1												
4054	36	9	1025	1											1022	46	8	2	1												
4055	36	9	1025	1											1023	34	8	4	1												
4056	36	9	1025	1											1024	46	8	2	1												
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4062	36	9	1025	1											1030	46	8	2	1												
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4072	36	9	1025	1											1040	46	8	2	1												
4073	36	9	1025	1											1041	34	8	4	1												
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4075	36	9	1025	1											1043	34	8	4	1												
4076	36	9	1025	1											1044	46	8	2	1												
4077	36	9	1025	1											1045	34	8	4	1												
4078	36	9	1025	1											1046	46	8	2	1												
4079	36	9	1025	1											1047	34	8	4	1												
4080	36	9	1025	1											1048	46	8	2	1												
4081	36	9	1025	1											1049	34	8	4	1												
4082	36	9	1025	1											1050	46	8	2	1												
4083	36	9	1025	1											1051	34	8	4	1												
4084	36																														

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22

LOCATION										LOCATION											
NO. OF LOC.		MARK		LENGTH		NO. BARS		V. AG		B		C		D		E		F		H	
PT. IN.		PT. IN.		PT. IN.		PT. IN.		PT. IN.		PT. IN.		PT. IN.		PT. IN.		PT. IN.		PT. IN.		PT. IN.	
10010		42-5		2-3		2-0		42-5		2-0		42-5		2-0		42-5		2-0		42-5	
10011		41-0		2-3		2-0		41-0		2-0		41-0		2-0		41-0		2-0		41-0	
10012		41-8		2-3		2-0		41-8		2-0		41-8		2-0		41-8		2-0		41-8	
10013		31-0		8-1		2-0		31-0		8-1		31-0		8-1		31-0		8-1		31-0	
10014		47-1		4-1		2-0		47-1		4-1		47-1		4-1		47-1		4-1		47-1	
10015		3-4		8-1		2-0		3-4		8-1		3-4		8-1		3-4		8-1		3-4	
SPAN 3 AT PIER 2																					
4010		25-1		150-1		2-0		4010		25-1		150-1		2-0		4010		25-1		150-1	
4011		25-1		150-1		2-0		4011		25-1		150-1		2-0		4011		25-1		150-1	
4012		25-1		150-1		2-0		4012		25-1		150-1		2-0		4012		25-1		150-1	
4013		25-1		150-1		2-0		4013		25-1		150-1		2-0		4013		25-1		150-1	
4014		25-1		150-1		2-0		4014		25-1		150-1		2-0		4014		25-1		150-1	
4015		25-1		150-1		2-0		4015		25-1		150-1		2-0		4015		25-1		150-1	
4016		25-1		150-1		2-0		4016		25-1		150-1		2-0		4016		25-1		150-1	
4017		25-1		150-1		2-0		4017		25-1		150-1		2-0		4017		25-1		150-1	
4018		25-1		150-1		2-0		4018		25-1		150-1		2-0		4018		25-1		150-1	
4019		25-1		150-1		2-0		4019		25-1		150-1		2-0		4019		25-1		150-1	
4020		25-1		150-1		2-0		4020		25-1		150-1		2-0		4020		25-1		150-1	
4021		25-1		150-1		2-0		4021		25-1		150-1		2-0		4021		25-1		150-1	
4022		25-1		150-1		2-0		4022		25-1		150-1		2-0		4022		25-1		150-1	
4023		25-1		150-1		2-0		4023		25-1		150-1		2-0		4023		25-1		150-1	
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4025		25-1		150-1		2-0		4025		25-1		150-1		2-0		4025		25-1		150-1	
4026		25-1		150-1		2-0		4026		25-1		150-1		2-0		4026		25-1		150-1	
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4028		25-1		150-1		2-0		4028		25-1		150-1		2-0		4028		25-1		150-1	
4029		25-1		150-1		2-0		4029		25-1		150-1		2-0		4029		25-1		150-1	
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4033		25-1		150-1		2-0		4033		25-1		150-1		2-0		4033		25-1		150-1	
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4062		25-1		150-1		2-0		4062		25-1		150-1		2-0		4062		25-1		150-1	
4063		25-1		150-1		2-0		4063		25-1		150-1		2-0		4063		25-1		150-1	
4064		25-1		150-1		2-0		4064		25-1		150-1		2-0		4064		25-1		150-1	
4065		25-1		150-1		2-0		4065		25-1		150-1		2-0		4065		25-1		150-1	
4066		25-1		150-1		2-0		4066		25-1		150-1		2-0		4066		25-1		150-1	
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4069		25-1		150-1		2-0		4069		25-1		150-1		2-0		4069		25-1		150-1	
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4079		25-1		150-1		2-0		4079		25-1		150-1		2-0		4079		25-1		150-1	
4080		25-1		150-1		2-0		4080		25-1		150-1		2-0		4080		25-1		150-1	
4081		25-1		150-1		2-0		4081		25-1		150-1		2-0		4081		25-1		150-1	
4082		25-1		150-1		2-0		4082		25-1		150-1		2-0		4082		25-1		150-1	
4083		25-1		150-1		2-0		4083		25-1		150-1		2-0		4083		25-1		150-1	
4084		25-1		150-1		2-0		4084		25-1		150-1		2-0		4084		25-1		150-1	
4085		25-1		150-1		2-0		4085		25-1		150-1		2-0		4085		25-1		150-1	
4086		25-1		150-1		2-0		4086		25-1		150-1		2-0		4086		25-1		150-1	
4087		25-1		150-1		2-0		4087		25-1		150-1		2-0		4087		25-1		150-1	
4088		25-1		150-1		2-0		4088		25-1		150-1		2-0		4088		25-1		150-1	
4089		25-1		150-1		2-0		4089		25-1		150-1		2-0		4089		25-1		150-1	
4090		25-1		150-1		2-0		4090		25-1		150-1		2-0		4090		25-1		150-1	
4091		25-1		150-1		2-0		4091		25-1		150-1		2-0		4091		25-1		150-1	
4092		25-1		150-1		2-0		4092		25-1											

CALCULATION SHEET

PROJECT: I-75 / I-575 NORTHWEST CORRIDOR

JOB NUMBER NH000-0073-03(242)

CALC NO. BR#33

SUBJECT: Bridge Maintenance Reports

BY: JCR

DATE: 11/30/2009

SHEET NO.

SHEET REV.

BRIDGE INVENTORY DATA LISTING GEOG A DEPARTMENT OF TRANSPORTATION

Structure ID: 067-0085-0

Cobb

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Location & Geography

* Structure I.D.No: 067-0085-0
 * 200 Bridge Information 06
 * 6A Feature Int: CR 160 STEVE FREY ROAD
 * 6B Critical Bridge: 0
 * 7A Route Number Carried: SR00401
 * 7B Facility Carried: I-75 (NBL)
 * 9 Location: 2.4 MI NE OF KENNESAW
 * 2 DOT District: 7
 * 207 Year Photo: 2009
 * 91 Inspection Frequency: 24 Date: 03/19/2009
 * 92A Fract Crit Insp Freq: 00 Date: 02/01/1901
 * 92B Underwater Insp Freq: 00 Date: 02/01/1901
 * 92C Other Spec. Insp Freq: 00 Date: 02/01/1901
 * 4 Place Code: 00000
 * 5 Inventory Route (O/U): 1
 * Type: 1
 * Designation: 1
 * Number: 00075
 * Direction: 0
 * 16 Latitude: 34-02.5890 MMS Prefix: SR
 * 17 Longitude: 84-34.8770 MMS Suffix: 00 MP: 271.97
 * 98 Border Bridge: 000 %Shared: 00
 * 99 ID Number: 0000000000000000
 * 100 STRAHNET: 1
 * 12 Base Highway Network: 1
 * 13A LRS Inventory Route: 671040100
 * 13B Sub Inventory Route: 0
 * 101 Parallel Structure: R
 * 102 Direction of Traffic: 1
 * 264 Road Inventory Mile Post: 014.34
 * 208 Inspection Area: 09 Initials: JMC
 * Engineer's Initial: sgm
 * Location I.D. No.: 067-00401D-271.97N

Signs & Attachments

* 104 Highway System: 1
 * 26 Functional Classification: 11
 * 204 Federal Route Type: 1 No.: 00007
 * 105 Federal Lands Highway: 0
 * 110 Truck Route: 1
 * 206 School Bus Route: 0
 * 217 Benchmark Elevation: 0000.00
 * 218 Datum: 0
 * 19 Bypass Length: 01
 * 20 Toll: 3
 * 21 Maintenance: 01
 * 22 Owner: 01
 * 31 Design Load: 6
 * 37 Historical Significance: 5
 * 205 Congressional District: 11
 * 27 Year Constructed: 1976
 * 106 Year Reconstructed: 0000
 * 33 Bridge Median: 1
 * 34 Skew: 60
 * 35 Structure Flared: 0
 * 38 Navigation Control: N
 * 213 Special Steel Design: 0
 * 267 Type of Paint: 5
 * 42 Type of Service on: 1
 * 214 Movable Bridge: 0
 * 203 Type Bridge: Z-O-M-O
 * 259 Pile Encasement: 3
 * 43 Structure Type Main: 3 02
 * 45 No. Spans Main: 003
 * 44 Structure Type Appr: 0 00
 * 46 No. Spans Appr: 0000
 * 226 Bridge Curve Horiz: 1 Vert: 0
 * 111 Pier Protection: 0
 * 107 Deck Structure Type: 1
 * 108 Wearing Surface Type: 1 M, F
 * 225 Expansion Joint Type: 15
 * 242 Deck Drains: 0
 * 243 Parapet Location: 3
 * Height: 2.30
 * Width: 1.60
 * 238 Curb: 0.00 0
 * 239 Handrail: 7 7
 * 240 Median Barrier Rail: 0
 * 241 Bridge Median Height: 0.00
 * Width: 0.00
 * 230 Guardrail Loc Dir Rear: 3
 * Fwd: 2
 * Oppo Dir Rear: 0
 * Fwd: 0
 * 244 Approach Slab: 3
 * 224 Retaining Wall: 0
 * 233 Posted Speed Limit: 65
 * 236 Warning Sign: 0
 * 234 Delineator: 1
 * 235 Hazard Boards: 0
 * 237 Utilities Gas: 00
 * W 00
 * Ele 22
 * Telephone: 00
 * St 00
 * 247 Lighting Street: 0
 * Navigaton: 0
 * Aerial: 0
 * 248 County Continuity No.: 00

BRIDGE INVENTORY DATA LISTING GEOG A DEPARTMENT OF TRANSPORTATION

Structure ID: 067-0085-0

Cobb

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Programming Data

201 Project No.: 1-75-3 (40) 284 CT.5
 202 Plans Available: 4
 249 Prop. Proj. No. 000000000000000000
 250 Approval Status: 0000
 251 P.L. No.: 00000000
 252 Contract Date: 02/01/1901
 260 Seismic No.: 00000
 75 Type Work: 00 0
 94 Bridge Imp. Cost: \$ 0
 95 Roadway Imp. Cost: \$ 0
 96 Total Imp Cost: \$ 0
 76 Imp. Length: 000000
 97 Imp. Year: 0000
 114 Future ADT: 206940 Year: 2027

Measurements

* 29 ADT: 137960 Year: 2007
 109 % Trucks: 0
 * 28 Lanes On: 03 Under: 04
 210 No. Tracks On: 00 Under: 00
 * 48 Max. Span Length: 0123
 * 49 Structure Length: 321
 51 Br. Rwdy. Width: 60.20
 52 Deck Width: 63.20
 * 47 Tot. Horiz. Cl: 60.20
 50 Curb/Sdewlk Width: 0.00/0.00
 32 Approach Rdwy Width: 056
 * 229 Shoulder Width:

Rear Lt: 10.00 Type: 2 Rt: 10.00
 Fwd Lt: 10.00 Type: 2 Rt: 10.00

Pavement Width:

Rear: 36.00 Type: 2
 Fwd: 36.00 Type: 2

Intersection Rear: 0 Fwd: 0

36 Safety Features Br. Rail:

Transition: 1

App. G. Rail: 1

App. Rail End: 1

53 Minimum Cl.Over:

Under: H

* 228 Min. Vertical Cl

Act. Od. Dir:

Oppo. Dir:

Posted Od. Dir:

Oppo. Dir:

55 Lateral Undercl. Rt:

56 Lateral Undercl. Lt:

* 10 Max Min Vert Cl:

39 Nav Vert Cl:

116 Nav Vert Cl Closed:

245 Deck Thickness Main:

Deck Thick Approach:

246 Overlay Thickness:

212 Year Last Painted:

Sup: 1995 Sub: 0000

253 Notification Date: 02/01/1901

253 Fed Notify Date: 02/01/1901

0

Hydraulic Data

215 Waterway Data
 Highway Elev.: 0000.0 Year: 1900
 Avg. Streambed Elev.: 0000.0 Freq.: 00
 Drainage Area: 00000
 Area Of Opening: 000000
 113 Scour Critical: N
 216 Water Depth: 00.0 Br. Height: 00.0
 222 Slope Protection: 4
 221 Sp. Dikes Rear: 0 Fwd: 0
 219 Fender System: 0
 220 Dolphin: 0
 223 Culvert Cover: 000
 Type: 0
 No. Barrels: 0
 Width: 0.00 Height: 0.00
 Length: 0 Apron: 0
 265 U/W Insp. Area: 0 Diver: ZZZ

* Location I.D. No.: 067-0040ID-271.97N

Ratings

65 Inventory Rating Method: 1
 63 Inventory Rating Method: 1
 66 Inventory Type: 2 Rating: 23
 64 Operating Type: 2 Rating: 38
 231 Calculated Loads
 H-Modified: 21 0
 HS-Modified: 30 0
 Type 3: 33 0
 Type 3s2: 38 0
 Timber: 36 0
 Piggyback: 39 0

261 H Inventory Rating: 32
 262 H Operating Rating: 54
 67 Structural Evaluation: 5
 58 Deck Condition: 7
 59 Superstructure Condition: 8
 * 227 Collision Damage: 0
 60A Substructure Condition: 7
 60B Scour Condition: N
 60C Underwater Condition: N
 71 Waterway Adequacy: N
 61 Channel Protection Cond: N
 68 Deck Geometry: 9
 69 UnderClr. Horiz/Vert: 5
 72 Appr. Alignment: 8
 62 Culvert: N

Posting Data

70 Bridge Posting Required: 5
 41 Struct Open, Posted, Cl: A
 * 103 Temporary Structure: 0
 232 Posted Loads H-Modified: 00
 HS-Modified: 00
 Type 3: 00
 Type3s2: 00
 Timber: 00
 Piggyback: 00

253 Notification Date: 02/01/1901
 253 Fed Notify Date: 02/01/1901

0

GEORGIA DEPARTMENT OF TRANSPORTATION

Bridge Inspection Report

District: 7 Inspection Date: 3/19/2009 Inspection Area: 09
 Bridge Inspector: Jerry Cooper Over: CR 160 STEVE FREY ROAD Bridge Status: 06
 Location ID: 067-00401D-271.97N County: Cobb
 Structure ID: 067-0085-0 Road Name: I-75 (NBL)

EVALUATION & DEFICIENCIES

SubStructure:

Year Painted: 0000

Concrete Caps At Both Abutments.
 Bents 2 And 3 Have Concrete Caps On 4 Concrete Columns.
 Minor cracking in both abutment caps.
 Bent #2 = H-32 Calculated 2004 by Central Office (Load Factor) Revised February 2009 SGM

SuperStructure:

Year Painted: 1995

3 Span Steel Plate Girders (8 Beams Per Span) Beam Measurement (501/2" X 18").
 Steel Rocker Bearings At Bents 2, 3 And Abutment 4.
 Very minor corrosion on the bearings.
 All bearings are functioning as designed.
 Span #2 = H-43 Calculated 2004 by Central Office (Load Factor).

Deck:

7.5" Concrete Slab.
 Metal-Stay-In-Place Deck Forms
 Minor Transverse cracking in the deck surface throughout with some light scaling.
 Metal headers filled with Evazote at all bents.
 The Metal header is loose at bent 3.
 Joints are leaking at the bents.
 Deck: H-34 Calculated 2004 by Central Office (Load Factor).

General:

Built in 1976 Project #I-75-3 (40) 284 CT, 5.
 Calculations for this structure were determined by the Central Office. - February, 2004. Revised February 2009 SGM
 This structure is in Good Condition minor cracking and minor corrosion.
 Hand tools and ladder used.

Condition Rating

Temp Shored: No

Component	Material	Rating	Truck Type	Gross/H-Mod	HSMod	Tand	3-S-2	Log	Piggy
Substructure	Concrete	7	Calculated Posting	21	30	33	38	36	39
Superstructure	Steel	8	Posting Required	No	No	No	No	No	No
Deck	Concrete	7	Existing Posting	00	00	00	00	00	00

Not a School Bus Route.

Structure Does Not Require Posting

GEORGIA DEPARTMENT OF TRANSPORTATION

Deficiency Report

District: 7 Inspection Date: 3/19/2009 Inspection Area: 09
Bridge Inspector: Jerry Cooper Over: CR 160 STEVE FREY ROAD
Location ID: 067-00401D-271.97N County: Cobb
Structure ID: 067-0085-0 Asst. District Engineer: Shun Pringle

EVALUATION & DEFICIENCIES

I-75 (NBL) Over CR 160 STEVE FREY ROAD-----2.4 MI NE OF KENNESAW

Item	Units	Work	P	Date Reported	Location	Date Completed	Complete
800	LIN. FT.	700	B	5/29/2001		12/14/2001	199.00
805	LIN. FT.	240	B	3/19/2009	See comments		***

Comments:

800: Clean and seal joints at all bents.

BRIDGE INVENTORY DATA LISTING GEOGRAPHIC A DEPARTMENT OF TRANSPORTATION

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SUFF. RATING

Cobb

Structure ID: 067-0085-0

Location & Geography

* Structure I.D. No: 067-0085-0
 * 6A Feature Int: I-75 NBL
 * 6B Critical Bridge: 0
 * 7A Route Number Carried: CR00160
 * 7B Facility Carried: STEVE FREY ROAD
 * 9 Location: 2.4 MI NE OF KENNESAW
 * 91 Inspection Frequency: 00 Date: 02/01/1901
 * 4 Place Code: 00000
 * 5 Inventory Route (O/U): 2
 * Type: 4
 * Designation: 1
 * Number: 00160
 * Direction: 0
 * 16 Latitude: 34-02.5890 HMMS Prefix:
 * 17 Longitude: 84-34.8770 HMMS Suffix: MP:
 * 100 STRAHNET: 0
 * 12 Base Highway Network:
 * 13A LRS Inventory Route: 1
 * 13B Sub Inventory Route: 672016000
 * 101 Parallel Structure: 0
 * 102 Direction of Traffic: R
 * 104 Highway System: 2
 * 26 Functional Classification: 0
 * 204 Federal Route Type: 17 No.:
 * 105 Federal Lands Highway: 0
 * 110 Truck Route: 0
 * 19 Bypass Length: 02
 * 20 Toll: 3
 * 21 Maintenance: 01
 * 22 Owner: 01
 * 27 Year Constructed: 1976
 * 42 Type of Service on: 1 Under: 1
 * 43 Structure Type Main: 3 02
 * 208 Inspection Area: 09 Initials: JMC
 * Location I.D. No.: 067-00160X-000.77N
 * XReference I.D. No: 067-00401D-271.97N

Signs & Attachments

* 240 Median Barrier Rail: 0
 * 230 Guardrail Loc Dir Rear: 6
 Fwd: 6
 Oppo Dir Rear: 0
 Fwd: 0

Ratings

* 227 Collision Damage: 0

Measurements

* 29 ADT: 002200 Year: 1998
 * 28 Lanes On: 03 Under: 04
 * 48 Max. Span Length: 0123
 * 49 Structure Length: 321
 * 47 Tot. Horz. Cl: 48.00
 * 229 Shoulder Width:

Rear Lt: 2.00 Type: 1 Rt: 2.00
 Fwd Lt: 2.00 Type: 1 Rt: 2.00
 Pavement Width:
 Rear: 44.00 Type: 2
 Fwd: 44.00 Type: 2
 Intersection Rear: 1 Fwd: 0

* 228 Min. Vertical Cl

Act. Odm Dir: 20 ' 02 "
 Oppo. Dir: 99 ' 99 "
 Posted Odm. Dir: 00 ' 00 "
 Oppo. Dir: 00 ' 00 "
 * 10 Max Min Vert Cl: 20 ' 11 " Dir: 2

Hydraulic Data

* 265 U/W Insp. Arc 0 Diver: ZZZ

GEORGIA DEPARTMENT OF TRANSPORTATION
Bridge Component Report

District: 7
Bridge Inspector: Jerry Cooper
Location ID: 067-00401D-271.97N
Structure ID: 067-0085-0

Inspection Date: 3/19/2009
Over: CR 160 STEVE FREY ROAD
County: Cobb
Road Name: I-75 (NBL)

Inspection Area: 09

SubStructure Data

Bent#	Type	Foundation	Col	#Cols	Piling	#Piles	Sway	CAP	Remarks
1	A	DP		0		0		C	Only cap exposed
2	B	SF	C	4		0		C	Good
3	B	SF	C	4		0		C	Good
4	A	DP		0		0		C	Only cap exposed

SuperStructure Data

Span#	Beam Type	Spacing	Length	#Beams	Remarks
1	Steel Beams	7.90	90.00	8	50.5" Plate Girder
2	Steel Beams	7.90	123.00	8	50.5" Plate Girder
3	Steel Beams	7.90	108.00	8	50.5" Plate Girder

Bearing Data

Span#	Rear Type Bearing	FWD Type Bearing	Remarks
1	02 - Fixed Plate	05 - Rocker	Good
2	04 - Fixed Pedestal	05 - Rocker	Good
3	04 - Fixed Pedestal	05 - Rocker	Good